

# Annex P - Peat Slide Risk Assessment (PSRA)

February 2023





# CROSSAIG SUBSTATION ENVIRONMENTAL APPRAISAL

# PEAT LANDSLIDE HAZARD AND RISK ASSESSMENT

FEBRUARY 2023





Prepared By:

### **Arcus Consultancy Services**

7<sup>th</sup> Floor 144 West George Street Glasgow G2 2HG

#### T +44 (0)141 847 0340 I E info@arcusconsulting.co.uk w www.arcusconsulting.co.uk

Registered in England & Wales No. 5644976



# TABLE OF CONTENTS

1	INTRODUCTION1	
2	SITE INFORMATION AND DESK STUDY	
3	SITE SURVEYS AND RESULTS	
4	GUIDANCE AND METHODOLOGY7	
5	HAZARD AND EXPOSURE ASSESSMENT	
6	HAZARD RANKING16	
7	SLIDE RISK AND MITIGATION17	
8	CONCLUSIONS	
9	SOURCES OF INFORMATION	
APPEN	IDIX A - FIGURES	
APPENDIX B - SITE PHOTOGRAPHS		
APPENDIX C – HAZARD RANK ASSESSMENT RECORDS		

**APPENDIX D – PEAT CORING RECORDS** 



#### 1 INTRODUCTION

#### 1.1 Background

Arcus Consultancy Services Ltd (Arcus) was commissioned by SSEN Ltd (the Applicant) to carry out a Peat Landslide Hazard and Risk Assessment (PLHRA) for the proposed Crossaig Substation, Temporary Works Area (TWA), Sustainable Urban Drainage System (SUDS) attenuation pond and permanent access tracks (the Development) as part of the Argyll and Kintyre 275 kV Substations Upgrade located approximately 18 kilometres (km) south of Tarbert and 12 km north of Carradale on the eastern coast of the Kintyre peninsula (the Site).

The Development will be subject to Town and Country Planning, while the OHL Tie-In, temporary Diversion Towers and Temporary Works Area (hereby known as the Associated Development) will be submitted for Section 37 consent. The Site Layout Plan is shown on **Figure 1** in **Appendix A**.

It should be noted that the Project's construction schedules will be aligned. Therefore, peat excavation and re-use will be considered within the wider scope of the Project.

This PLHRA has been prepared to inform Argyll & Bute Council (ABC) and statutory consultees of the prevalence of peat across the Proposed Development and Associated Development as well as highlighting any potential risk of peat slide.

This PLHRA has been undertaken to Scottish Government Guidance 'Proposed electricity generation developments: peat landslide hazard best practice guide'<sup>1</sup>.

The PLHRA is accompanied by the following appendices:

- Appendix A: Figures;
- Appendix B: Site Photographs;
- Appendix C: Hazard Rank Calculations, and;
- Appendix D: Peat Coring Records.

#### 1.2 The Development

The Development will consist of the following key infrastructure:

- Substation (approx. 184 m x 129 m) ;
- Two Pylon Towers at least 43 m in height to make the connection into and out of the proposed substation;
- Four temporary Diversion Towers to divert the electricity transmission from the existing substation during construction phase of the Development;
- Temporary Work Area (approx 300 m x 120 m);
- A Sustainable Urban Drainage System (SUDS) Attenuation Pond (approximately 80 m x 30 m);
- Permanent access track, approximately 660 m in length to the new access track between the existing Crossaig substation and the proposed Crossaig North substations and for access to the SuDS pond; and
- An extension to the south of the substation platform at the existing Crossaig substation of (approx 17.5m x 30m) to support electrical equipment and associated access.

The Site Layout is shown on Figure 1 in Appendix A.

<sup>&</sup>lt;sup>1</sup> Scottish Government (2017) Proposed electricity generation developments: peat landslide hazard best practice guide <u>Proposed electricity generation developments: peat landslide hazard best practice guide - gov.scot (www.gov.scot)</u> (Accessed 02/08/2022)



#### 1.3 Scope and Purpose

The scope of this PLHRA is to:

- Review available desk-based information on the Site;
- Undertake a site walkover survey and peat probe surveys to characterise the prevailing ground conditions and identify existing or potential peat instability;
- Report on the findings of the survey and assess the potential instability risk and estimate the hazard from any potential peat slide; and
- Recommend mitigation measures and specific construction methodologies that should be considered during the construction period, if required.

This PLHRA provides factual information on the peat survey results relating to the proposed infrastructure locations. The desk-based information and site surveys have been utilised to assess the potential risk of any peat slide. The methodology adopted, and details on the assessment, are outlined in **Sections 3**, **4 and 5** of this PLHRA. The assessment has been undertaken in accordance with Scottish Government Guidance in assessing the likelihood, and consequence, of peat slide<sup>2</sup>.

#### 1.4 Project Team

Team Member	Job Title	Qualifications	No. Years Experience
Gregor Hirst	Senior Engineer	BSc (Hons)	6 Years
David Ballentyne	Principal Engineer	BSc (Hons)	18 Years
Tomos Ap Tomos	Technical Director	BEng (Hons) MCIHT	25 Years

This assessment was undertaken by Gregor Hirst (BSc Hons), a Geo-Environmental Engineer of 6 years, and was supported by David Ballentyne a Geo-Environmental Civil Engineer with for over 18 years of experience in ground condition assessment. This Chapter has been technically reviewed by Tomos Ap Tomos, Technical Director of Engineering.

<sup>2</sup> Scottish Government (2017): Peat Landslide Hazard and Risk Assessments: Best Practice Guide for Proposed Electricity Generation Developments; Second Edition, April 2017 [Online]. Available at: <u>https://www.gov.scot/binaries/content/documents/govscot/publications/advice-and-guidance/2017/04/peat-landslide-hazard-risk-assessments-best-practice-guide-proposed-electricity/documents/00517176-pdf/00517176-</u>



#### 2 SITE INFORMATION AND DESK STUDY

#### 2.1 Site Description and Topography

The land within the site boundary (the Site) which contains the Development is located approximately 18 kilometres (km) south of Tarbert, covering an area of approximately 80 hectares (ha) centred on National Grid Reference (NGR) 182545, 650307. The Site is located within the administrative boundary of Argyll & Bute Council (the Council). The Site is adjacent to the existing Crossaig Substation which connects to the B842 from the east.

The topography of the Site and immediate vicinity is gently undulating throughout. The elevation of the Site ranges from around 80 metres (m) Above Ordnance Survey Datum (AOD) to around 96 m AOD in the area of the proposed substation.

There are a number of unnamed surface water features, mainly in the form of drainage channels associated with the forestry plantation, however no watercourses are recorded other than Allt na Buaile Salaich, which runs along the south western Project boundary and is the receptor for the proposed SUDS outfall.

The predominant land use within the Site consists of commercial forestry plantation.

#### 2.2 Site Walkover

The purpose of the desk study and site visit was to gain a thorough understanding of site conditions including topography, geology, existing peat instability and hydrology. The outcome of this stage of the study was to determine which areas required detailed intrusive survey (by peat probing) and ultimately provide data for the assessment of PLHRA.

A site walkover was undertaken in November 2021 prior to the commencement of the peat probing exercise. The Site was examined for evidence of peatlands, presence of landslip and localised hagging. Geological mapping and areas of interest were pre-loaded to a handheld device for reference during the site walkover. Following a review of these in parallel with the initial site walkover, the desk study aimed to identify and or verify the following:

- The general condition of peat deposits;
- Evidence of any previous peat instability;
- The presence of low lying wet/peat lands; and
- Watercourses and potential other receptors.

#### 2.2.1 Site Conditions

The entirety of the Site is utilised for forestry plantations, other than the area of the proposed temporary works area, adjacent to the south of the existing Crossaig substation. This area contains a mixture of upfilled land that has been engineered to act as a working platform with an access track running through it, while the remainder of the area has been subject to felling and currently comprises open hummocky ground. Within the plantation area there are a number of forestry rides and clearings which were noted to contain sphagnums and high groundwater levels, resulting in areas of soft ground.

Extensive felling has recently been undertaken in the area north and east of the proposed substation, associated with the ongoing infrastructure works in the area.

Neither mining or quarry activities are known to have taken place at the Site.

Site photographs taken during the site walkover are included in **Appendix B**.



#### 2.3 Published Geology

#### 2.3.1 Superficial Soils

Available British Geological Survey (BGS)<sup>3</sup> indicates an absence of superficial deposits across the majority of the Site. The exception being the presence of glacial deposits in the form of Devensian Till which are recorded at the northern extent of the Site.

Figure 2 illustrates the 'Superficial Soils' map included in Appendix A.

#### 2.3.2 Solid Geology

Published bedrock geology mapping information on solid geology indicates the entirety of the Site to be underlain by Gritty Psammite and Pelite of the Beinn Bheula Schist Formation.

No geological faults or linear features are present at the Site or in the surrounding area.

Figure 3 illustrates the 'Solid Geology' included in Appendix A.

#### 2.4 Hydrology and Hydrogeology

The Site is characterised by its generally low-gradient topography, but the area surrounding the Site has a more variable landscape in terms of topography. The Site lies within the Kintyre Coastal catchment that is mainly drained by a river, the Crossaig Water.

Crossaig Water passes to the north of the Site and flows in an eastern direction. This watercourse has a Scottish Environment Protection Agency (SEPA) overall classification<sup>4</sup> of 'Good'. There are several smaller watercourses located on the Site that drain either directly to the Firth of Clyde, or into Crossaig Water.

Initial desk-based review indicated the Site is likely to be partially underlain by peat with significant quantities of pockets of deep peat in isolated areas.

The SEPA Aquifer Classification Map of Scotland<sup>5</sup> reveals that the Site is situated within an area underlain by a low productivity aquifer where flow is virtually all through fractures and other discontinuities.

The SEPA River Basin Management Plan Interactive Map reveals that the Site is underlain by the Oban and Kintyre groundwater body. This groundwater body is classified by SEPA under the Water Framework Directive<sup>6</sup> as having a status of Good.

Figure 4 illustrates the Geomorphology of the Site and is included in Appendix A.

#### 2.5 Historical Landslip and Geomorphology

No evidence of historic landslip or peat hagging was noted during the Site walkover and topsoil, where undisturbed, generally appeared to be in good condition. Due to the presence of extensive forestry plantations at the Site; it is considered that properties of the peat deposits may have been altered and may not pose the same risk of instability as undisturbed peat. Nonetheless, the possibility of instability within peat soils cannot be discounted, especially where there are significant topographic variances and the presence of watercourses.

<sup>&</sup>lt;sup>3</sup> British Geological Survey (2019) Geology of Britain [Online] Available at:

http://mapapps.bgs.ac.uk/geologyofbritain/home.html (Accessed 03/08/2022)

<sup>&</sup>lt;sup>4</sup> SEPA Water Classification Hub (2020) [Online] Available at: <u>Water Classification Hub (sepa.org.uk)</u> (Accessed 03/08/2022)

<sup>&</sup>lt;sup>5</sup> Scotland's Environment (2019) SEPA Aquifer Classification Map of Scotland [Online] Available at: <u>https://map.environment.gov.scot/sewebmap/</u> (Accessed 03/08/2022)

<sup>&</sup>lt;sup>6</sup> European Parliament (2000) Directive 2000/60/EC [Online] Available at: <u>https://eur-</u>

lex.europa.eu/resource.html?uri=cellar:5c835afb-2ec6-4577-bdf8-756d3d694eeb.0004.02/DOC\_1&format=PDF (Accessed 03/08/22)



#### 3 SITE SURVEYS AND RESULTS

#### 3.1 Investigations

The existing peat depths across the Site have been determined through a multi-phased peat probe survey undertaken as recommended in the NatureScot (formally Scottish Natural Heritage), Scottish Government and James Hutton Institute guidance for investigating peat<sup>7</sup>.

The probe positions for the survey were determined by the proposed layout of the Development and provided detailed information across the various proposed infrastructure at frequencies as follows:

- Substation 10 m x 10 m grid to the extent of the proposed footprint;
- Pylon Locations 10 m x 10 m grid to an area of 50 m<sup>2</sup>;
- Temporary Works Area 25 m x 25 m grid; and
- Tracks Every 50 m along the centreline with perpendicular offsets, 15-25 m either side.

It should be acknowledged that natural variations in peat depth/thickness could occur between probe positions, although areas of infrastructure had undergone intensely spaced probing and this would be less likely.

#### 3.2 Summary of Peat Depths

Throughout the peat survey, a total of 714 probes were progressed. The average peat depth across the Site is 0.40 m with greater than 77% of probes recording peat depths of 0.5 m or less and 91% recording depths of 1.0 m or less. Thick peat (where the depth was greater than >1.0 m) was recorded at 9% of locations. The majority of thick peat was recorded at depths between 1.0 m – 2.0 m with only 1.3% of all probes recording depths in excess of 2.0 m.

The maximum peat depth recorded at the Site was 3.2 m within a clearing between trees not utilised within the commercial plantation. Topographically the area is relatively flat and surface vegetation in the form of sphagnum and high groundwater levels were recorded. The area is located between the proposed substation and the first proposed pylon location to the north of the proposed substation, therefore there is no proposed infrastructure in this area.

Peat Depth Range (m)	Nº of Peat Probes	Percentage of Total
0.00 - 0.50	551	77.17
0.51 - 1.00	99	13.87
1.01 - 1.50	39	5.46
1.51 - 2.00	16	2.24
2.01 - 2.50	5	<1.0
2.51 - 3.00	3	<1.0
3.01 - 3.50	1	<1.0
Σ =	714	

 Table 1 summarises the recorded peat depths.

Table 1 · Peat Denth Summary

<sup>&</sup>lt;sup>7</sup> Scottish Government, Scottish Natural Heritage, SEPA (2017) Peatland Survey. Guidance on Developments on Peatland, online version only. Available at: <u>Guidance+on+developments+on+peatland+++peatland+survey+++2017.pdf (www.gov.scot)</u> Accessed (03/08/2022)



The peat probe locations and depths are shown on **Figure 5** appended with this PLHRA, and details of probe records are included in **Appendix C**.

The Interpolated Peat Depths are illustrated on Figure 6.



#### 4 GUIDANCE AND METHODOLOGY

#### 4.1 Overview of Guidance and Peat Failure Mechanisms

#### 4.1.1 Peat Depth and Slope

The Scottish Government guidance divides peat instability into two categories: 'peat slides' and 'bog bursts'. The guidance states that peat slides have a greater risk of occurrence in areas where:

- Peat is encountered at or near to ground surface level;
- The thicknesses are recorded in the region of 2.0 m (above which, in general terms, peat instability would increase with peat thickness); and
- The slope gradients are steep (between 5° and 15°).

Bog bursts are considered to have a greater risk of occurrence in areas where:

- Peat depth is greater than 1.5 m; and
- Slope gradients are shallow (between 2° and 10°).

It should be noted however that peat instability events, although uncommon, can occur out with these limits. Reports of bog bursts are generally restricted to the Republic and Northern Ireland.

Further to the general guidance above, in relation to peat depth, it is considered that the extent and depth of peat is controlled to a degree by rainfall and elevation, giving rise to three common types of peat (Boylan et al. 2008<sup>8</sup>):

- Upland Blanket Bog: Blanket bogs are typically about 3 m thick however, they can be up to 5 m thick. Generally thinning at greater elevations;
- Raised Bog: Raised bogs generally tend to be 3-12 m thick, averaging 7 m with their growth occurring above the water table; and
- Lowland Blanket Bog: Much the same as the upland version; however, they form around sea level in areas of very high rainfall.

Generally, the potential for peat instability increases with peat depth, however other instability indicators need to be considered, namely slope and substrate.

#### 4.1.2 Substrate

Peat slide failures tend to occur at the interface of the peat and underlying substrate therefore, understanding the nature of the underlying substrate can provide a key factor when considering the risk stability.

Using the peat probe refusal, an estimation of the underlying materials can be determined based on:

- Gradual refusal Clay;
- Crunching/Gritty Weathered Rock/Sand and Gravel; or
- Abrupt Refusal/Hard Rock.

Where sand and/or gravel is recorded, the interface is considered to be the best-case scenario with the highest friction value.

Where clay is recorded, the upper horizons of the clay are typically softened through poor drainage in this soil group with low shear strengths expected. While rock substrate provides a high strength, the surface being smooth can lead to a weak interface, with similar risk to that of a clay substrate.

<sup>&</sup>lt;sup>8</sup> Boylan et al (2008) Peat Slope Failure in Ireland



The presence of slip material, or evidence of peat instability would represent the worstcase scenario for the assessment of substrate.

The substrate parameters are included in the Hazard and Exposure Assessment in **Section 5** of this PLHRA.

#### 4.1.3 Other Considerations

Preparatory factors which effect the stability of peat slopes in the short to medium-term include:

- Loss of surface vegetation (deforestation);
- Changes in sub-surface hydrology;
- Increase in the mass of peat through accumulation, increase in water content and growth of tree planting; or
- Reduction in shear strength of peat or substrate due to chemical or physical weathering, progressive creep and tension cracking.

Triggering factors which can have immediate effect on peat stability and act on susceptible slopes include:

- Intensive rainfall or snow melt causing pressures along existing or potential peat/substrate interfaces;
- Snow melt;
- Alterations to drainage patterns, both surface and sub-surface;
- Peat extraction at the toe of the slope reducing the support of the upslope material;
- Peat loading (commonly due to stockpiling) causing an increase in shear stress; and
- Earthquakes or rapid ground accelerations such as due to blasting or mechanical movement.

Consideration of peat stability should form an integral part of the design and construction of infrastructure in peatland areas. While peat does not wholly provide a development constraint, areas of deep peat or peat deposits on steep slopes should be either avoided through design and micro-siting; or mitigation measures should be designed to avoid instability and movement.

#### 4.2 Methodology

Despite being an application under the Town and Country Planning (Scotland) Act 1997<sup>9</sup>, the PLHRA has been carried out in accordance with the Energy Consents Unit, Scottish Government guidance of 2017 titled Peat Landslide Hazard and Risk Assessments - Best Practice Guide for Proposed Electricity Generation Developments<sup>10</sup>.

In June 2014, Scottish Planning Policy<sup>11</sup> (SPP) and National Planning Framework (NPF3)<sup>12</sup> were published. In relation to peat and the assessment of effects on resource, NPF3 references SNH Scotland's National Peatland Plan<sup>13</sup>. These policy, framework and guidance documents are considered in this PLHRA. The PLHRA undertaken is based on:

- Desk based assessment;
- Site Walkover;

<sup>&</sup>lt;sup>9</sup> Scottish Government (1997) Town and Country Planning (Scotland) Act 1997 [Online] Available at: <u>http://www.legislation.gov.uk/ukpga/1997/8/contents</u> (Accessed 20/08/22)

<sup>&</sup>lt;sup>10</sup> Scottish Government (2017) Peat Landslide Hazard and Risk Assessment: Best Practice Guide for Proposed Electricity Generation Development [Online] Available at: <u>https://www.gov.scot/Publications/2017/04/8868 (</u>Accessed 20/08/22)

<sup>&</sup>lt;sup>11</sup> Scottish Government (2014) Scottish Planning Policy [Online] Available at: <u>http://www.scotland.gov.uk/Topics/Built-Environment/planning/Policy (</u>Accessed 20/08/22)

<sup>&</sup>lt;sup>12</sup> Scottish Government (2014) National Planning Framework 3 [Online] Available at:

http://scotland.gov.uk/Resource/0045/00453683.pdf (Accessed 20/08/22)

<sup>&</sup>lt;sup>13</sup> SNH (2015) Scotland's National Peatland Plan [Online] Available at: <u>https://www.nature.scot/climate-change/taking-action/carbon-management/restoring-scotlands-peatlands/scotlands-national-peatland-plan (</u>Accessed 20/08/22)



- Infrastructure specific probing; and
- A hazard and risk ranking assessment.

The area of the Site subject to assessment was determined by the proposed development layout which considered both anticipated peat deposits as well as other physical and environmental constraints.

#### 4.2.1 Development of Hazard Rank

The early stages of the PLHRA including the desk study, site visit and peat probing were carried out in parallel with the assessment of wider constraints to inform the layout of the Development. Following identification of peat depths within the Site, the assessment has determined the potential effects on the peat resource from construction activities which would include:

- Construction of tracks;
- Foundation construction;
- Construction of hardstanding; and
- Temporary storage of peat and soils.

An assessment of the peat probing data and a review against desk study information was undertaken and a hazard rank was calculated for different zones across the site reflecting risk of peat instability/constraint to construction.

Where practical, the Development design would be progressed to avoid areas of a risk score above 'low'. Where this has would not be achievable, areas affected would be discussed in both the EIA as having significant effect, with relative mitigation measures proposed to reduce this, and recorded on a risk register which sets out specific mitigation measures which are considered necessary to reduce the risk of inducing instability.

Details of the hazard and risk ranking assessment is included in **Sections 5 and 6** of this PLHRA.



#### 5 HAZARD AND EXPOSURE ASSESSMENT

#### 5.1 Background

A 'Hazard Ranking' system has been applied across the Site based on the analysis of risk of peat slide as outlined in the Scottish Government guidance. This is applied on the principle:

```
Hazard Ranking = Hazard x Exposure
```

Where 'Hazard' represents the likelihood of any peat slide event occurring and 'Exposure' being the impact or consequences that a peat slide may have on sensitive receptors that exist on and around the Site.

#### 5.2 Methodology

The determination of Hazard and Exposure values is based on a number of variables which impact the likelihood of a peat slide (the Hazard), and the relative importance of these variables specific to the Site.

Similarly, the consequences or Exposure to receptors is dependent on variables including the particular scale of a peat slide, the distance it will travel and the sensitivity of the receptor.

In the absence of a predefined system, the approach to determining and categorising Hazard and Exposure is determined on a Site by Site basis. The particular system adopted for the Development PLHRA assessment is outlined in the following sub sections.

#### 5.3 Hazard Assessment

The potential for a peat slide to occur during construction depends on several factors, the importance of which can vary from Site to Site. The factors requiring considerations would typically include:

- Peat depth;
- Slope gradient;
- Substrate material;
- Evidence of instability or potential instability;
- Vegetation cover; and
- Hydrology.

Of these, peat depth and slope gradient are considered to be principal factors. Without a sufficient peat depth and a prevailing slope, peat slide hazard would be negligible.

The Slope Gradient has been established using a Digital Terrain Model (DTM) to a resolution of 5 m, which is illustrated on **Figure 7**. For the Development and Associated Development, the substrate material is also considered a relevant factor in relation to slide.

Vegetation cover and evidence of instability or potential instability were assessed during site surveys and, alongside satellite photography, informed the Geomorphology Map presented in **Figure 4**. This information was also considered during the adoption of hazard zones across the Site, which are presented in **Figure 9: Hazard Rank Zonation Plan**.

Due to the nature of the assessment and number of data points used to establish hazard ranking, gathering hydrological data at each probe point through the use of groundwater boreholes and a subsequent monitoring period is considered impractical. Therefore, an assumption on groundwater levels has been adopted for the assessment that 90% of the



peat at each probe location is below the water table. As such, it is assumed that the water table across the Site is relatively high.

#### 5.4 Hazard Rating

When several factors may impact on the Hazard potential, a relative ranking process is applied attributing different weighting to each factor as shown below.

#### Table 2: Coefficients for Slope Gradients

Slope Angle (degrees)	Slope Angle Coefficients
Slope < 2°	1
$2^{\circ} < \text{Slope} < 4^{\circ}$	2
4° < Slope < 8°	4
8° < Slope < 15°	6
Slope >15°	8

#### Table 3: Coefficients for Peat Thickness and ground conditions

Peat Thickness	Ground Conditions Coefficients
Peaty or organic soil (<0.5 m)	1
Thin Peat (0.5 – 1.0 m)	2
Deep Peat (>1.0 m)	3*
Deep Peat (>3.0 m)	8

\* - Note that thicker peat generally occurs in areas of shallow gradient and records and research indicate that thick peat does not generally occur on the steeper gradients.

#### Table 4: Coefficients for Substrate

Substrate Material	Substrate Coefficients
Sand/gravel	1
Rock	1.5
Clay	2
Not proven	2
Slip material (Existing materials)	5

The Hazard Rating Coefficient for a particular location is calculated using the following equation:

## Hazard Rating Coefficient = Slope Gradient x Peat Thickness x Substrate

From the Hazard Rating Coefficient, the risk to stability can be ranked as set out in **Table 5**.

Hazard Rating Co-efficient	Potential Stability Risk (Pre-Mitigation)
<5	Negligible
5 to 15	Low
16 to 30	Medium
31 to 50	High

#### Table 5: Hazard Rating



> 50 Very High

#### 5.5 Peat Stability Assessment

The likelihood of a particular slope or hillside failing can be expressed as a Factor of Safety. For any potential failure surface, there is a balance between the weight of the potential landslide (driving force or shear force) and the inherent strength of the soil or rock within the hillside (shear resistance).

The guidance states that the 'Infinite Slope' method of analysis, after Skempton and DeLory (1957), is the most well established and commonly applied method for the assessment of peat slope stability. The stability of a slope can be assessed by calculating the factor of safety F, which is the ratio of the sum of resisting forces (shear strength) and the sum of the destabilising forces (shear stress):

$$F = \frac{c' + (\gamma - m\gamma_w) z \cos^2 \beta \tan \phi'}{\gamma z \sin \beta \cos \beta}$$

Where *c*' is the effective cohesion, *y* is the bulk unit weight of saturated peat, *yw* is the unit weight of water, *m* is the height of the water table as a fraction of the peat depth, *z* is the peat depth in the direction of normal stress, *b* is the angle of the slope to the horizontal and  $\phi$  ' is the effective angle of internal friction. Values of F < 1 indicate a slope would have undergone failure under the conditions modelled; values of F > 1 suggest conditions of stability.

Assumed geotechnical parameters have been utilised in the formula to inform the stability assessment, based on literature values to inform the stability analysis, as included in **Table 6**.

Reference	Effective Cohesion C' (kPa)	Effective Angle of Friction <b>¢</b> (°)	<b>Unit Weight Ƴ</b> (kN/m2)	Comments
Hanrahan et al (1967) <sup>14</sup>	5.5 – 6.1	36.6 - 43.5	-	Remoulded H4 Sphagnum peat
Hollingshead and Raymond (1972) <sup>15</sup>	4.0	34	-	-
Hollingshead and Raymond (1972)	2.4 - 4.7	27.1 – 35.4	-	Sphagnum peat (H3, mainly fibrous)
Carling (1986) <sup>16</sup>	6.52	0	10	-
Kirk (2001) <sup>17</sup>	2.7 – 8.2	26.1 - 30.4		Ombrotrophic blanket peat

Table 6: Literature for Geotechnical Parameters of Peat

<sup>&</sup>lt;sup>14</sup> Hanrahan et al (1967) - Hanrahan, E.T., Dunne, J.M., and Sodha, V.G. 1967. Shear strength of peat. Proceedings Geotechnical Conference, Oslo, Vol. 1, pp. 193–198.

<sup>&</sup>lt;sup>15</sup> Hollingshead and Raymond (1972) - Hollingshead, G.W., and Raymond, G.P. 1972. Field loading tests on Muskeg, Canadian Geotechnical Journal, 9(3): 278–289.

 <sup>&</sup>lt;sup>16</sup> Carling (1986) - Peat slides in Teesdale and Weardale, northern pennines, july 1983: Description and failure mechanisms
 <sup>17</sup> Kirk (2001) - Initiation of a multiple peat slide on Cuilcagh Mountain, Northern Ireland



Warburton et al (2003) <sup>18</sup>	5.0	23	9.68	Basal Peat
Warburton et al (2003)	8.74	21.6	9.68	Fibrous Peat
Dykes and Kirk (2006)	3.2	30.4	9.61	Acrotelm
Dykes and Kirk (2006)	4.0	28.8	9.71	Catotelm

C' – effective cohesion (kPa), typically ranging from 2.5 to 8.5 therefore 5.0 has been adopted for the purposes of the assessment.

 $\phi$  – effective angle of friction (°), typically ranging from 21.6 to 43.5 therefore 29.6 has been adopted for the purposes of the assessment.

 $\Upsilon$  – unit weight (kN/m2), typically ranging from 9.61 to 10, therefore 10 has been adopted for the purposes of the assessment.

In accordance with the best practice method, F values of <1.0 indicate slopes that would experience failure under the modelled conditions and as such are considered areas of high risk. However, Boylan et al (2008) indicate that a relatively high value of F=1.4 should be used to identify slopes with the potential for instability. Adopting this approach, high risk areas area indicated where F is <1.0, medium risk areas are indicated as 1.01 to 1.50 and >1.5 are low risk.

Using digital terrain modelling and GPS co-ordinates of each peat probe, a factor of Safety, F has been calculated for each probe locations which has been interpolated through ArcGIS Spatial Analyst tools. The Factor of Safety Assessment provides a sense check of the ranking based system, providing an absolute approach to the 'Factor of Safety Plan' is shown on **Figure 8**.

The results of the Factor of Safety calculations indicated all points on the Site as low risk. This was primarily due to the light undulating topography and generally flat-lying conditions on the Site combined with generally shallow peat depths across the Site.

#### 5.6 Exposure Assessment

The main exposure receptors identified at the Site and in the surrounding areas which could potentially be affected in the event of a peat slide are the existing Crossaig Substation, located adjacent to the Site to the east, the proposed development, private dwellings located approximately 200 m north east of the northernmost temporary tower and various unnamed watercourses that flow within the Site boundary before joining the Firth of Clyde to the east.

The impact of a peat slide on receptors can be assessed on a relative scale based on the potential for loss of habitat, a historical feature or disruption/danger to the public. To effectively assess the impact, the assessment of Exposure effect must also consider the distance between the hazard and the receptor, and the relative elevation between the two.

#### 5.7 Exposure Rating

Similar to the Hazard Rating, the Exposure Ratings were determined using relative ranking process by attributing the different weighting systems to each factor as shown below:

<sup>&</sup>lt;sup>18</sup> Warburton et al (2003) - Anatomy of a Pennine peat slide, Northern England

### Table 7: Coefficients for Receptor Type

Receptor	Receptor Coefficients
Road, path or track	3
Minor water feature	6
Site infrastructure	6
Dwelling	8
Major water feature	8
Blanket bog	8

 Table 8: Coefficients for Distance from Receptor

Distance from Receptor	Distance Coefficients
> 1 km	1
100 m to 1 km	2
10 m to 100 m	3
<10 m	4

#### Table 9: Coefficients for Receptor Elevation

Receptor Elevation	Elevation Coefficients
< 10 m	1
10 m to 50 m	2
50 m to 100 m	3
> 100 m	4

The Exposure Rating Coefficient for a particular location is calculated using the following equation:

## Exposure Rating Coefficient = Receptor x Distance x Elevation

From the Exposure Rating Coefficient, the risk to stability can be ranked as set out in **Table 10**.

Table 10: Exposure Rating

Exposure Rating Co-efficient	Potential Stability Risk (Pre-Mitigation)
<6	Very Low
6 to12	Low
13 to 24	High
24 to 30	Very High
>30	Extremely High



#### 5.8 Rating Normalisation

In order to achieve an overall Hazard Ranking in accordance with the Scottish Government Guidance, the Hazard and Exposure Rating Coefficient derived from the coefficient tables are normalised as shown in **Table 11**.

Table 11: Rating Normalisation

Hazard Rating		Exposure Rating		
Current Scale	Normalised Scale	Current Scale	Normalised Scale	
< 5 Negligible	1	<6 Very Low	1	
5 to 15 Low	2	6 to 12 Low	2	
15 to 30 Medium	3	13 to 24 High	3	
30 to 50 High	4	25 to 30 Very High	4	
>50 Very high	5	>30 Extremely High	5	

The record of the Hazard Rank Assessment is included in **Appendix C** of this PLHRA.



#### 6 HAZARD RANKING

Having identified the rating coefficients in **Section 5** of this PLHRA, it is possible to categorise areas of the Site with a Hazard Ranking by multiplying the Hazard and Exposure Rating. Hazard Ranking and associated suggested actions matrix are shown in **Tables 12** and **13** below:

Table 12: Hazard	Ranking and	Suggested Actions

Hazard Ranking		Action Suggested in the Scottish Executive Guidance	
17-25	High	Avoid project development at these locations.	
11-16	Medium	Project should not proceed unless hazard can be avoided or mitigated at these locations, without significant environmental impact, in order to reduce hazard ranking to low or less	
5-10	Low	Project may proceed pending further investigation to refine assessment. Mitigation of hazards maybe required through micro- siting or re-design at these locations.	
1-4	Negligible	Project should proceed with monitoring and mitigation of peat landslide hazards at these locations as appropriate.	

#### Table 13: Hazard Ranking Matrix

	5	Low	Low	Medium	High	High
Rating	4	Negligible	Low	Medium	Medium	High
	3	Negligible	Low	Low	Medium	Medium
Hazard	2	Negligible	Negligible	Low	Low	Low
	1	Negligible	Negligible	Negligible	Negligible	Low
		1	2	3	4	5
	Exposure Rating					

Receptor exposure was assessed for each of the seven hazard zones using the approach in **Section 5**. A summary of the Hazard Ranking result for each identified area is summarised in **Table 14** and is presented in **Figure.9** - Hazard Ranking Zonation Plan. The zonation is based on a combination of considerations including calculated hazard result, peat depth, topography and receptors and land uses.



#### 7 SLIDE RISK AND MITIGATION

#### 7.1 General

The PLHRA has shown the Site to be generally of 'negligible' hazard ranking, with isolated areas of 'low' hazard ranking. No Medium or High risk areas have been identified within the Proposed Development or Associated Development and therefore a significant risk of peat slide is not considered to be present based on the Hazard Ranking assessment. Nonetheless, a risk from peat slide may still exist and mitigation measures as outlined in **Section 7.3** of this PLHRA should be applied to minimise any risk.

Where the hazard ranking has been lowered through mitigation measures, the original ranking will remain in the overall hazard zoning plan. It should be acknowledged that the hazard zonation plan is based on the pre-mitigation status.

While specific recommended mitigation in 'low' ranked areas are proposed, other mitigation is embedded in the design. It is also necessary for detailed design and construction of the Proposed Development and Associated Development to be undertaken in a competent and controlled manner and in line with best practice measures, specifically relating to the management and reuse of excavated peat.

The embedded mitigation and good practice measures are set out in Section 7.2 and Section 7.3 of this PLHRA. It should be noted that the mitigation measures defined are not exclusive and other forms of mitigation may well be required and should be implemented during construction of the Proposed Development and Associated Development.

	Hazard Area and Infrastructure		Unmitigated Hazard		
Hazard Area	Infrastructure Affected	Ranking	Key Aspects	Specific Actions	Ranking
H1	Proposed temporary works area, SUDS attenuation pond and proposed permanent access track	Negligible	Location and topography: Southern and eastern sectors of the Proposed Development. Indicated by the Indicative Town & Country Planning Boundary in Figure 9 within <b>Appendix A</b> . Hydrology: None Peat Depth: 0.0 m – 3.0 m. Generally, <1.0 m Slope Gradient: 0° to >10° Exposure: Proposed infrastructure	Micro-siting in to areas of thinner peat where required. Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Annex N: Water Construction Environmental Management Plan (WCEMP) and management of peat and peaty soils as outlined in Annex O: Peat Management Plan (PMP).	Negligible
H2	Proposed Substation	Negligible	Location and topography: Western and north western	Micro-siting in to areas of thinner	Negligible

# Table 14: Hazard Ranking



Hazard / Infrastru	Area and ucture	Unmitigated	Hazard	Mitigated Hazard	
			sectors of the Proposed Development comprising the southern two thirds of the proposed substation. Hydrology: None Peat Depth: 0.0 m – 2.1 m. Generally, <0.5 m Slope Gradient: 0° to <5° Exposure: Proposed Infrastructure	peat where required. Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in <b>Annex</b> <b>N: WCEMP</b> and management of peat and peaty soils as outlined in <b>Annex O: PMP</b> .	
НЗ	Proposed Substation	Low	Location and topography: Small zone to the north of the Proposed Development containing the northern third of the proposed substation. Hydrology: None Peat Depth: 0.0 m – 3.0 m. Generally, <1.0 m Slope Gradient: 0° to <10° Exposure: Proposed Infrastructure	Micro-siting in to areas of thinner peat where required. Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in <b>Annex</b> <b>N: WCEMP</b> and management of peat and peaty soils as outlined in <b>Annex O: PMP.</b> During construction visual inspections and monitoring in areas with the potential for peat slide risk should take place.	Negligible
H4	Proposed indicative tower location, proposed OHL alignment and proposed permanent access track	Negligible	Location and topography: Southern sector of the Associated Development, adjacent to the north of the Proposed Development. Hydrology: None	Micro-siting in to areas of thinner peat where required. Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in <b>Annex</b> <b>N: WCEMP</b> and management of	Negligible



Hazard / Infrastru	Area and ucture	Unmitigated	Hazard	Mitigated Hazard	
			Peat Depth: 0.1 m – 3.2 m. Generally, <1.0 m Slope Gradient: 0° to <15° Exposure: Proposed infrastructure	peat and peaty soils as outlined in <b>Annex O: PMP.</b>	
H5	Proposed OHL alignment	Low	Location and topography: Central western sector of the Associated Development Hydrology: An unnamed watercourse runs from west to east through the zone Peat Depth: 0.1 m – 1.7 m. Generally, <1.0 m Slope Gradient: 0° to <10° Exposure: Proposed infrastructure	Micro-siting in to areas of thinner peat where required. Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in <b>Annex</b> <b>N: WCEMP</b> and management of peat and peaty soils as outlined in <b>Annex O: PMP.</b> During construction visual inspections and monitoring in areas with the potential for peat slide risk should take place.	Negligible
H6	Proposed indicative tower location, proposed OHL alignment and proposed permanent access track	Negligible	Location and topography: Central eastern sector of the Associated Development Hydrology: An unnamed watercourse runs from west to east through the zone Peat Depth: 0.0 m - 0.3 m. Generally, <0.2 m Slope Gradient: 0° to <10° Exposure: Proposed infrastructure	Micro-siting in to areas of thinner peat where required. Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in <b>Annex</b> <b>N: WCEMP</b> and management of peat and peaty soils as outlined in <b>Annex O: PMP</b> .	Negligible

Hazard I Infrastr	Area and ucture	Unmitigated	Hazard	Mitigated Hazard	
H7	Proposed temporary towers	Negligible	Location and topography: Eastern sector of the Associated Development Hydrology: An unnamed watercourse runs from south west to north east through the zone Peat Depth: 0.0 m - 1.5 m. Generally, <0.5 m Slope Gradient: 0° to <10° Exposure: Proposed infrastructure	Micro-siting in to areas of thinner peat where required. Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in <b>Annex</b> <b>N: WCEMP</b> and management of peat and peaty soils as outlined in <b>Annex O: PMP</b> .	Negligible

#### 7.2 Embedded Mitigation

Embedded mitigation includes measures taken during design of the Development to reduce the potential for peat slide risk. In summary the principal measures that have been taken are:

- Locating infrastructure on shallower slopes, where possible; and
- Locating infrastructure on areas of shallow peat (or no peat) where possible.

#### 7.3 Peat Slide Mitigation Recommendations

The following mitigation measures should be adopted post consent stage to validate the PLHRA and influence the detailed design of the Development, including:

- Ground investigations prior to detailed design;
- Identification of areas sensitive to changes in drainage regime prior to detailed design;
- Update the PLHRA as necessary following detailed ground investigations;
- Development of a drainage strategy that will not create areas of concentrated flow and will not affect the current peatland hydrology;
- Design of a Development drainage system for tracks and hardstanding that will require minimal ongoing maintenance during the operation of the windfarm;
- Inspection and maintenance of the drainage systems during construction and operation;
- Identification of suitable areas for stockpiling material during construction prior to commencement of works; and
- Consideration of specific construction methods appropriate for infrastructure in peat land (i.e. geogrids) as part of design Development.



#### 8 CONCLUSIONS

This PLHRA has been undertaken for the Development in accordance with best practice, as detailed in **Section 4.2** of the PLHRA. The assessment included a desk study followed by completion of an intensive probing exercise across the proposed infrastructure and surrounding areas at the Proposed Development and Associated Development. The information gathered during this investigation was used to develop a Hazard Ranking across the Site.

The findings of the probing indicate that deep peat is present at the Site, however a vast majority of the Development is underlain by peat less than 1.0 m in thickness. Pockets of deep peat were recorded at up to 3.0 m in the southern area of the Proposed Development and up to 3.2 m in the southern area of the Associated Development.

Based on the scope of the study, the PLHRA has indicated that the majority of the Site is generally of 'negligible hazard ranking with two areas highlighted as 'low' hazard ranking.

Notwithstanding the findings of the PLHRA, the final design of infrastructure should be carefully sited and micro-siting adopted if required in order to maintain the design objective of avoiding any potential peat slide risk.



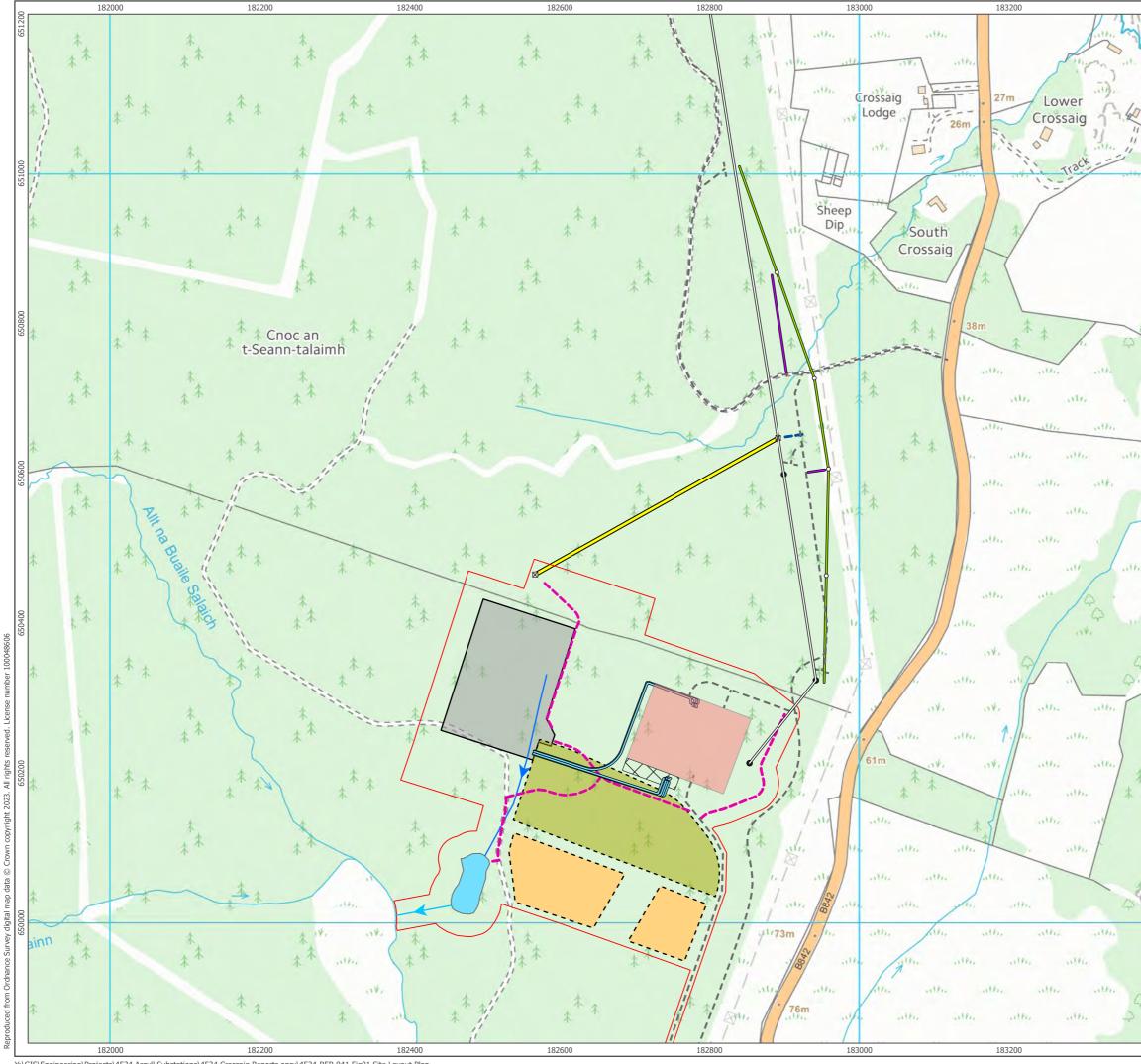
#### 9 SOURCES OF INFORMATION

The following sources of information were used as part of the desk study investigations:

- British Geological Survey Online GeoIndex;
- Ordnance Survey (OS) topographical information;
- Aerial and Satellite photography.
- Soil Survey of Scotland MacAulay Institute for Soil Research (1984);
- Soil Survey of Scotland Scottish Peat Surveys (1964);
- Scottish Government Peat Landslide Hazard and Risk Assessments (2017);
- Scottish Government, Scottish Natural Heritage, SEPA (2017) Peatland Survey, Guidance on Developments on Peatland;
- The Scottish Government Scotland's Third National Planning Framework (2014);
- The Scottish Government Scottish Planning Policy (2014);
- Assessments by other EIA specialists (specifically hydrology and ecology for data on sensitive receptors); and
- Scotland's Environment Interactive Map.

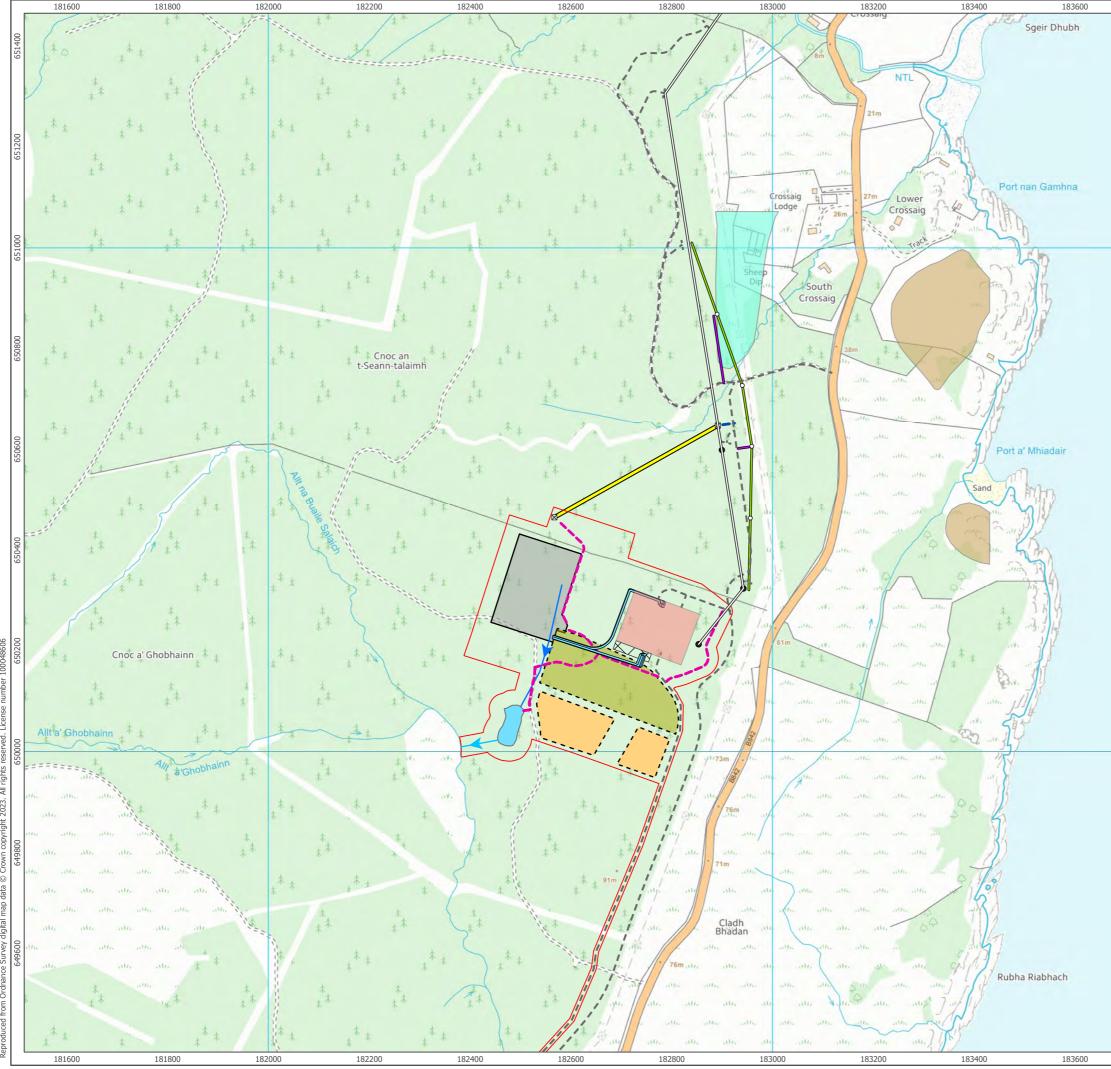


# **APPENDIX A - FIGURES**

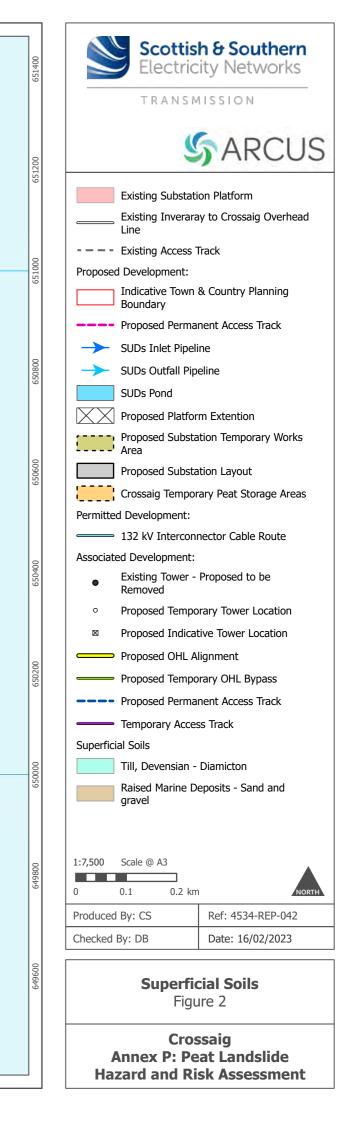


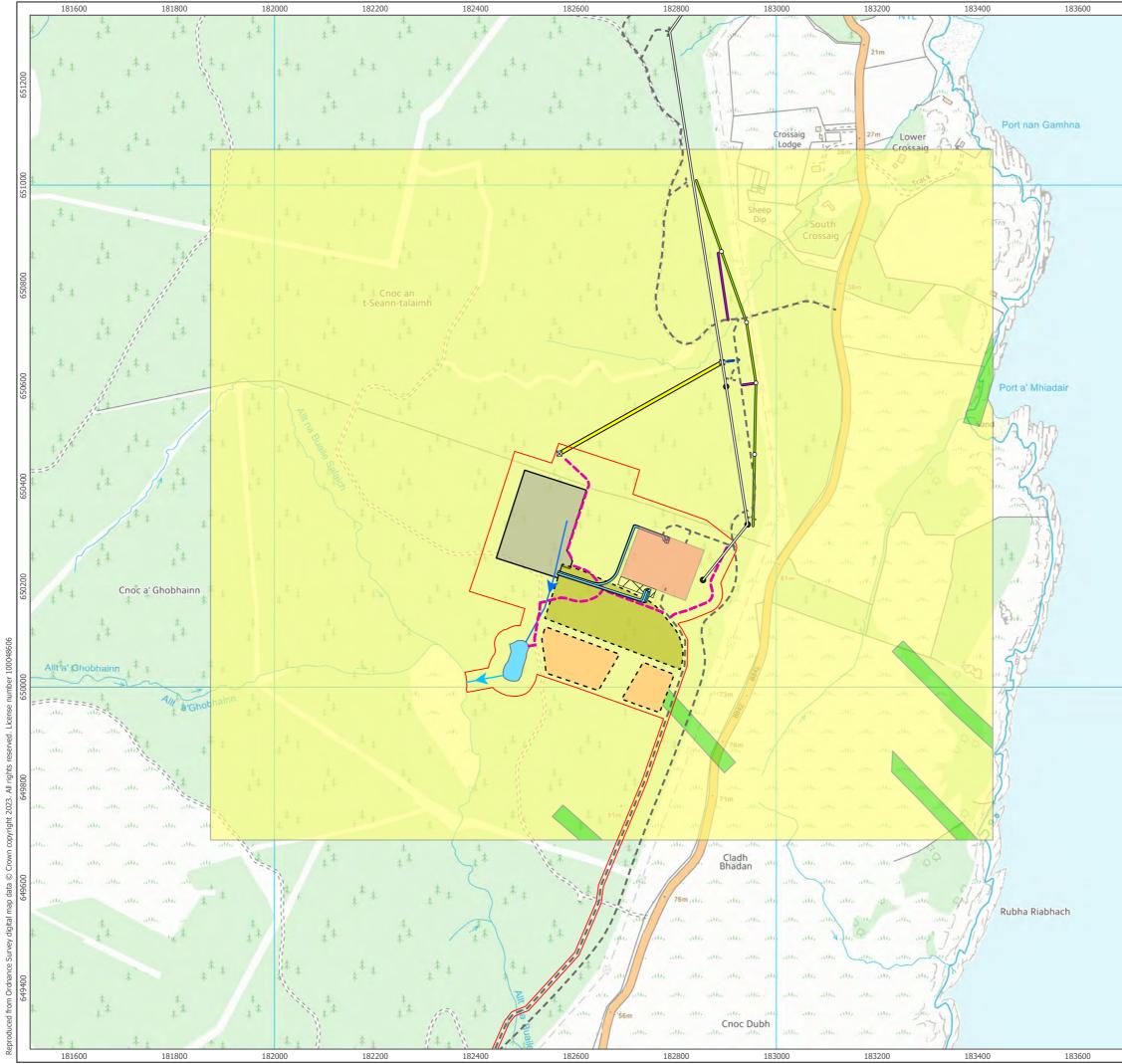
Y:\GIS\Engineering\Projects\4534 Argyll Substations\4534 Crossaig Reports.aprx\4534-REP-041 Fig01 Site Layout Plan

183400	Scottish & Southern Electricity Networks TRANSMISSION SARCUS
651000	Existing Substation Platform
	Existing Inveraray to Crossaig Overhead Line
	Existing Access Track
- 197	Proposed Development:
	Indicative Town & Country Planning Boundary
220800	Proposed Permanent Access Track
6	->> SUDs Inlet Pipeline
	->- SUDs Outfall Pipeline
	SUDs Pond
$\sim$	Proposed Platform Extention
	Proposed Substation Temporary Works Area
650600	Proposed Substation Layout
2	Crossaig Temporary Peat Storage Areas
Si	Permitted Development:
	— 132 kV Interconnector Cable Route
Title	Associated Development:
650400	<ul> <li>Existing Tower - Proposed to be Removed</li> </ul>
3	<ul> <li>Proposed Temporary Tower</li> <li>Location</li> </ul>
-	Proposed Indicative Tower Location
	Proposed OHL Alignment
	Proposed Temporary OHL Bypass
500	Proposed Permanent Access Track
650200	Temporary Access Track
	1:5,000 Scale @ A3
	0 0.1 0.2 km
174	Produced By: CS Ref: 4534-REP-041
-10 8	Checked By: DB Date: 16/02/2023
65000	<b>Site Layout Plan</b> Figure 1
183400	Crossaig Annex P: Peat Landslide Hazard and Risk Assessment

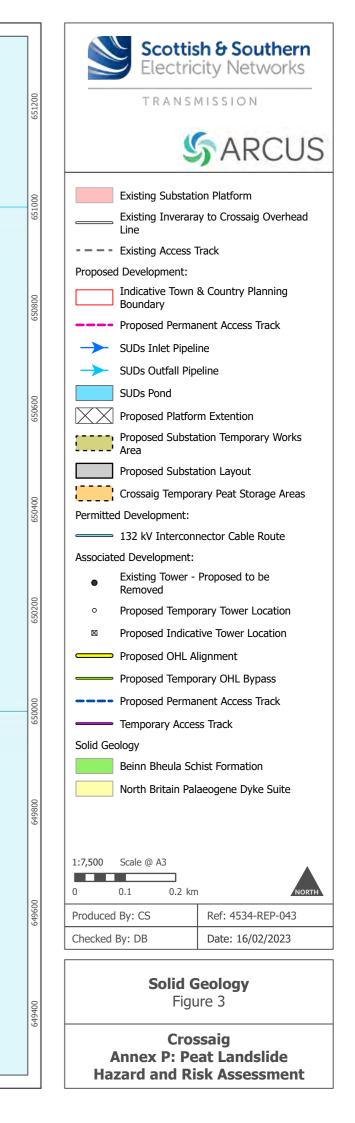


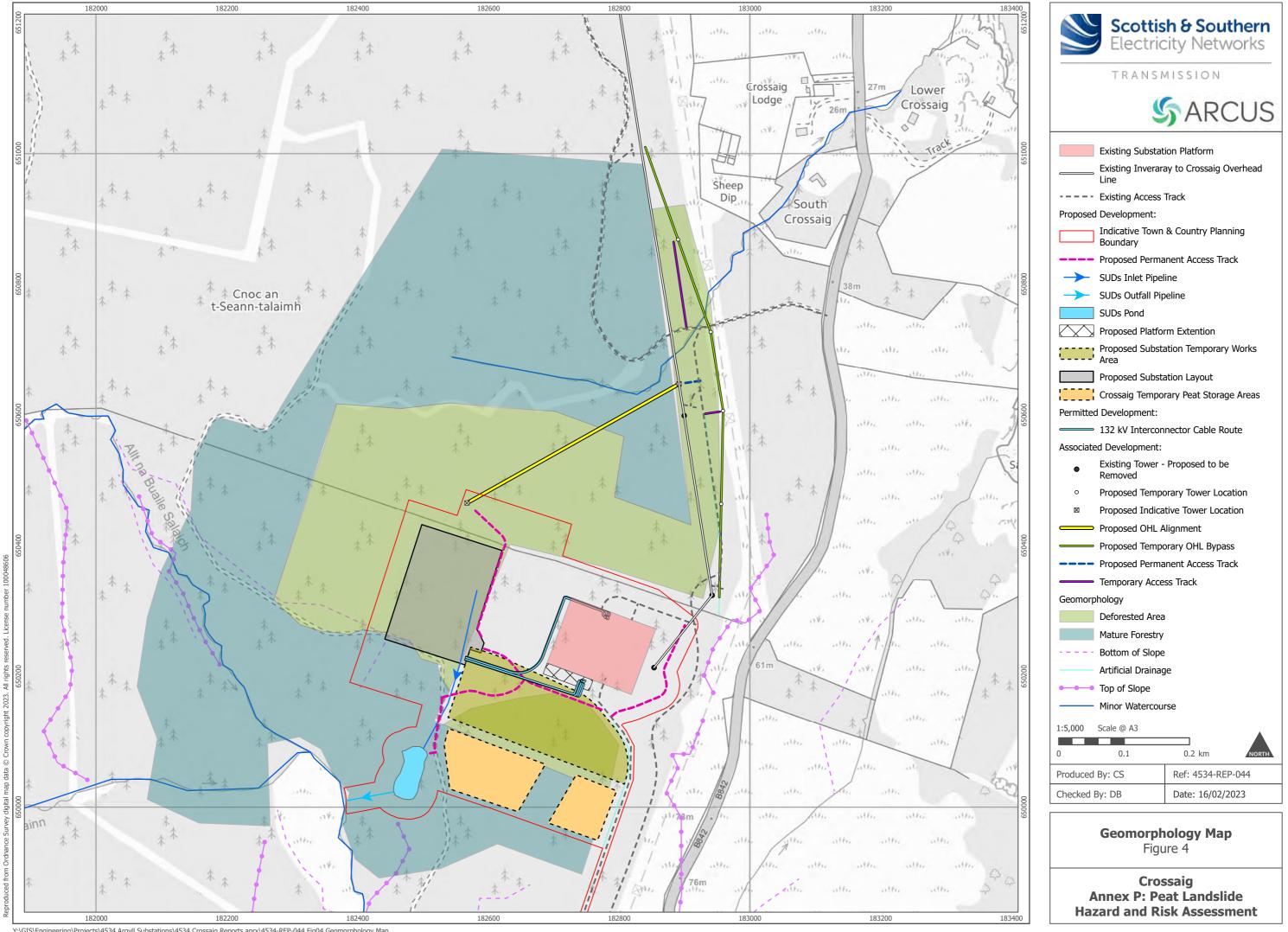
Y:\GIS\Engineering\Projects\4534 Argyll Substations\4534 Crossaig Reports.aprx\4534-REP-042 Fig02 Superficial Soils



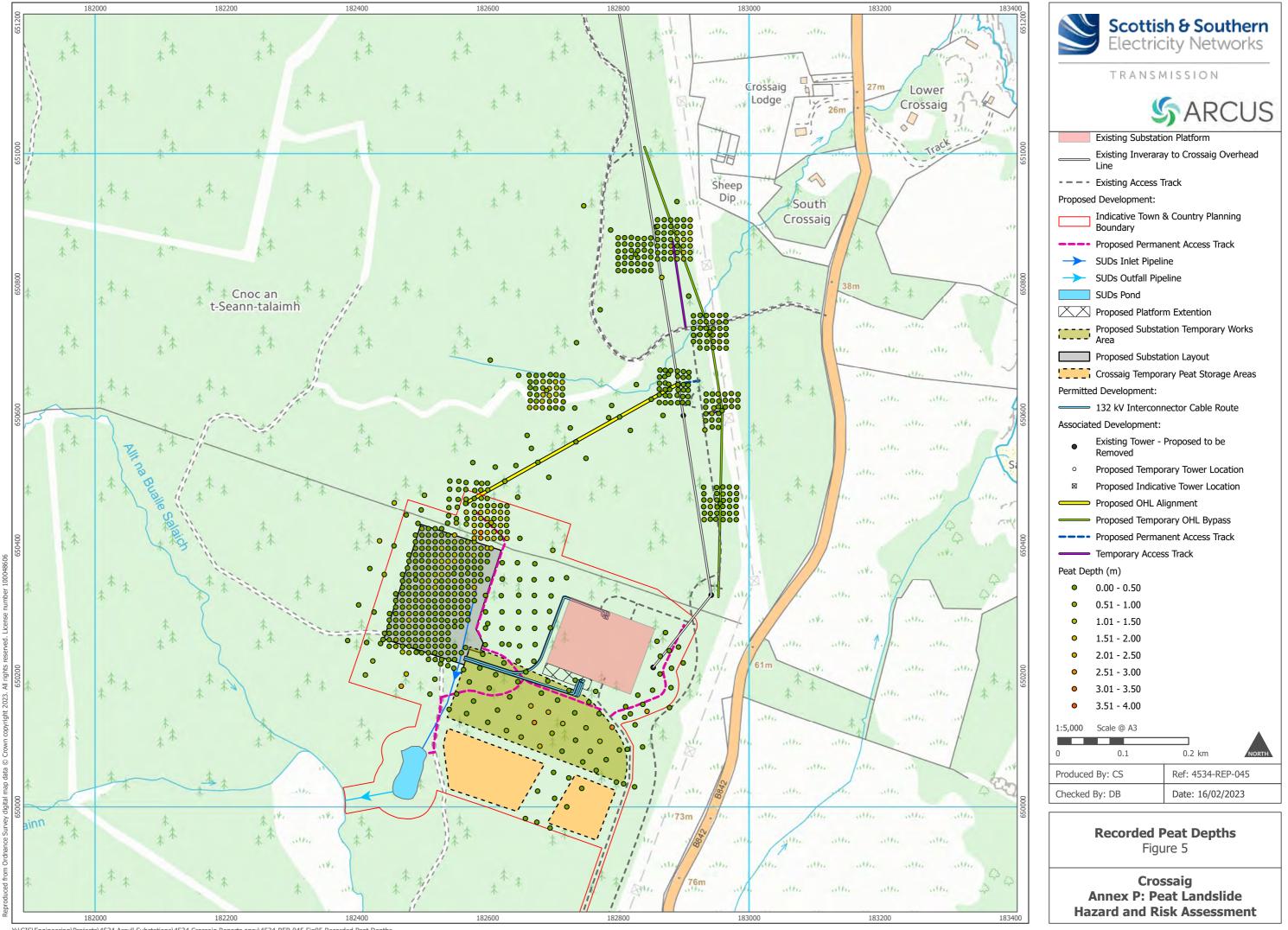


Y:\GIS\Engineering\Projects\4534 Argyll Substations\4534 Crossaig Reports.aprx\4534-REP-043 Fig03 Solid Geology

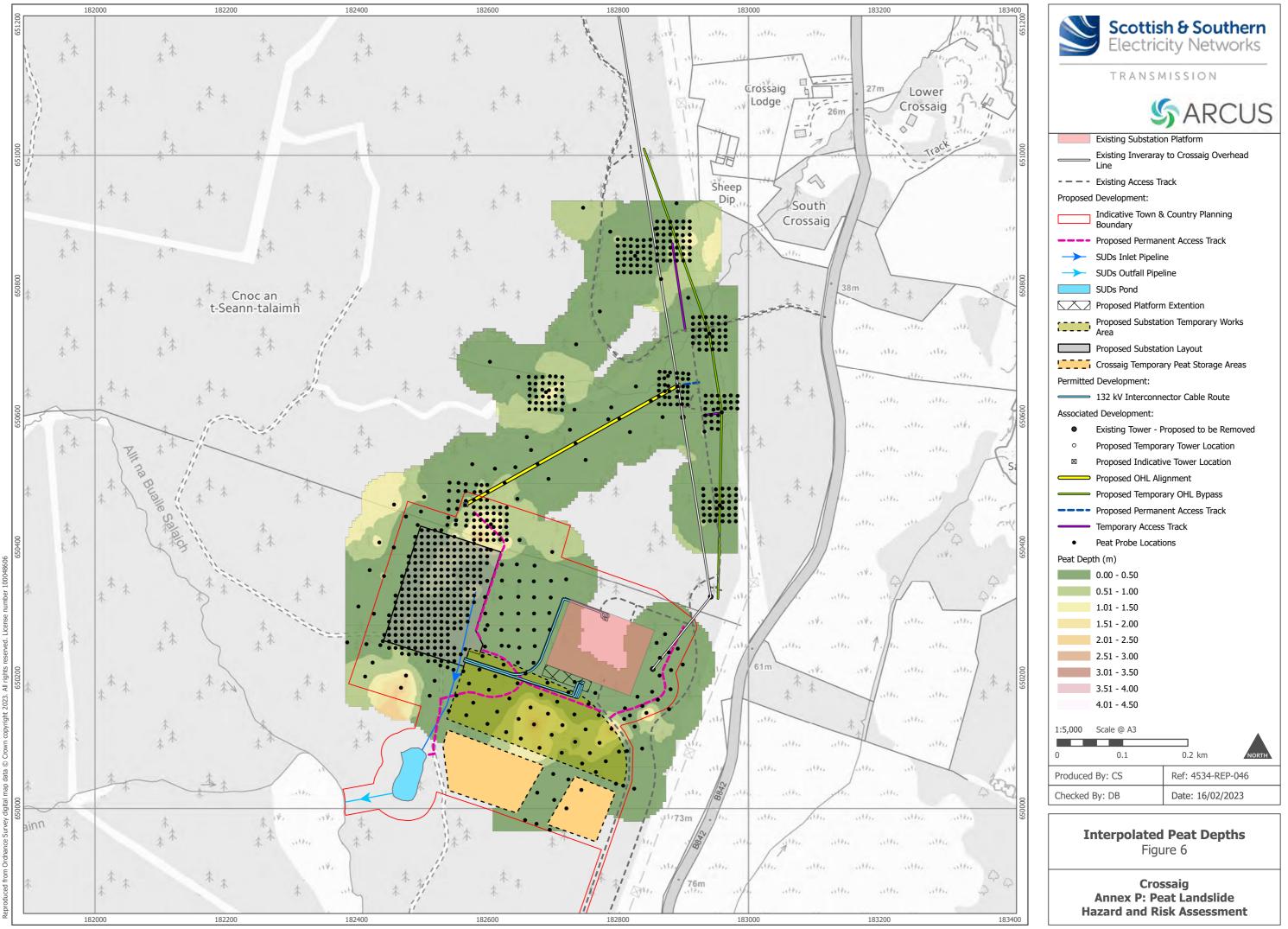




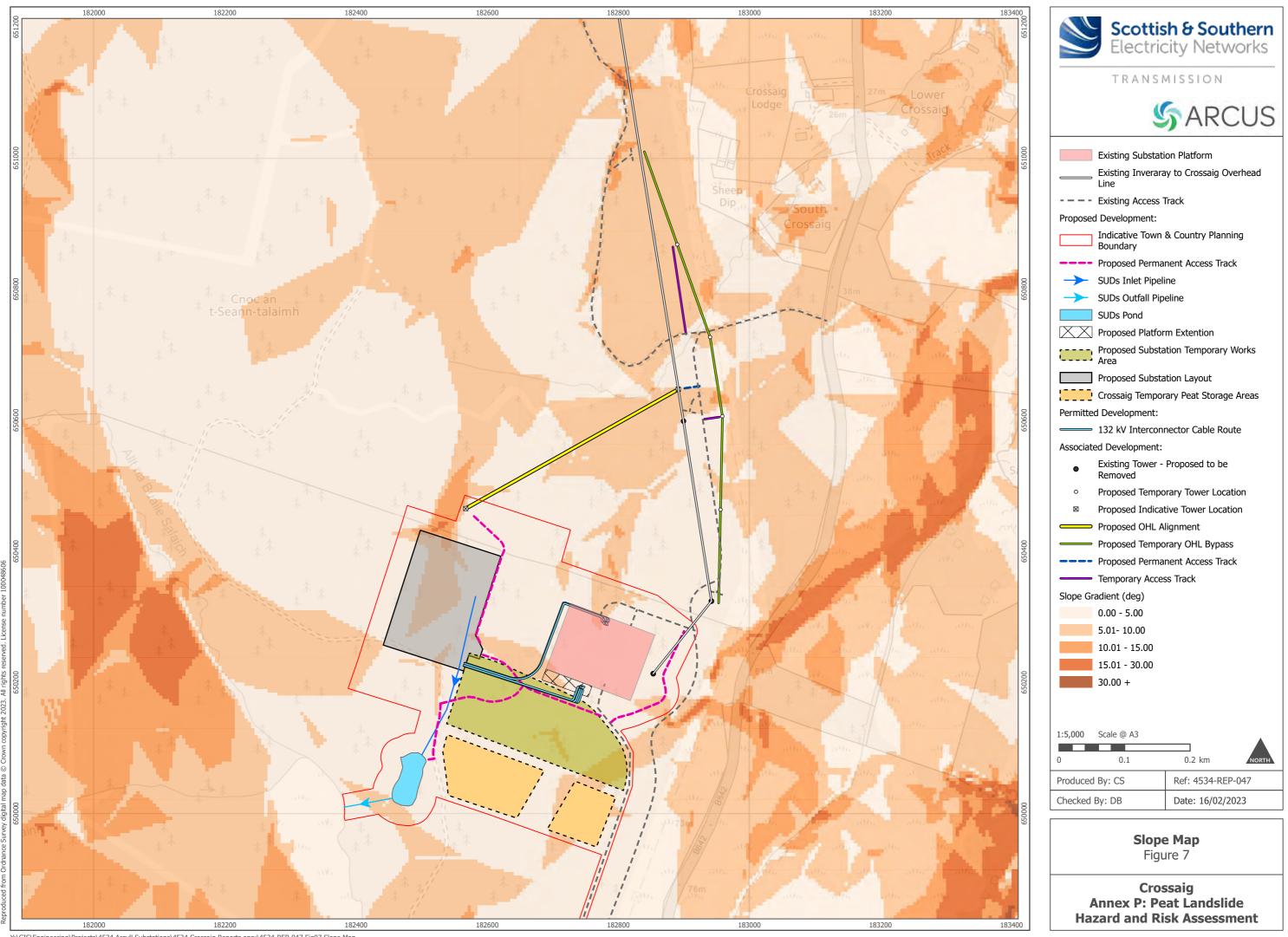
Y:\GIS\Engineering\Projects\4534 Argyll Substations\4534 Crossaig Reports.aprx\4534-REP-044 Fig04 Geomorphology Map



Y:\GIS\Engineering\Projects\4534 Argyll Substations\4534 Crossaig Reports.aprx\4534-REP-045 Fig05 Recorded Peat Depths



Y:\GIS\Engineering\Projects\4534 Argyll Substations\4534 Crossaig Reports.aprx\4534-REP-046 Fig06 Interpolated Peat Depths

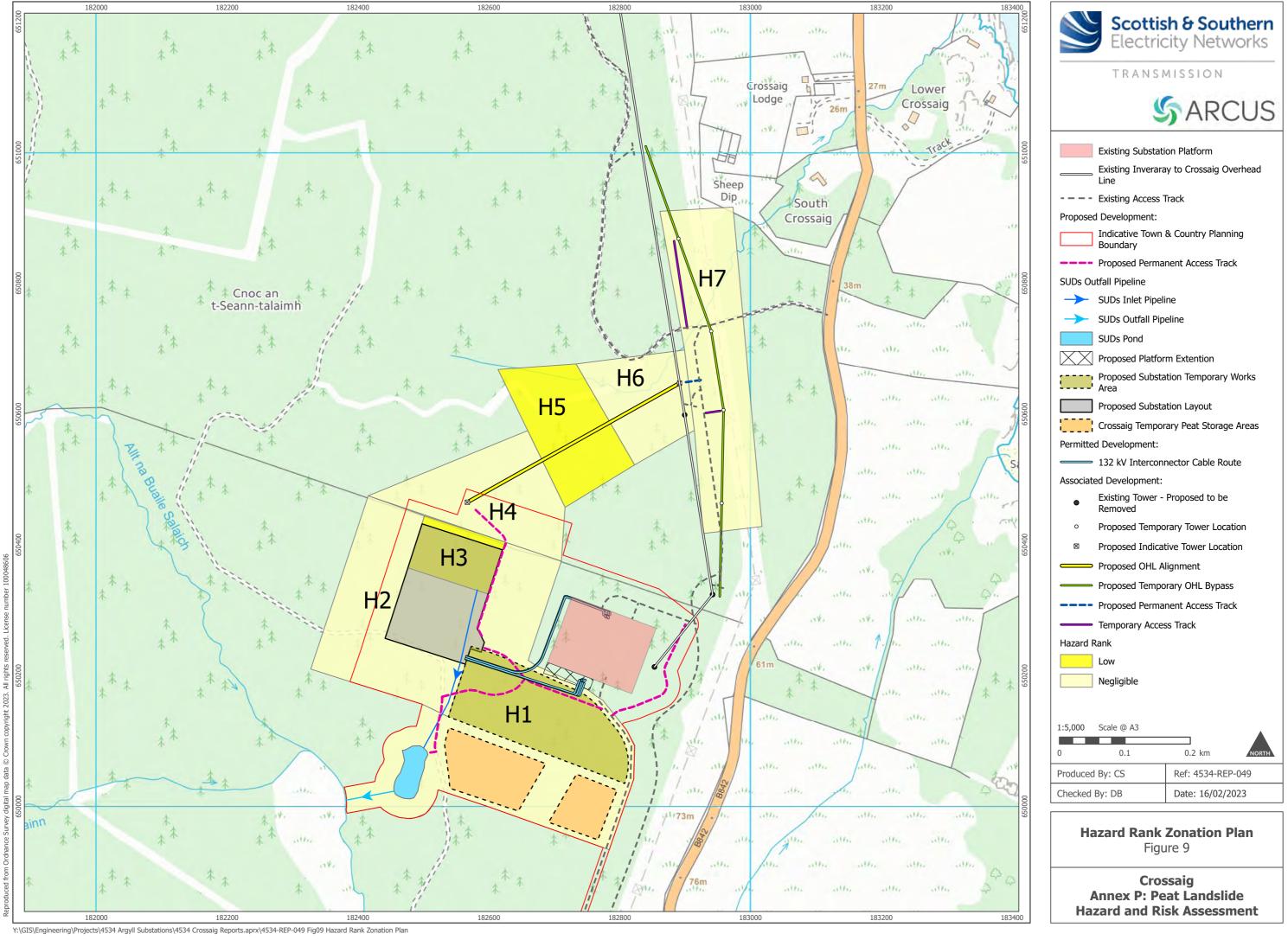


Y:\GIS\Engineering\Projects\4534 Argyll Substations\4534 Crossaig Reports.aprx\4534-REP-047 Fig07 Slope Map



Y:\GIS\Engineering\Projects\4534 Argyll Substations\4534 Crossaig Reports.aprx\4534-REP-048 Fig08 Factor of Safety Plan

183400	Scottish & Southern Electricity Networks
	\$ ARCUS
651000	Existing Substation Platform Existing Inveraray to Crossaig
	Overhead Line
	Existing Access Track
- 1 P.	Proposed Development:
	Indicative Town & Country Planning Boundary
650800	Proposed Permanent Access Track
65(	->- SUDs Inlet Pipeline
1	SUDs Outfall Pipeline
-	SUDs Pond
. 1	Proposed Platform Extention
_	Works Area
650600	Proposed Substation Layout
920	Areas
F	Permitted Development:
23	
	Associated Development:
anthe second	Existing Tower - Proposed to be     Removed
650400	<ul> <li>Proposed Temporary Tower</li> <li>Location</li> </ul>
3	Proposed Indicative Tower Location
	Proposed OHL Alignment
	Proposed Temporary OHL Bypass
	Proposed Permanent Access Track
	Temporary Access Track
650200	Factor of Safety
0	Low Risk 1:5,000 Scale @ A3
174	
20	Produced By: CS Ref: 4534-REP-048
650000	Checked By: DB Date: 16/02/2023
Q	Factor of Safety Plan Figure 8
183400	Crossaig Annex P: Peat Landslide Hazard and Risk Assessment





# **APPENDIX B - SITE PHOTOGRAPHS**

*Photograph 1: View north west from existing access track showing existing Crossaig Substation.* 



Photograph 2: Cutting for installation of drainage ditch showing ground conditions at existing access track.





*Photograph 3: View east showing current conditions of proposed Temporary Works Area* 



Photograph 4: Windblown tree at eastern edge of proposed substation area





*Photograph 5: Current conditions at proposed substation in area of forestry plantation* 



Photograph 6: Windblown trees in at proposed substation location





*Photograph 7: View north west of recently felled area north of the proposed substation* 



Photograph 8: View south east from northernmost temporary tower across felled area





Photograph 9: View north from northernmost permanent tower across felled area



*Photograph 10: View west from southernmost temporary tower of log piles and recently constructed track* 

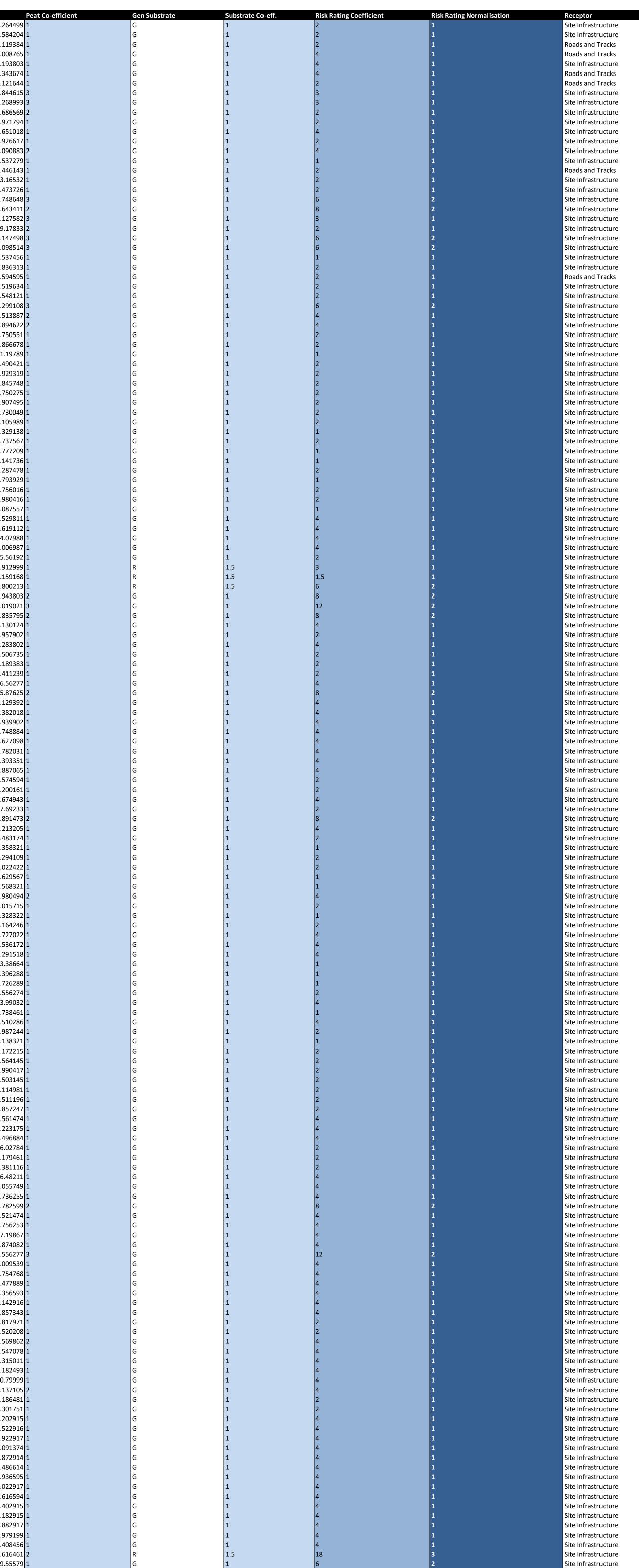




APPENDIX C – HAZARD RANK ASSESSMENT RECORDS

4534 - Argyll Substations - PLHRA - Tabulated Peat Probe Data - Crossaig

1 2 3 4	182808 182797 182825 182837	65003580.27449965003879.59420465003081.31938465009278.208765	3.442082 2 3.483088 2 2.854728 2 5.752233 4	0.0 0.0 0.2 0.2	. 79.584 81.119
5	182802 182814	650087 76.493803 650088 77.353674	7.346636 4 7.349225 4	0.3 0.02	3         76.193           5         77.343
7	182810	650137 74.621644	2.473116 2	0.5	71.844
8	182790	650122 74.544615	1.448394 1	2.7	
9	182772	650100 74.468993	1.42645 1	1.2	
10	182757	650085 74.386569	1.432718 1	0.7	73.686
11	182745	650069 74.371794	2.528519 2		73.971
12	182714	650085 72.051018	4.92011 4	0.4	72.926
13	182734	650102 73.326617	2.903196 2	0.4	
14	182750	650121 73.690883	2.248737 2	0.6	
15	182771	650143 73.837279	1.43606 1	0.3	73.537
16	182765	650177 73.456143	2.085929 2	0.02	73.446
17	182755	650160 73.17532	2.292666 2	0.02	. 72.473
18	182733	650144 72.483726	2.134081 2	0.02	
19	182715	650128 71.948648	2.597448 2	1.2	
20	182698	650113 70.543411	5.28134 4	0.9	69.643
21	182680	650093 70.827582	1.366475 1		69.127
22 23 24	182651 182672 182693	650107 70.17833 650129 71.147498 650145 71.698514	1.579188 1 2.336846 2 2.063882 2	1.6	68.147
25	182707	650163 71.637456	0.825452 1	0.1	. 71.537
26	182724	650178 72.846313	3.917573 2	0.01	. 72.836
27	182734	650194 73.604595	2.226678 2	0.0	. 72.519
28	182692	650192 72.619634	2.251287 2	0.1	
29	182682	650174 72.648121	2.255689 2	0.2	
30 31	182666 182648	650154 72.199108 650137 71.513887	2.327157 2 2.334099 2	1.9	70.299
32	182629	650117 70.694622	2.287221 2	0.8	70.750
33	182600	650130 71.050551	2.261375 2	0.3	
34	182568	650143 71.166678	2.083035 2	0.3	
35	182541	650149 71.29789	1.64992 1	0.2	71.19 <sup>-</sup>
36	182552	650173 71.990421	2.060105 2		71.490
37 38 39	182579 182615 182634	65016271.93931965014871.85574865016872.760275	2.084684 2 2.27471 2 2.286549 2	0.02 0.02 0.02	. 71.845
40 41	182602 182646	650182 72.917495 650192 73.740049	2.065268 2 2.300212 2	0.02	72.907
42	182659	650206 74.115989	3.328563 2	0.02	. 74.329
43	182625	650220 74.339138	1.16564 1	0.02	
44	182612	650202 73.747567	2.084688 2	0.02	
44 45 46	182588 182593	650213 73.787209 650233 74.151736	1.798176 1 0.934103 1	0.02	73.777
47 48 40	182563 182566 182572	650210 73.387478 650244 73.993929 650101 73.856016	2.05054 2 0.945201 1	0.1	73.793
49	182572	650191 72.856016	2.082598 2	0.1	72.980
50	182548	650212 73.280416	2.068705 2	0.3	
51	182539	650216 73.287557	1.817235 1	0.2	
52 53	182528 182520	650219 73.629811 650226 74.819112	6.399948 4 6.007652 4	0.1	74.619
54	182529	650235 74.37988	6.256231 4	0.3	75.006
55	182519	650236 75.306987	5.288048 4	0.3	
56	182509	650236 75.86192	2.354529 2	0.3	
57	182499	650236 76.012999	3.44562 2	0.1	. 76.159
58	182499	650245 76.259168	1.893194 1	0.2	
59	182491	650237 75.900213	4.761181 4	0.3	5 74.943
60	182480	650236 75.543803	5.035845 4	0.6	
61	182470	650237 75.419021	4.999892 4	1.4	
62	182460	650246 75.835795	4.784462 4	0.02	. 74.835
63	182470	650246 76.140124	4.935982 4		. 76.130
64	182480	650256 76.967902	2.257784 2	0.0	76.283
65	182480	650246 76.383802	4.566987 4	0.1	
66	182490	650246 76.516735	2.674941 2	0.0	
67	182479	650266 77.199383	3.968912 2	0.0	. 77.189
68	182470	650266 77.511239	3.606616 2		. 77.411
69	182470	650256 76.96277	4.039678 4	0.4	5 75.87
70	182460	650255 76.47625	4.711371 4	0.6	
71	182450	650246 75.329392	4.187316 4	0.2	
72	182436	650250 75.582018	5.056934 4	0.2	2 75.382
73	182440	650256 76.039902	5.02589 4		. 75.939
74	182450	650256 75.948884	4.266357 4	0.2	76.627
75	182450	650266 76.637098	4.108956 4	0.02	
76	182442	650266 76.792031	4.854788 4	0.02	
77	182450	650276 77.403351	4.547221 4	0.0	. 77.393
78	182450	650286 78.187065	4.725157 4	0.3	77.887
79	182460	650286 77.974594	3.846993 2	0.4	77.200
80	182460	650276 77.400161	3.815528 2	0.2	
81	182460	650266 76.974943	4.171287 4	0.3	
82	182470	650276 77.99233	3.749071 2	0.3	77.69
83	182480	650276 77.891473	5.150876 4		76.891
84	182490	650276 77.223205	5.014487 4	0.0	76.483
85	182489	650266 76.783174	2.828837 2	0.3	
86	182490	650256 76.658321	1.936274 1	0.3	
87	182499	650266 76.394109	2.378766 2	0.1	76.294
88	182499	650255 76.322422	2.005716 2	0.3	76.022
89	182509	650246 75.929567	1.993913 1	0.3	75.568
90	182510	650256 75.968321	1.980732 1	0.4	
91	182520	650266 75.680494	2.082422 2	0.7	
92	182510	650266 76.025715	2.182919 2	0.0	76.015
93	182520	650256 75.628322	1.983517 1	0.3	75.328
94	182520	650246 75.564246	2.581505 2	0.4	74.727
95	182530	650246 75.027022	5.206643 4	0.3	
96	182530	650226 73.736172	5.117649 4	0.2	
97	182510	650226 75.391518	4.183315 4	0.1	. 75.291
98	182540	650225 73.48664	1.120443 1		. 73.38
99	182550	650226 73.596288	0.977292 1	0.2	73.726
100	182560	650236 73.826289	0.940687 1	0.2	
101	182540	650236 73.656274	2.495786 2	0.2	
102	182540	650246 74.09032	4.864349 4	0.1	. 73.99
103	182550	650246 73.838461	1.084682 1		. 73.738
104	182540	650256 74.710286	5.081712 4	0.2	74.987
105	182530	650256 75.287244	2.537759 2	0.3	
106	182530	650266 75.338321	1.995989 1	0.2	
107	182530	650276 75.472215	2.694202 2	0.3	75.172
108	182520	650275 75.864145	2.89738 2	0.3	
109	182539	650276 75.090417	2.504994 2	0.1	5 74.503
110	182539	650266 75.003145	2.499427 2	0.5	
111	182539	650285 75.414981	3.069266 2	0.3	
112	182530	650286 75.811196	3.076328 2	0.3	8 75.511
113	182530	650296 76.157247	3.652703 2	0.3	8 75.857
114	182530	650306 76.761474	5.556186 4	0.2	77.223
115	182520	650306 77.423175	5.86219 4	0.2	
116	182520	650296 76.696884	5.045239 4	0.2	
113 117 118	182520 182510	650286 76.22784 650276 76.279461	3.265554 2 3.040879 2	0.2	76.02
119	182500	650275 76.681116	3.623546 2	0.3	76.48
120	182510	650286 76.68211	4.386345 4	0.2	
121	182510	650296 77.355749	5.79511 4	0.3	
121 122 123	182510 182500	650306 78.136255 650316 79.582599	5.875601 4 5.873362 4	0.4	77.736
124	182500	650306 78.821474	5.879881 4	0.3	77.756
125	182500	650296 78.056253	5.875598 4	0.3	
126	182500	650286 77.29867	5.554653 4	0.1	
120 127 128	182300 182490 182480	650286 77.974082 650286 78.656277	5.864408 4 4.521293 4	0.1	. 77.874
129 130	182469 182450	650286 78.409539 650296 78.954768	4.075762 4 4.759698 4	0.4	78.754
131	182460	650296 78.677889	4.342659 4	0.2	79.356
132	182460	650306 79.456593	4.740178 4	0.2	
133	182460	650316 80.242916	4.794414 4	0.2	
134 135	182470 182470	650316 79.957343 650306 79.317971	4.07954 4 3.827641 2	0.1	78.817
136	182469	650296 78.820208	3.899414 2	0.3	78.569
137	182480	650296 79.269862	3.848375 2	0.7	
138	182490	650296 78.747078	5.876797 4	0.2	
139	182490	650306 79.515011	5.69646 4	0.2	2 79.315
140	182490	650316 80.282493	5.117588 4		. 80.182
141	182489	650325 80.99999	4.263953 4	0.2	79.137
142	182480	650305 79.837105	3.824068 2	0.7	
143	182480	650316 80.286481	3.745844 2	0.2	
144	182479	650326 80.701751	3.730707 2	0.4	80.301
145	182470	650336 81.502915	4.794914 4	0.3	8 81.202
146 147 148	182470 182460 182470	650326 80.722916 650326 81.022917 650346 82 291374	4.550351 4 4.806222 4 4.818793 4	0.2	80.922
148	182470	650346 82.291374	4.818793 4	0.2	82.872
149	182470	650356 83.072914	4.786724 4	0.2	
150	182477	650365 83.586614	4.787597 4	0.2	
151	182480	650376 84.336595	4.826659 4	0.4	83.936
152	182480	650386 85.122917	4.794432 4	0.2	85.022
153	182490	650386 84.816594	4.815329 4	0.2	85.402
154	182490	650396 85.602915	4.794426 4	0.2	
155	182490	650406 86.382915	4.806213 4	0.2	
156	182500	650406 86.082917	4.7359 4	0.2	85.882
157	182490	650416 87.179199	5.156109 4	2.0	
158	182500	650416 86.908456	5.639814 4	2.0	



	Recentor Co. off	7 Bosontor	Distance	acomtar Dist Ca off	7 Difference (remove =/ )	Percenter clouation Co off	Impact Da
	Receptor Co-eff. 3 3	Z Receptor 80.161298 79.54744	Distance R 0 4 1.495255 4			1	Impact Ra 12 12
	3	80.933442 78.313435	6.389245 4 15.976199 3		0.385942 -0.10467	1	12 9
	3	76.529624 77.639626	0 <mark>4</mark> 2.875036 4		-0.035821 -0.285952		12 12
:	3 3	74.066825 74.552259	10.477288 3 0 4		0.554819 -0.007644	1	9 12
	3	74.493381 74.36822	0404		-0.024388 0.018349	1	12 12
	3	74.347391 72.101048 73.337211	0 4 0 4 0 4		0.024403 -0.05003 -0.010594	1	12 12 12
	3	73.687237 73.826648	0404		-0.010394 0.003646 0.010631	1	12 12 12
	3	73.490369 73.170372	1.002574 4 0 4		-0.034226 0.004948	1	12 12 12
:	3 3	72.452089 71.929248	0 4 0 4		0.031637 0.0194		12 12
:	3 3	70.488735 70.823879	0 4 0 4		0.054676 0.003703	1	12 12
	3	70.200695 71.170224	0404		-0.022365 -0.022726	1	12 12
	3	71.718003 71.647876 72.825909	0 4 0 4 0 4		-0.019489 -0.01042 0.020404	1	12 12 12
	3	73.917052 72.628901	8.211862 4 0 4		-0.312457 -0.009267	1	12 12 12
	3	72.628001 72.158405	0 4 0 4		0.02012 0.040703		12 12
:	3 3	71.534261 70.720441	0 4 0 4		-0.020374 -0.025819	1	12 12
	3	71.046918 71.193028	0404		0.003633 -0.02635	1	12 12
	3	71.30944 72.01103 71.927036	0 4 0 4 0 4		-0.01155 -0.020609 0.012283	1	12 12 12
	3	71.828559 72.72444	0 4 0 4		0.027189 0.035835	1	12 12 12
	3	72.913024 73.730694	0 4 0 4		0.004471 0.009355	1	12 12
3	3 3	74.098582 74.324518	0 4 0 4		0.017407 0.01462	1	12 12
	3	73.723028 73.815568	0404		0.024539 -0.028359	1	12 12
	3	74.150997 73.365029 73.992443	0 4 0 4 0 4		0.000739 0.022449 0.001486	1	12 12 12
	3	72.873041 73.255025	0404		-0.017025 0.025391	1	12 12 12
:	3	73.263039 73.603231	0 4 0 4		0.024518 0.02658	1	12 12
3	3 3	74.70563 74.44169	0 4 0 4		0.113482 -0.06181	1	12 12
	3	75.371691 75.893257	0404		-0.064704 -0.031337	1	12 12
	3	75.971051 76.293252 75.960701	0 4 0 4 0 4		0.041948 -0.034084 -0.060488	1	12 12 12
	3	75.546619 75.474621	0 4 0 4		-0.002816 -0.0556	1	12 12 12
	3	75.859124 76.144299	0 4 0 4		-0.023329 -0.004175	1	12 12
:	3 3	76.941924 76.38662	0 4 0 4		0.025978 -0.002818	1	12 12
	3 3	76.496029 77.240696	0404		0.020706 -0.041313	1	12 12
	3	77.527802 76.969656 76.512478	0 4 0 4 0 4		-0.016563 -0.006886 -0.036228	1	12 12 12
	3	75.353202 75.519981	0404		-0.02381 0.062037	1	12 12 12
	3	75.965992 75.967653	0 4 0 4		0.07391 -0.018769	1	12 12
:	3 3	76.605504 76.782678	0 4 0 4		0.031594 0.009353	1	12 12
	3 3	77.358662 78.14284	0404		0.044689 0.044225	1	12 12
	3	77.970215 77.444925 77.020002	0404		0.004379 -0.044764	1	12 12 12
	3	77.020092 78.036588 77.809097	0 4 0 4 0 4		-0.045149 -0.044258 0.082376	1	12 12 12
	3	77.151903 76.8026	04		0.071302 -0.019426	1	12 12 12
:	3 3	76.625254 76.423023	0 4 0 4		0.033067 -0.028914		12 12
	3	76.346594 75.952084	0404		-0.024172 -0.022517	1	12 12
	3	75.935254 75.64692 75.991757	0 4 0 4 0 4		0.033067 0.033574 0.033958	1	12 12 12
	3	75.595256 75.536922	0404		0.033066 0.027324	1	12 12 12
:	3 3	74.899703 73.646356	0 4 0 4		0.127319 0.089816	1	12 12
:	3 3	75.391545 73.494987	0 4 0 4		-2.7E-05 -0.008347	1	12 12
	3	73.603318 73.833319 73.645163	0 4 0 4 0 4		-0.00703 -0.00703 0.011111	1	12 12 12
	3	74.002368 73.844985	0404		0.087952 -0.006524	1	12 12 12
	3	74.609702 75.251756	0 4 0 4		0.100584 0.035488	1	12 12
:	3 3	75.305255 75.430427	0 4 0 4		0.033066 0.041788		12 12
	3	75.826196 75.125135	04		0.037949 -0.034718	1	12 12
	3	75.033257 75.443357 75.766198	0 4 0 4 0 4		-0.030112 -0.028376 0.044998	1	12 12 12
	3	76.116197 76.679097	04		0.04105 0.082377	1	12 12 12
	3	77.366776 76.624224	0 4 0 4		0.056399 0.07266	1 1	12 12
	3 3	76.176196 76.236199	0404		0.051644 0.043262	1	12 12
	5 3 3	76.64453 76.611731 77.286775	0 4 0 4 0 4		0.036586 0.070379 0.068974	1	12 12 12
	3	78.054264 79.506776	0404		0.081991 0.075823	1	12 12 12
:	3	78.739097 77.974262	0 4 0 4		0.082377 0.081991	1	12 12
:	3 3	77.206777 77.892596	0 4 0 4		0.091893 0.081486		12 12
	3	78.576776 78.347252	0404		0.079501 0.062287	1	12 12
	3	78.922839 78.626827 79.40915	0 4 0 4 0 4		0.031929 0.051062 0.047443	1	12 12 12
	3	80.196829 79.924325	0404		0.047443 0.046087 0.033018	1	12 12 12
	3	79.345099 78.771762	0 4 0 4		-0.027128 0.048446	1	12 12 12
	3	79.244987 78.659097 70.426775	0404		0.024875 0.087981	1	12 12
	3	79.426775 80.194263 81.06488	0 4 0 4 0 4		0.088236 0.08823 -0.06489	1	12 12 12
	3	81.06488 79.868902 80.332603	0 4 0 4 0 4		-0.06489 -0.031797 -0.046122	1	12 12 12
	3	80.641761 81.456827	0 4 0 4		0.05999 0.046088	1	12 12 12
	3	80.676828 80.97683	0 4 0 4		0.046088 0.046087	1 1	12 12
	5 3 3	82.244314 83.026826 83.62683	0404		0.04706 0.046088 -0.040216	1	12 12 12
	3	83.62683 84.28915 85.076829	0 4 0 4 0 4		-0.040216 0.047445 0.046088	1	12 12 12
	3 3 3	85.076829 84.76915 85.556828	0 4 0 4 0 4		0.046088 0.047444 0.046087	1	12 12 12
		86.336828 86.036828	0 4		0.046087 0.046089	1 1	12 12
	3	87.134815 86.862252	0404		0.044384 0.046204 0.051687	1	12 12
	3	88.164774 89.340409	0 4 2.489247 4		0.051687 0.415381		12 12

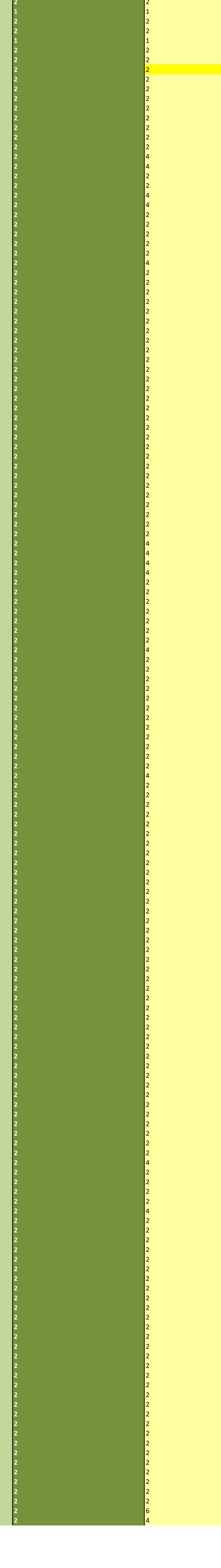


 1 TO 4
 Negligible

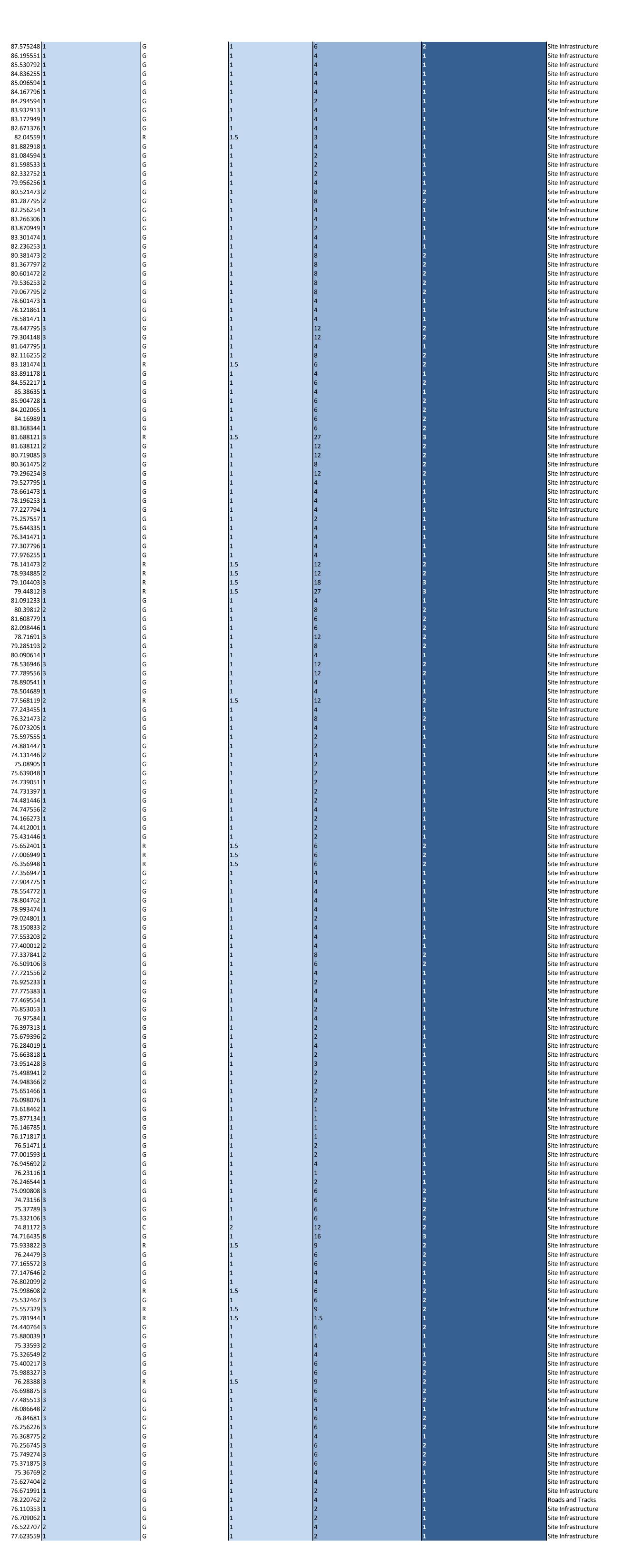
 5 TO10
 Low

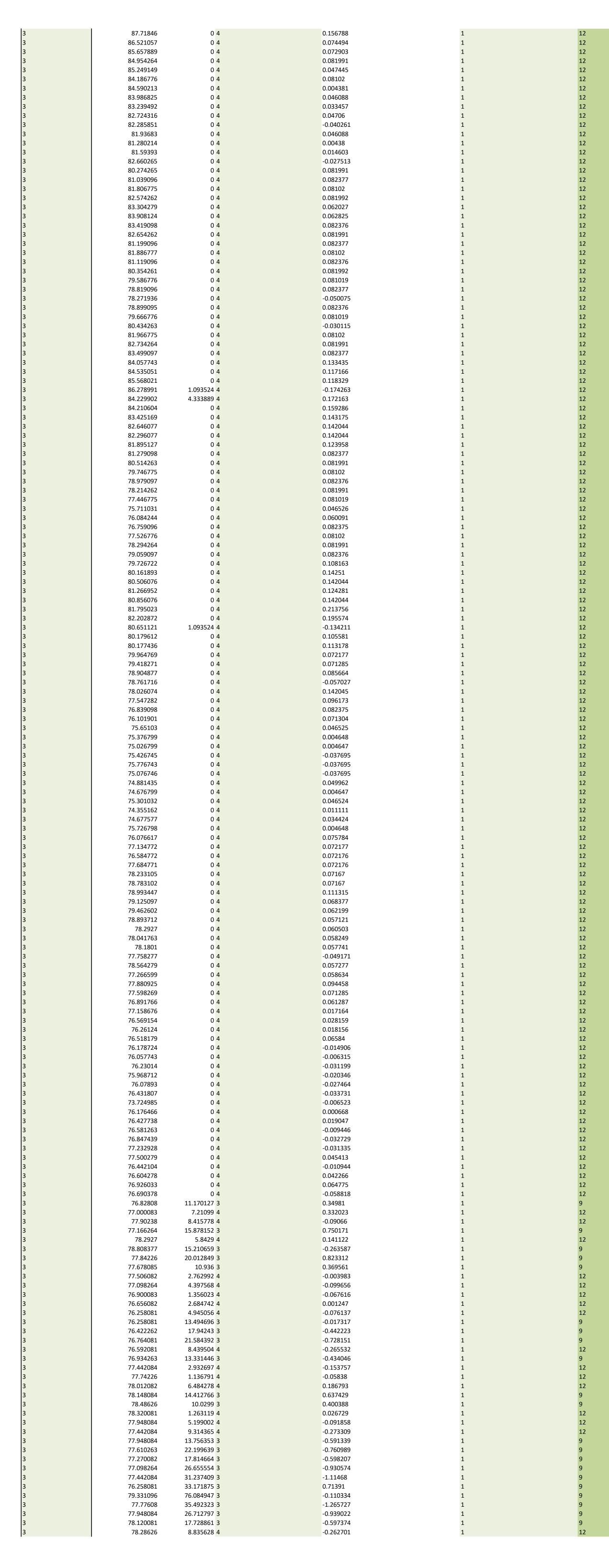
 11 TO 16
 Medium

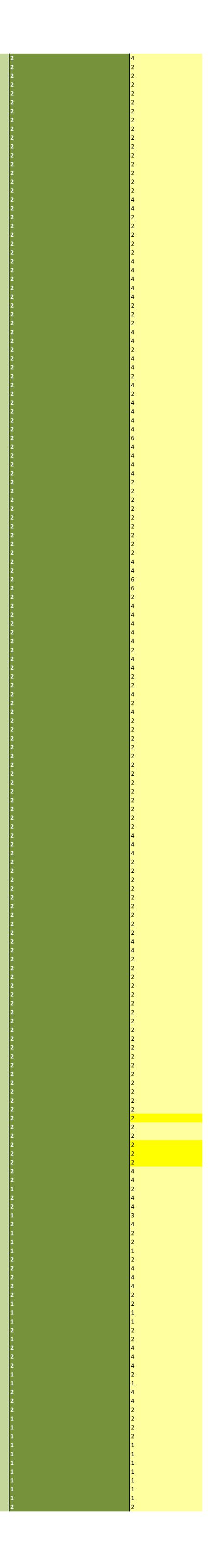
 17 TO 25
 High



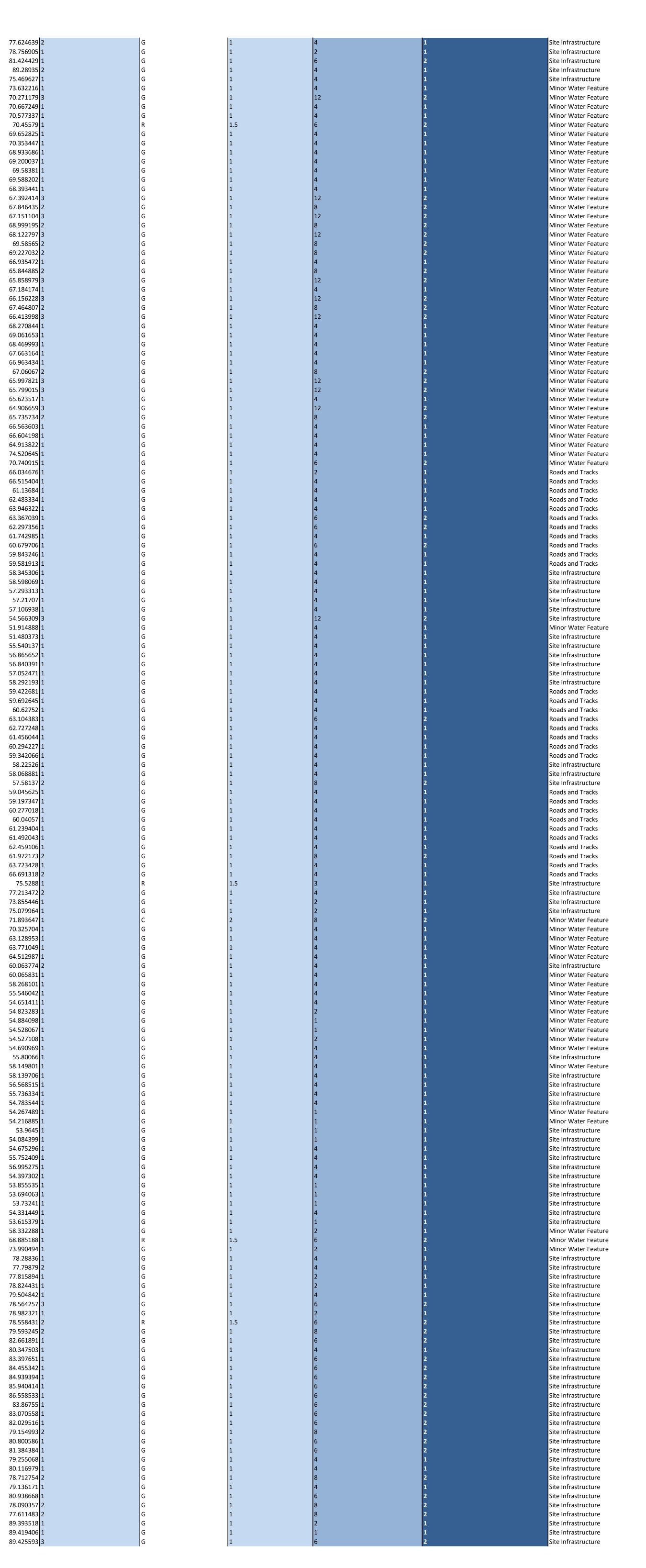
161	182510	650426 87.875248	11.1294 6	0.3
162	182510	650416 86.595551	6.626411 4	0.4
163	182510	650406 85.730792	5.631876 4	0.2
164	182510	650396 85.036255	5.218139 4	0.2
165	182500	650396 85.296594	4.607984 4	0.2
166	182510	650386 84.267796	5.413129 4	0.1
167	182500	650386 84.594594	3.963624 2	0.3
168	182490	650376 84.032913	4.546326 4	0.1
169	182490	650366 83.272949	4.076675 4	0.1
170	182480	650356 82.771376	4.726049 4	0.1
171	182490	650347 82.24559	3.420725 2	0.2
172	182480	650346 81.982918	4.369433 4	0.1
173	182480	650336 81.284594	3.840656 2	0.2
174	182490	650336 81.608533	3.81834 2	0.01
175	182490	650356 82.632752	3.657716 2	0.3
176	182500	650326 80.356256	5.875595 4	0.4
177	182500	650336 81.121473	5.879885 4	0.6
178	182500	650346 81.887795	5.545061 4	0.6
179	182500	650356 82.656254	4.949722 4	0.4
180	182500	650366 83.366306	4.149635 4	0.1
181	182499	650376 83.970949	3.890085 2	0.1
182	182510	650376 83.501474	5.865155 4	0.2
183	182510	650366 82.736253	5.875598 4	0.5
184	182520	650356 81.281473	5.879886 4	0.9
185	182510	650356 81.967797	5.873394 4	0.6
186	182510	650346 81.201472	5.879879 4	0.6
187	182510	650336 80.436253	5.875606 4	0.9
188	182510	650326 79.667795	5.873389 4	0.6
189	182510	650316 78.901473	5.879883 4	0.3
190	182519	650315 78.221861	5.875413 4	0.1
191	182520	650326 78.981471	5.879876 4	0.4
192	182520	650336 79.747795	5.873394 4	1.3
193	182521	650345 80.404148	5.879207 4	1.1
194	182520	650366 82.047795	5.873397 4	0.4
195	182520	650376 82.816255	5.873312 4	0.7
196	182520	650386 83.581474	6.19082 4	0.4
197	182520	650396 84.191178	7.274456 4	0.3
198	182520	650406 84.652217	8.352255 6	0.1
199	182520	650416 85.68635	7.557128 4	0.3
200	182520	650426 86.104728	11.929178 6	0.2
201	182530	650426 84.402065	10.650164 6	0.2
202	182530	650416 84.36989	9.277375 6	0.2
203	182530	650406 83.568344	9.84806 6	0.2
204	182530	650396 82.788121	8.355026 6	1.1
205	182530	650386 82.438121	8.15127 6	0.8
206	182530	650376 82.019085	7.042154 4	1.3
207	182530	650366 81.361475	6.08097 4	1
208	182530	650356 80.596254	5.873743 4	1.3
209	182530	650346 79.827795	5.873391 4	0.3
210	182530	650336 79.061473	5.879879 4	0.4
211	182530	650326 78.296253	5.875606 4	0.1
212	182530	650316 77.527794	5.873399 4	0.3
213	182540	650296 75.757557	3.102645 2	0.5
214	182540	650306 76.144335	4.318731 4	0.5
215	182540	650316 76.841471	5.801514 4	0.5
216	182540	650326 77.607796	5.873394 4	0.3
217	182540	650336 78.376255	5.875608 4	0.4
218	182540	650346 79.141473	5.981071 4	1
219	182540	650356 79.834885	6.763997 4	0.9
220	182540	650366 80.304403	7.93865 4	1.2
221	182540	650376 80.64812	8.170426 6	1.2
222	182540 182540	650396 81.391233	7.679898 4 7.750014 4	0.3
223 224	182540	650386 80.99812 650406 82.008779	11.041999 6	0.6 0.4
225	182540	650416 82.398446	11.681549 6	0.3
226	182550	650416 80.51691	7.739468 4	1.8
227	182550	650406 80.285193	7.094434 4	1
228	182550	650396 80.290614	6.319539 4	0.2
229	182550	650386 80.036946	5.20056 4	1.5
230	182550	650376 79.489556	5.4859 4	1.7
231	182550	650366 78.990541	6.117413 4	0.1
232	182549	650357 78.704689	7.256363 4	0.2
233	182550	650346 78.168119	7.071894 4	0.6
234	182550	650336 77.643455	6.363213 4	0.4
235 236	182550 182550 182550	650326 76.921473 650316 76.173205	5.937194 4 5.014497 4	0.6
237	182550	650306 75.697555	3.260475 2	0.1
238	182560	650306 75.381447	2.369396 2	0.5
239	182560	650296 75.031446	2.369395 2	0.9
240	182570	650296 75.38905	3.445962 2	0.3
241	182570	650306 75.739048	3.445982 2	0.1
242	182570	650286 75.039051	3.420595 2	0.3
243	182550	650284 74.931397	3.009151 2	0.2
244	182560	650286 74.681446	2.341612 2	0.2
245	182550	650296 75.347556	3.08566 2	0.6
246	182560	650276 74.366273	2.035209 2	0.2
247	182550	650276 74.712001	2.628877 2	0.3
248	182560	650316 75.731446	2.586405 2	0.3
249	182560	650326 76.152401	4.229405 4	0.5
250 251	182560 182560 182560	650346 77.206949 650336 76.656948	4.973589 4 5.312085 4	0.2
252	182560	650356 77.756947	4.797563 4	0.4
253	182560	650366 78.304775	4.802002 4	0.4
254	182560	650376 78.854772	4.995818 4	0.3
255	182560	650386 79.104762	5.817491 4	0.3
256	182560	650396 79.193474	4.835947 4	0.2
257	182560	650406 79.524801	3.793413 2	0.5
258	182570	650406 78.950833	3.525406 2	0.8
259	182580	650406 78.353203	3.575772 2	0.8
260	182580	650396 78.100012	3.685322 2	0.7
261	182570	650386 78.237841	4.06151 4	0.9
262	182579	650385 77.709106	3.734793 2	1.2
263	182570	650396 78.621556	3.731535 2	0.9
264	182580	650376 77.325233	3.754224 2	0.4
265	182570	650376 77.975383	4.991156 4	0.2
266	182570	650366 77.669554	4.8386 4	0.2
267	182580	650366 76.953053	3.737163 2	0.1
268	182570	650357 77.17584	4.715417 4	
269	182580	650356 76.597313	2.812236 2	0.2
270	182580	650346 76.279396	1.945115 1	0.6
271	182570	650346 76.584019	4.037341 4	0.3
272	182570	650337 76.163818	2.699623 2	0.5
273	182580	650336 76.051428	0.9508 1	2.1
274	182580	650326 76.198941	1.930478 1	0.7
275	182570	650326 75.948366	1.156816 1	1
276	182570	650316 76.051466	2.400118 2	0.4
277	182580	650316 76.398076	2.116578 2	0.3
278	182550	650236 73.718462	0.930606 1	0.1
279	182590	650346 76.177134	1.043157 1	0.3
280	182590	650356 76.446785	1.552465 1	0.3
281	182589	650365 76.571817	1.487892 1	
281 282 283	182589 182589 182589	650376 76.81471 650386 77.201593	3.344499 2 3.742308 2	0.4 0.3 0.2
284	182590	650396 77.545692	3.645261 2	0.6
285	182599	650376 76.43116	1.401373 1	0.2
286	182600	650386 76.646544	3.238367 2	0.4
287	182600	650396 76.990808	3.538762 2	1.9
288	182605	650395 76.63156	3.122194 2	1.9
289	182600	650411 77.17789	3.410258 2	1.8
290	182599	650420 77.332106	3.200317 2	2
291	182590	650411 77.81172	3.658501 2	3
292	182590	650420 77.916435	3.631177 2	3.2
293	182580	650411 78.433822	3.587606 2	2.5
294	182580	650421 78.54479	3.657848 2	2.3
295	182580	650431 78.665572	3.666901 2	1.5
296	182590	650431 78.047646	3.479123 2	0.9
297	182600	650431 77.502099	3.059843 2	0.7
298	182610	650431 76.998608	3.040305 2	1
299 300	182610	650421 76.832467 650411 76.657329	3.040572 2	1.3
301	182610 182620 182630	650411 76.181944	3.041952 2 1.899352 1 2.435687 2	1.1 0.4 1.8
302 303	182630 182630	650411 76.240764 650421 75.980039	2.435687 2 1.455961 1 2.400481 2	1.8 0.1
304	182629	650431 76.03593	2.490481 2	0.7
305	182619	650420 76.326549	2.867598 2	
306	182620	650431 76.500217	3.031509 2	1.1
307	182605	650435 77.288327	3.042996 2	1.3
308	182599	650441 77.68388	3.023035 2	1.4
309	182589	650441 78.198875	3.234606 2	1.5
310	182580	650441 78.785513	3.641316 2	1.3
311	182580	650451 78.886648	3.522774 2	0.8
312	182590	650450 78.34681	3.0706 2	1.5
313	182600	650451 77.856226	3.049324 2	1.6
314	182610	650451 77.168775	3.046841 2	0.8
315	182610	650451 77.356745	3.023038 2	
315 316 317	182610 182620 182620	650451 77.356745 650451 76.849274 650441 76.671875	3.046736 2 3.038519 2	1.1 1.1 1.3
318	182630	650441 76.16769	2.981315 2	0.8
319 320	182630 182650 182700	650451 76.327404 650411 76.971991	3.036927 2 2.969757 2 2.178216 2	0.7 0.3
321	182700	650393 79.220762	2.178316 2	1
322	182630	650460 76.510353	3.032354 2	0.4
222	182630	650461 77.000062	2.026237 2	0.2
323	182620	650461 77.009062	3.036227 2	0.3
324	182610	650461 77.522707	3.0384 2	
325	182600	650461 78.023559	3.037743 2	0.4



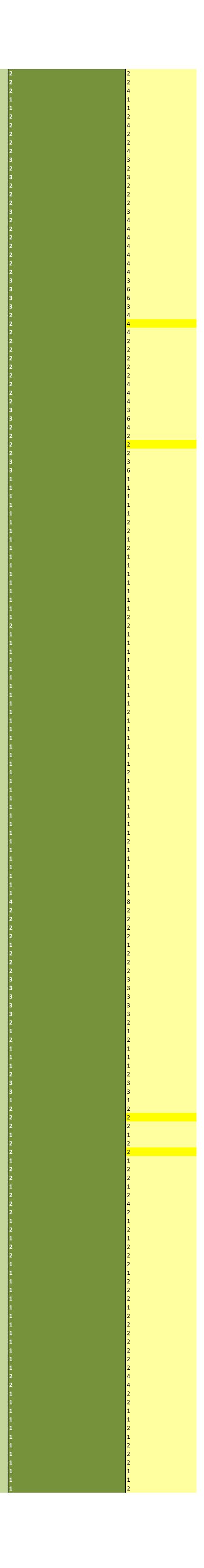




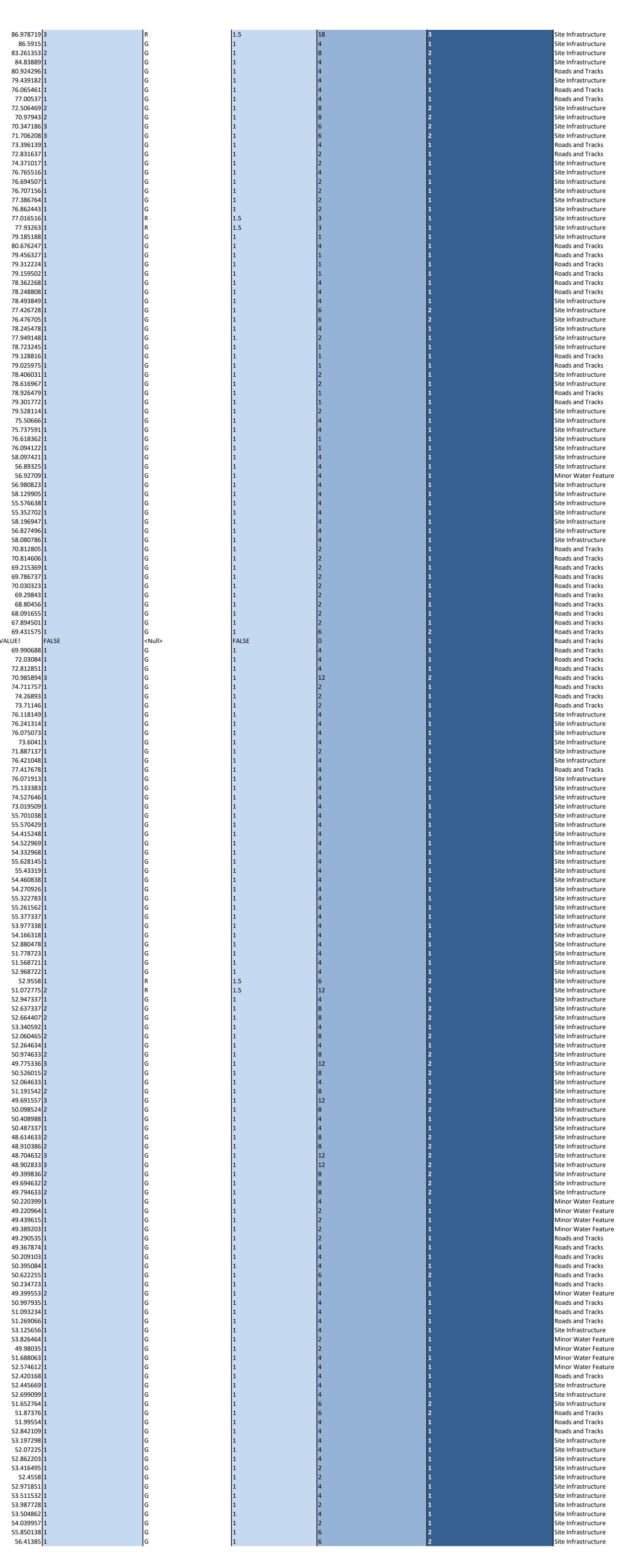
326	182590	650461	78.524639	3.036615 2	0.9
327	182579	650461	79.056905	3.298329 2	0.3
328	182554	650459	81.524429	12.417987 6	0.1
329	182503	650477	89.88935	2.425541 2	0.6
330	182643	650522	75.969627	4.038519 4	0.5
331	182660	650568	73.832216	4.159982 4	0.2
332	182664	650611	71.471179	5.726591 4	1.2
333	182665	650621	70.967249	5.697264 4	0.3
334	182665	650632	70.777337	5.701785 4	0.2
335 336	182665 182664	650642 650661	70.55579	5.574978 4 6.5501 4	0.1 0.3
337	182665	650650	70.453447	5.269915 4	0.1
338	182674	650660	69.333686	5.712457 4	0.4
339	182674	650650	69.600037	5.358445 4	0.4
340	182673	650640	69.78381	5.478262 4	0.2
341	182675	650630	69.788202	5.67952 4	0.2
342	182685	650660	68.493441	5.290087 4	0.1
343	182685	650651	68.592414	5.363981 4	1.2
344	182684	650641	68.746435	5.372629 4	0.9
345	182685	650630	68.851104	5.384724 4	1.7
346	182684	650611	69.899195	4.890601 4	0.9
347 348	182684 182674	650621 650611	69.322797 70.58565	5.208419 4 5.500826 4	1.2
349	182675	650621	70.127032	5.696061 4	0.9
350	182696	650661	67.435472	4.946696 4	0.5
351	182705	650661	66.744885	4.315277 4	0.9
352	182704	650650	66.958979	4.353361 4	1.1
353	182695	650651	67.684174	4.912638 4	0.5
354	182694	650640	67.856228	4.671182 4	1.7
355	182690	650637	68.264807	5.034281 4	0.8
356	182694	650629	68.113998	4.911669 4	1.7
357	182695	650620	68.670844	5.104583 4	0.4
358	182695	650610	69.261653	4.899404 4	0.2
359	182704	650610 650611	68.669993	5.288509 4 5.545765 4	0.2 0.2 0.4
360 361	182714 182716	650620	68.063164 67.263434	5.564689 4	0.3
362	182704	650621	67.96067	5.541075 4	0.9
363	182704	650631	67.297821	4.8514 4	1.3
364	182706	650641	66.999015	4.37736 4	1.2
365	182715	650660	66.023517	4.190876 4	0.4
366	182714	650650	66.206659	4.329598 4	1.3
367	182715	650640	66.335734	4.339601 4	0.6
368	182714	650630	66.663603	5.15614 4	0.1
369	182733	650610	66.704198	5.553281 4	0.1
370	182785	650595	65.213822	6.154286 4	0.3
371	182604	650683	74.720645	7.247243 4	0.2
372	182647	650660	71.040915	8.722743 6	0.3
373	182736	650710	66.134676	3.013444 2	0.1
374	182772	650761	66.715404	4.409353 4	0.2
375	182820	650820	61.43684	7.701969 4	0.3
376	182809	650820	62.783334	7.57976 4	0.3
377	182800	650820	64.046322	7.51338 4	0.1
378	182800	650830	63.767039	8.169546 6	0.4
379	182809	650832	62.397356	8.224506 6	0.1
380	182810	650841	61.942985	7.841934 4	0.2
381	182820	650831	60.979706	8.070055 6	0.3
382	182830	650820	60.043246	7.969149 4	0.2
383	182829	650831	59.681913	7.406031 4	0.1
384	182840	650831	58.445306	6.747778 4	0.1
385	182839	650820	58.698069	7.70589 4	0.1
386	182850	650821	57.393313	6.956649 4	0.1
387	182850	650830	57.31707	6.663587 4	0.1
388	182850	650841	57.206938	6.77936 4	0.1
389	182866	650810	55.666309	5.796682 4	1.1
390	182908	650782	52.214888	6.406655 4	0.3
391	182890	650926	51.680373	6.845376 4	0.2
392	182858	650887	55.840137	6.833636 4	0.3
393	182850	650870	56.965652	6.842238 4	0.1
394	182850	650861	57.040391	6.833652 4	0.2
395	182850	650850	57.152471	6.820239 4	0.1
396	182840	650841	58.392193	6.590568 4	0.1
397	182830	650840	59.522681	6.61973 4	0.1
398	182826	650846	59.892645	6.5824 4	0.2 0.1
399 400	182819 182800	650841 650840	60.72752 63.404383	7.075874 4 8.192559 6	0.3
401	182799	650850	63.027248	7.617765 4	0.3
402	182810	650850	61.756044	6.808368 4	0.3
403	182820	650851	60.594227	6.575943 4	0.3
404	182830	650851	59.442066	6.572234 4	0.1
405	182839	650852	58.32526	6.660352 4	0.1
406	182839	650861	58.268881	6.746225 4	0.2
407	182839	650870	58.18137	6.815744 4	0.6
408	182830	650869	59.345625	6.605457 4	0.3
409	182830	650860	59.397347	6.575717 4	0.2
410	182819	650860	60.577018	6.572232 4	0.3
411	182820	650871	60.44057	6.572235 4	0.4
412	182810	650871	61.639404	6.572234 4	0.4
413	182810	650861	61.692043	6.572235 4	0.2
414	182800	650861	62.859106	6.630559 4	0.4
415	182800	650871	62.772173	6.577091 4	0.8
416	182788	650883	64.023428	6.572219 4	0.3
417	182747	650919	67.591318	3.914551 2	0.9
418 419	182646 182627		75.9288 77.913472	3.042286 2 3.938443 2	0.4 0.7
420	182677	650527	74.055446	2.517339 2	0.2
421	182694	650504	75.479964	3.22967 2	0.4
422	182750	650533	72.193647	5.593585 4	0.3
423	182735	650558	70.525704	5.029334 4	0.2
424	182790	650614	63.228953	6.333528 4	0.1
425	182802	650596	64.071049	6.519757 4	0.3
426 427	182818 182932	650576 650577	65.012987 60.763774	6.781569 4 3.863246 2	0.5
428	182868	650599	60.165831	6.054367 4	0.1
429	182850	650623	58.368101	6.505685 4	0.1
430	182863	650639	55.946042	7.36149 4	0.4
431	182863	650648	54.951411	4.939524 4	0.3
432	182863	650657	54.923283	2.194235 2	0.1
433	182864	650668	54.984098	1.610321 1	0.1
434	182872	650668	54.728067	1.990483 1	0.2
435	182871	650658	54.627108	2.055407 2	0.1
436	182872	650648	54.790969	4.673952 4	0.1
437	182872	650639	55.90066	7.096042 4	0.1
438	182863	650619	58.249801	6.079932 4	0.1
439	182880	650618	58.339706	6.091243 4	0.2
440	182890	650630	56.868515	7.403996 4	0.3
441	182879	650638	55.836334	7.26955 4	0.1
442	182877	650646	54.883544	5.697389 4	0.1
443 444	182877 182880	650640 650662	54.467489	1.830888 1 1.937243 1	0.2
444 445 446	182880 182890 182891	650667 650659	54.1685 54.1645 54.184399	1.937243 1 1.076989 1 0.977226 1	0.2 0.2 0.1
446 447 448	182891 182891 182892	650659 650646 650638		6.070453 4 7.453731 4	0.01 0.01 0.01
449	182898	650628	57.005275	7.552496 4	0.01
450	182899	650646	54.597302	6.138965 4	0.2
451	182899	650657	54.055535	0.959945 1	0.2
452	182908	650665	53.894063	0.924319 1	0.2
453	182907	650657	53.93241	1.030433 1	0.2
454	182907	650646	54.531449	6.222766 4	0.2
455	182900	650666	54.015379	0.918474 1	0.4
456	182827	650646	58.432288	3.74462 2	0.1
457	182726	650580	69.285188	5.351572 4	0.4
458	182667	650548	74.090494	2.746744 2	0.1
459	182612	650520	78.38836	4.815399 4	0.1
460	182590	650472	78.69879	3.032531 2	0.9
461	182600	650472	78.215894	3.049009 2	0.4
461 462 463	182579 182566	650472 650464	79.224431 79.904842	3.086102 2 5.129843 4	0.4 0.4 0.4
464	182567	650451	79.664257	3.672861 2	1.1
465 466	182569 182567 182552	650441 650432	79.482321 79.458431	3.682516 2 3.674536 2 6.222412 4	0.5 0.9
467	182552	650435	80.493245	6.222412 4	0.9
468	182539	650434	82.861891	13.12724 6	0.2
469	182552	650441	80.547503	7.539499 4	0.2
470	182540	650445	83.497651	14.653076 6	0.1
471	182541	650458	84.555342	13.761121 6	0.1
472	182541	650471	85.039394	12.655889 6	0.1
473	182542	650486	86.040414	12.235865 6	0.1
474	182542	650498	86.658533	10.883847 6	0.1
474 475 476	182556 182556	650498 650498	83.96755 83.170558	10.883847 6 11.863213 6 12.204541 6	0.1 0.1 0.1
476	182555	650486	83.170558	12.204541 8	0.1
477	182555	650470	82.129516	12.326565 6	0.1
478	182567	650471	79.954993	6.614727 4	0.8
479	182567	650486	80.900586	10.49557 6	0.1
480	182567	650496	81.584384	10.462127 6	0.2
481	182580	650484	79.555068	4.538889 4	0.3
482	182583	650496	80.216979	5.075017 4	0.1
483	182591	650495	79.712754	5.088042 4	1
484	182600	650495	79.236171	5.077307 4	0.1
485	182577	650527	81.138668	8.365747 6	0.2
486	182590	650485	79.090357	4.522416 4	1
487	182600	650485	78.511483	4.315255 4	0.9
488	182498	650454	89.693518	2.494478 2	0.3
489	182476	650447	89.619406	1.433672 1	0.2
490	182457	650465	90.925593	3.063468 2	1.5



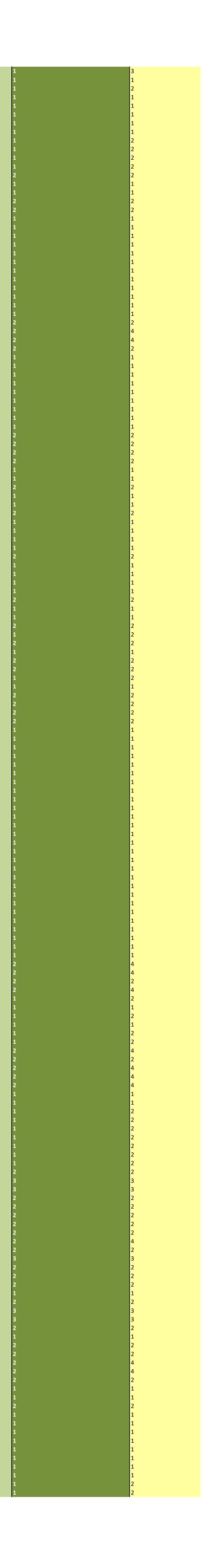
3	78.590085	1.323209 4	-0.065446	1	12
3	78.826085	5.539516 4	0.23082	1	12
3	80.15146 89.305531	9.958141 4 45.742419 3	1.372969 0.583819	1	12 9
3	78.762084 68.672505	80.153479 3 95.600001 3	-2.792457 5.159711	1	9 18
6	69.151347	53.208522 3	2.319832	1	18
6	69.151347	42.62162 3	1.815902	1	18
6	69.151347	32.788632 3	1.62599		18
6	69.151347	23.083787 3	1.404443	1	18
6	69.369851	4.944128 4	0.582974		24
6	69.369851	15.125946 3	1.083596	1	18
6	69.043349	3.455631 4	0.290337	1	24
6	69.043349	13.430112 3	0.556688	1	18
6	68.672505	23.39554 3	1.111305	1	18
6	68.672505	32.06735 3	1.115697	1	18
6	68.484504	1.199698 4	0.008937	1	24
6	68.484504	10.612835 3	0.10791	1	18
6	67.766511	20.382658 3	0.979924	1	18
6	67.766511	30.003714 <mark>3</mark>	1.084593	1	18
6	67.766511	49.582242 <mark>3</mark>	2.132684	1	18
6	67.766511	39.774458 <mark>3</mark>	1.556286	1	18
6	68.672505	51.191522 3	1.913145	1	18
6	68.672505	41.551069 <mark>3</mark>	1.454527	1	18
	67.395455	1.974909 4	0.040017	1	24
6	66.81298	3.529729 <mark>4</mark>	-0.068095	1	24
6	66.81298	7.025093 4	0.145999	1	24
6	67.580983	8.768021 4	0.103191	1	24
6	67.108982	18.347962 3	0.747246	1	18
6	67.766511 67.108982	22.523042 3 28.708227 3	0.498296 1.005016	1	18 18
6	67.108982 67.108982	37.731197 3 47.359204 3	1.561862 2.152671	1	18 18
6	66.252984 65.692981	45.58039 3 44.27435 3	2.417009 2.370183	1	18 18 18
6	65.692981	34.075981 3	1.570453	1	18
6	66.252984 66.252984	35.246876 3 25.482714 3	1.707686 1.044837	1	18 18
6	66.252984 66.104983	15.724997 3 4.544803 4	0.746031 -0.081466	1	18 24
6	66.104983 65.692981	5.477906 4 14.70113 3	0.101676 0.642753	1	24 18
6	65.692981	24.207801 3	0.970622	1	18
6	64.829157	41.162527 3	1.875041	1	18
6	60.42202	42.619041 3	4.791802	1	18
6	75.214081	6.17046 4	-0.493436	1	24
6	69.799527	8.744434 4	1.241388	1	24
3	65.909136	37.759967 3	0.22554	1	9
3	66.999017	11.024589 3	-0.283613	1	9
3	67.908833	49.566339 3	-6.471993	1	9
3	67.908833	39.434163 3	-5.125499	1	9
3	67.908833	30.07557 3	-3.862511	1	9
3	67.773529	29.286944 3	-4.00649	1	9
3	67.022738	38.702223 3	-4.625382	1	9
3	67.022738	37.473958 3	-5.079753	1	9
3	67.022738	48.7242 3	-6.043032	1	9
3	67.908833	59.568572 <mark>3</mark>	-7.865587	1	9
3	67.022738	58.204936 <mark>3</mark>	-7.340825	1	
3 3	52.596031 52.596031	58.302093 3 65.212859 3	5.849275 6.102038	1	9
3 3	52.407558 52.596031	57.813906 3 51.304768 3	4.985755 4.721039	1	9
3 3	52.596031 52.407558	44.152807 3 57.833595 3	4.610907 3.258751	1	9
6	49.147604 52.077871	29.826601 3 54.804073 3	3.067284 -0.397498	1	18
3	52.53643 52.553226	32.924518 3 36.923255 3	3.303707 4.412426	1	9
3	52.596031 52.596031	37.129782 3 39.965694 3	4.44436 4.55644	1	9
3	52.596031	52.732443 3	5.796162	1	9
3	67.022738 66.096741	57.357573 3 53.547201 3	-7.500057 -6.204096	1	9
3	67.022738 67.022738	47.021978 3 27.29273 3	-6.295218 -3.618355	1	9
3	66.096741 66.096741	26.629734 3 36.381015 3	-3.069493 -4.340697	1 1	9
3	66.096741	46.021128 3	-5.502514	1	9
3	66.096741	56.032616 3	-6.654675	1	9
3	52.596031	48.987179 3	5.729229	1	9
3	52.596031	47.35293 3	5.67285	1	9
3	52.553226	47.027756 3	5.628144	1	9
3	65.419828	53.214173 3	-6.074203	1	9
3	65.419828	54.806472 3	-6.022481	1	9
3	65.419828	44.838451 3	-4.84281	1	9
3	65.419828	43.505431 <mark>3</mark>	-4.979258	1	9
3	65.419828	33.128593 <mark>3</mark>	-3.780424	1	9
3	66.016741	35.164331 <mark>3</mark>	-4.324698	1	9
3	66.016741	25.043392 3	-3.157635	1	9
3	65.419828	23.338651 <mark>3</mark>	-2.647655	1	9
3	65.356383	11.678931 3	-1.332955	1	9
3	65.892383 77.948084	25.711401 <mark>3</mark> 55.98677 3	1.698935 -2.019284	1 1	9
3	78.626085 78.626085	51.637397 <mark>3</mark> 109.105152 3	-0.712613 -4.570639	1	9
3	78.28626	112.164493 3	-2.806296	1	9
	62.151739	112.068094 3	10.041908	2	36
6	62.151739 60.69602	92.120681 3 24.01893 3	8.373965 2.532933	1	18 18
6	60.42202 59.525873	37.066813 3 57.281518 3	3.649029 5.487114	1	18 18 18
3	59.642346 57.818705	35.936307 3 43.719894 3	1.121428 2.347126	1	9 18
6	57.818705 55.132727	13.303221 3 10.829522 3	0.549396 0.813315	1	18 18 18
6	54.91059	4.213404 4	0.040821	1	24
6	54.937618 54.887358 54 780324	0.423913 4 4.022599 4 1.902089 4	-0.014335 0.09674 -0.052257	1	24 24 24
6 6	54.780324 54.886693 54.91059	1.902089 4 6.617776 4 11.646967 3	-0.052257 -0.259585 -0.119621	1	24 24 18
3	54.91059 54.865059 57.818705	11.646967 3 16.328129 3 24.744965 3	-0.119621 1.035601 0.431096	1	18 9 18
3	57.818705 55.099208 55.074479	24.744965 3 26.265334 3	0.431096 3.240498 1.794036	1	18 9
3	55.074479 54.865059 54.865059	13.836012 3 10.497647 3	1.794036 0.971275 0.018485	1	9 9 12
6	54.865059 54.780324 54.732502	9.431342 4 9.800639 4	0.018485 -0.312835 -0.315617	1	12 24 24
3	54.732502 54.282947 54 282947	9.595509 4 15.111747 3 7 386301 4	-0.315617 -0.118447 -0.098548	1	24 9 12
3	54.282947 54.812075 55.049698	7.386301 4 1.194761 4 5.478922 4	-0.098548 -0.126779 0.712711	1	12 12 12
3	55.049698 55.049698 54.303101	5.478922 4 16.799484 3	0.712711 1.955577 0.204111	1	12 9 12
3	54.393191 54.258112 54.004076	1.825193 4 7.901333 4	0.204111 -0.202577 -0.110013	1	12 12
3	54.004076 54.035637 54.329263	13.321791 3 5.809759 4	-0.110013 -0.103227 0.202186	1	9 12 12
3	54.329263	3.012723 4	0.202186	1	12
	54.035637	16.098963 3	-0.020258	1	9
6	58.894357	10.574792 3	-0.462069	1	18
6	64.829157	72.071426 3	4.456031	1	18
6	67.766511	113.923541 3	6.323983	1	18
3	78.762084	59.943377 3	-0.373724	1	9
3	78.762084	7.854125 4	-0.063294	1	12
	78.626085	13.873057 3	-0.410191	1	9
3	78.862084	8.293915 4	0.362347	1	12
	79.877242	0.928987 4	0.0276	1	12
3	79.848981	10.663357 3	-0.184724	1	9
	79.722536	20.431552 3	-0.240215	1	9
3	79.593069	22.129439 3	-0.134638	1	9
	80.651121	19.449393 3	-0.157876	1	9
3	83.050549	14.659232 3	-0.188658	1	9
3	79.973852	23.797657 3	0.573651	1	9
3	84.229902	25.885554 3	-0.732251	1	9
3	80.15146	22.570865 3	4.403882	1	9
3	80.243371	22.06257 3	4.796023	1	9
3	80.243371	29.256677 3	5.797043	1	9
3	79.996909	37.883332 3	6.661624	1	9
3	79.996909	30.479498 3	3.970641	1	9
3	79.996909	19.525209 3	3.173649	1	9
3	80.243371	9.143752 4	1.886145	1	12
3	79.996909	1.496174 4	-0.041916	1	12
3	79.996909	16.202281 3	0.903677	1	9
3	79.996909	26.887243 3	1.587475	1	9
3	79.810547	18.905195 3	-0.255479	1	
3	79.810547	30.009908 3	0.406432	1	9
3	78.762084	29.775821 3	0.95067	1	9
3	78.762084	32.43826 3	0.474087	1	9
3	79.810547	58.086922 3	1.328121	1	
3	78.762084	19.664507 3	0.328273	1	9
3	78.762084	23.794424 3	-0.250601	1	
3	89.305531	22.874288 3	0.387987	1	9
3	89.340409	24.325491 3	0.278997	1	9
3	89.340409	50.22826 3	1.585184	1	9



			650407	88.078719	4.503714			1.1	8
49	93 1	182442	650399 650355	86.8915 83.861353	4.809611 4.726802	4		0.3 0.6	8
49	95 1	182403	650365 650309	85.13889 81.224296	4.704801 4.706535	4		0.3 0.3	8
49	97 1	182415	650298 650252	79.739182 76.165461	4.722792 5.151092	4		0.3 0.1	- - -
			650254 650223	77.01537 73.506469	5.151851 4.617381			0.01 1	-
		182413 182468	650202 650185	71.87943 72.447186	4.328297 2.979173			0.9 2.1	-
		182476 182519	650203 650195	73.506208 73.896139	2.982286 4.479274			1.8 0.5	
		182512 182596	650172 650248	72.931637 74.381017	2.922271 2.519913			0.1 0.01	- - -
		182597 182600	650273 650280	76.775516 76.704507	4.34046 3.720191			0.01 0.01	- - -
			650298 650323	76.807156 77.396764	3.378079 2.081454			0.1 0.01	-
52	10 1	182622	650349 650373	77.062443 77.116516	2.933103 2.833791	2		0.2 0.1	-
53	12 1	182645	650374 650372	78.13263 79.195188	2.481514 1.792272	2		0.2 0.01	-
53	14 1		650351 650348	80.686247 79.466327	5.37125 0.879135	4		0.01 0.01	8
53	16 1	182697	650323 650299	79.322224 79.169502	0.774487	1		0.01 0.01	-
52	18 1	182696 182673	650274 650248	78.372268 78.258808	4.233461 5.946965	4		0.01 0.01	- - -
52	20 1	182649	650246	78.593849	7.322617	4		0.1	-
52	22 1	182622	650249	77.436728 76.486705	8.642537 8.623069	6		0.01	-
52	24 1	182622	650273 650298	78.255478 77.959148	4.06029 2.077935	2		0.01 0.01	-
52	26 1	182671	650298 650348	78.733245 79.138816	0.755666	1		0.01 0.01	- -
52	28 1	182649	650348	79.035975 78.416031	0.558807 2.961456	2		0.01 0.01	-
53	30 1	182672		78.626967 78.936479	2.810129 0.512465	1		0.01 0.01	-
			650273 650273	79.311772 79.538114	1.892822 3.606057			0.01 0.01	
			650223 650223	75.51666 75.747591	5.880064 7.635208			0.01 0.01	-
			650323 650348	76.718362 76.294122	1.98568 1.298175			0.1 0.2	-
			650618 650629	58.297421 57.09325	5.530262 7.118391			0.2 0.2	Ĩ
			650630 650629	57.02709 57.080823	6.597041 7.350987			0.1 0.1	1
			650618 650638	58.329905 55.676638	6.994422 7.508273			0.2 0.1	
			650637 650619	55.552702 58.206947	7.320533 7.429162			0.2 0.01	!
			650628 650618	56.837496 58.090786	7.579183 7.592199			0.01 0.01	!
			650253 650267	70.822805 70.824606	2.27648 2.365296			0.01 0.01	- - -
			650245 650239	69.225369 69.796737	3.495449 3.226267			0.01 0.01	(
5	51 1	182864		70.040323 69.30843	2.281479 2.866606	2		0.01 0.01	-
5	53 1	182881	650212 650220	68.81456 68.101655	3.47585 3.504945	2		0.01 0.01	(
5	55 1	182880		67.904501 69.441575	3.888439 8.457698	2		0.01 0.01	(
5	57 1	182861	650166 650179	70.402663 70.000688	6.738395 5.077024	4	<null></null>	0.01	#VALU
5	59 1	182830	650175 650171 650157	72.04084 72.822851	5.345758 4.940507	4		0.01 0.01	-
50	61 1	182844	650146	73.185894	4.318498	4		2.2	- -
50	63 1	182818	650125 650142	75.111757 74.27893	2.69036 3.159477	2		0.4 0.01	
50	65 1	182781		73.72146 76.418149	3.131288 7.334648	4		0.01	-
50	67 1	182744	650028	76.641314 76.375073	5.456185 5.534292	4		0.4 0.3	-
50	69 1	182701	650044 650053	73.9041 72.087137	5.470438 3.360876	2		0.3 0.2	-
57	71 1	182696		76.921048 77.717678	5.448773 5.180495	4		0.5 0.3	-
57	73 1	182658	649976 649982	76.371913 75.433383	4.246405 4.289116	4		0.3 0.3	-
			650013 650024	74.827646 73.219509	4.992246 4.264151			0.3 0.2	-
			650838 650848	56.001038 55.870429	6.840688 6.855785			0.3 0.3	:
			650838 650848	54.815248 54.722969	6.643093 6.817118			0.4 0.2	!
			650858 650858	54.632968 55.828145	6.834391 6.860864			0.3 0.2	! !
		182860 182870	650868 650868	55.73319 54.560838	6.846857 6.847805			0.3 0.1	!
			650878 650878	54.470926 55.622783	6.861808 6.833647			0.2 0.3	! !
			650888 650898	55.561562 55.477337	6.83433 6.848437			0.3 0.1	! !
			650898 650888	54.277338 54.366318	6.847929 6.853557			0.3 0.2	!
			650898 650898	53.080478 51.878723	6.847608 6.846722			0.2 0.1	! !
			650888 650888	51.968721 53.168722	6.844248 6.840207			0.4 0.2	!
			650878 650878	53.2558 52.072775	6.838357 6.656796			0.3 1	ļ
			650868 650858	53.347337 53.437337	6.836899 6.644667			0.4 0.8	
			650848 650838	53.564407 53.740592	6.191069 5.829661			0.9 0.4	1
60	00 1	182890	650838 650848	52.760465 52.564634	5.722335 5.733848	4		0.7 0.3	1
			650838 650848	51.774633 51.575336	5.712505 5.73452			0.8 1.8	
60	04 1	182900		51.426015 52.364633	5.719118 5.819329	4		0.9 0.3	!
60	06 1	182890	650868	52.191542 51.191557	6.200006 5.714127	4		1 1.5	1
			650877 650888	51.098524 50.808988	5.820796 6.168899			1 0.4	:
63	10 1	182900	650898 650898	50.687337 49.614633	6.631308 5.824037	4		0.2 1	1
63	12 1	182910		49.810386 50.004632	5.745915 5.719671	4		0.9 1.3	2
63	14 1	182910	650868 650858	50.202833 50.399836	5.716395 5.736317	4		1.3 1	2
63	16 1	182910	650848 650838	50.594632 50.794633	5.712876 5.716434	4		0.9 1	
			650752 650752	50.620399 49.720964	6.554375 3.451776			0.4 0.5	
				49.639615 49.589203	3.558984 3.580476			0.2 0.2	
				49.590535 49.567874	3.678319 4.025211			0.3 0.2	4
			650742 650742	50.219103 50.405084	5.594131 7.315303			0.01 0.01	
			650742 650742	50.632255 50.244723	8.199825 4.07548			0.01 0.01	
			650742 650732	50.299553 51.007935	3.599406 4.873903			0.9 0.01	2
63	30 1	182925	650732 650732	51.103234 51.279066	6.721423 7.62208	4		0.01 0.01	1
63	32 1	182924	650712	53.135656 53.836464	4.88824 3.163684	4		0.01 0.01	1
63	34 1	182915	650742 650722	50.48035 51.988063	3.516926 5.001962	2		0.5 0.3	
63	36 1	182915	650712	52.774612 52.430168	4.919159 6.565588	4		0.2 0.01	, , ,
63	38 1	182935		52.645669 52.999099	7.674479 7.961932	4		0.2 0.3	
64	40 1	182945	650722 650731 650732	51.752764 51.97376	8.406726 8.666097	6		0.3 0.1 0.1	1
64	42 1	182965	650732	52.09554 52.942109	6.995224 7.025866	4		0.1 0.1 0.1	1
64	44 1	182956	650722 650722 650727	53.397298 52.17225	7.025866 5.692964 7.976142	4		0.1 0.2 0.1	1
64	46 1	182965		52.17225 52.962203 53.616495	7.976142 5.742604 3.34921	4		0.1 0.1 0.2	!
64	48 1	182965	650702	53.616495 52.6558 53.171851	3.34921 3.877705 4.019699	2		0.2 0.2 0.2	:
65	50 1	182945	650703	53.711532 54.087728	4.019699 4.021391 2.345224	4		0.2 0.2 0.1	:
65	52 1	182936		54.087728 53.904862 54.049957	2.345224 4.768556 2.168299	4		0.1 0.4 0.01	:
6	54 1	182934	650702 650632 650632	55.950138	2.168299 8.005859 10.239734	6		0.01 0.1 0.1	
0	1		550032		-v.209/34			<b>U.T</b>	



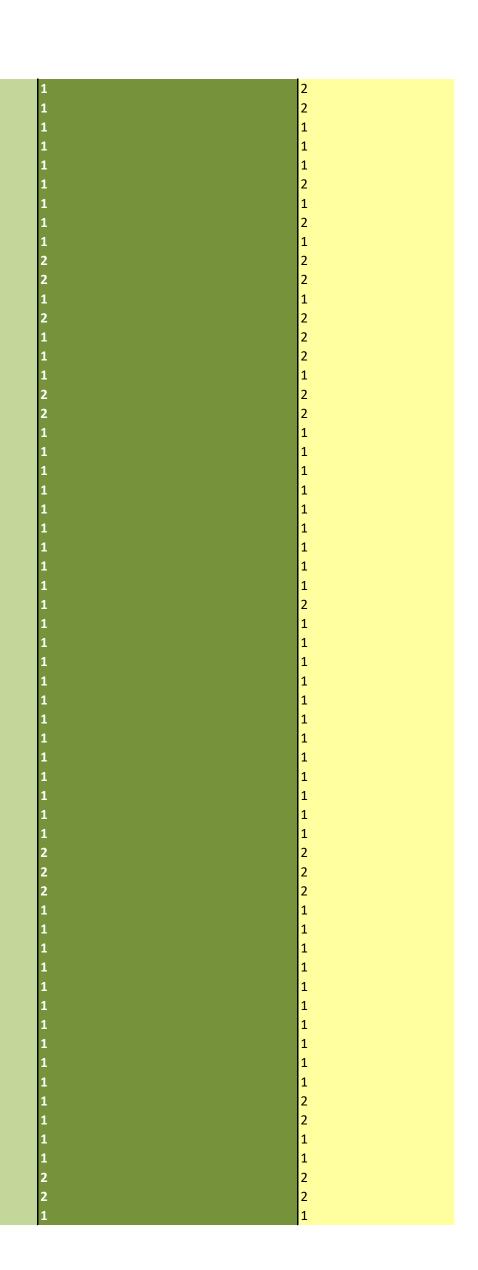
3	85.388829	49.173176 3	2.68989	1	9
3	85.388829	25.723091 <mark>3</mark>	1.502671	1	9
3	82.522829	25.808903 3	1.338524	1	9
3	82.522829	49.687634 <mark>3</mark>	2.616061	1	9
3	77.987994	39.576945 3	3.236302	1	9
3	78.666839	23.278292 3	1.072343	1	9
3	77.385993	13.866772 3	-1.220532	1	9
3	77.975992	11.145223 3	-0.960622	1	9
3	75.388055	26.10801 3	-1.881586	1	9
3	75.388055	50.223172 3	-3.508625	1	9
3	75.3054	49.683679 3	-2.858214	1	9
3	75.3054	29.444522 <mark>3</mark>	-1.799192	1	9
3	72.738095	9.135819 4	1.158044	1	12
3	72.146039	14.803204 <mark>3</mark>	0.785598	1	9
3	74.222997	10.561432 3	0.15802	1	9
3	76.648885	6.191536 <mark>4</mark>	0.126631	1	12
3	76.684819	1.051063 4	0.019688	1	12
3	76.421514	10.688996 3	0.385642	1	9
3	76.546145	25.52151 3	0.850619	1	9
3	76.3207	18.958911 3	0.741743	1	9
3	76.434721	12.020135 3	0.681795	1	9
3	76.500515	33.801241 3	1.632115	1	9
3	76.404514	59.708701 3	2.790674	1	9
3	79.331096	29.894459 3	1.355151	1	9
3	79.331096	39.485373 3	0.135231	1	9
3	79.099087	27.207412 <mark>3</mark>	0.223137	1	9
3	78.427865	21.097757 3	0.741637	1	9
3	77.766413	11.614371 3	0.605855	1	9
3	77.003241	24.268738 3	1.255567	1	9
3	77.286	9.360661 4	1.307849	1	12
3	77.539821	0.88238 4	-0.103093	1	12
3	77.454002	6.42895 4	-0.967297	1	12
3	78.089969	6.439072 4	0.165509	1	12
3	77.311974	24.76814 3	0.647174	1	9
3	78.089969	42.278046 3	0.643276	1	9
3	79.331096	61.276004 3	-0.19228	1	9
3	78.913014	51.644771 <mark>3</mark>	0.122961	1	9
3	76.3207	45.029327 3	2.095331	1	9
3	76.470144	50.89974 <mark>3</mark>	2.156823	1	9
3	78.122893	42.282051 3	0.813586	1	9
3	77.653072	33.715932 <mark>3</mark>	1.6587	1	9
3	77.878001	25.500884 3	1.660113	1	
3	74.607145 76.143357	9.838584 <mark>4</mark> 4.416799 4	0.909515 -0.395766	1	12 12
3	76.620465 76.316145	2.913435 4 0.903914 4	0.097897 -0.022023	1	12 12
3	55.099208 54.865059	30.236242 3 21.848592 3	3.198213 2.228191	1	9
6	57.424877 55.099208	16.805786 3 17.55617 3	-0.397787 1.981615	1	18
3	55.074479	25.162242 3	3.255426	1	9
3	55.049698	8.9933 4	0.62694	1	12
3	54.329263	10.169572 3	1.223439	1	9
3	55.049698	25.439974 3	3.157249	1	
3	54.329263	19.871711 3	2.508233	1	9
3	55.049698	28.946785 3	3.041088	1	
3	71.064583	8.474437 4	-0.241778	1	12
3		15.64682 3	-0.508702	1	9
3	69.922352	35.860667 3	-0.696983	1	9
3	70.957342	30.451788 3	-1.160605	1	
3 3	70.937342 70.987049 69.223318	20.803225 3 2.912603 4	-0.946726 0.085112	1 1	9 12
3	69.219295 69.219295	14.417261 3 33.880928 3	-0.404735 -1.11764	1	9
3	68.315857 70.012376	5.985593 4 23.550135 3	-0.411356 -0.570801	1	12 9
3	70.472377 70.276377	2.894632 4 11.188379 3	-0.069714 -0.275689	1	12 9
3	72.694322 72.809254	9.646082 4 1.017005 4	-0.653482 0.013597	1	12 12
3	72.312379 75.077374	13.33721 3 19.330089 3	0.873515 0.034383	1 1	9
3	73.913269	8.068815 <mark>4</mark>	0.365661	1	12
3	73.818794	2.599309 4	-0.097334	1	12
3	76.425616	0 4	-0.007467	1	12
3	76.684417	0 4	-0.043103	1	12
3	75.738416	28.850264 3	0.636657	1	9
3	73.745048	20.764253 3	0.159052	1	9
3	71.578088	21.396971 <mark>3</mark>	0.509049	1	9
3	75.174427	63.61781 3	1.746621	1	9
3	79.872188	86.825463 3	-2.15451	1	9
3	72.36505	101.692833 3	4.006863	1	9
3	71.447866	102.582836 3	3.985517	1	9
3	72.881047	58.111358 3	1.946599	1	9
3	71.447866	56.634254 <mark>3</mark>	1.771643	1	9
3	52.596031	37.855507 <mark>3</mark>	3.405007	1	9
3	52.596031	31.512965 <mark>3</mark>	3.274398	1	9
3	52.407558	31.232131 3	2.40769	1	9
3	52.596031	23.876505 3	2.126938	1	9
3	52.596031	18.047867 3	2.036937	1	9
3	52.596031	27.513184 <mark>3</mark>	3.232114	1	9
3	52.570416	26.481931 3	3.162774	1	9
3	52.570416	16.666716 3	1.990422	1	9
3	52.53643	17.939041 3	1.934496	1	9
3	52.53643	27.20084 3	3.086353	1	9
3	52.53643	31.354968 3	3.025132	1	9
3	52.53643	37.705791 3	2.940907	1	9
3	52.53643	31.47848 3	1.740908	1	9
3	52.53643	23.463557 3	1.829888	1	9
3	52.53643	27.150302 3	0.544048	1	9
3	52.077871	26.787376 3	-0.199148	1	9
3	52.077871	16.790637 3	-0.10915	1	9
3	52.53643	18.011793 3	0.632292	1	9
3	52.53643	9.464717 4	0.71937	1	12
3	52.077871	6.836154 4	-0.005096	1	12
3	52.570416	6.588163 4	0.776921	1	12
3	52.596031	9.741329 4	0.841306	1	12
3	52.407558	17.47356 <mark>3</mark>	1.156849	1	9
3	52.407558	26.624016 3	1.333034	1	9
3	52.209372	25.196231 3	0.551093	1	9
3	52.209372	15.227735 3	0.355262	1	9
3	52.209372	26.933509 3	-0.434739	1	9
3	52.209372	17.917921 3	-0.634036	1	9
3	51.971194	9.963695 4	-0.545179	1	12
3	52.209372	5.246132 4	0.155261	1	12
3	52.138944	0.939005 4	0.052598	1	12
3	51.735194	5.444376 4	-0.543637	1	12
3	51.851196	8.667617 4	-0.752672	1	12
3	51.851196	18.364637 3	-1.042208	1	9
3	51.851196	27.801041 3	-1.163859	1	9
3	51.851196	31.969765 3	-2.236563	1	9
	51.851196	24.216273 3	-2.04081	1	9
3	51.695194	17.778748 3	-1.690562	1	9
	51.735194	15.488946 3	-1.532361	1	9
3	51.735194	17.999702 3	-1.335358	1	9
3	51.971194	24.520577 3	-1.376562	1	9
3 6	52.209372 50.09268	31.852502 3 11.332402 3	-1.414739 0.527719	1 1	9 18 24
6	49.816761	4.300892 4	-0.095797	1	24
	49.669706	2.293059 4	-0.030091	1	24
6	49.409195	10.308276 3	0.180008	1	18
3	50.210191	8.44145 4	-0.619656	1	12
3	50.132717	6.648927 4	-0.564843	1	12
	50.337184	2.445387 4	-0.118081	1	12
3	50.462483 50.397581	0.454962 4 1.622906 4 4.742012 4	-0.057399 0.234674	1	12 12
3	50.588117	4.743912 4	-0.343394	1	12
6	50.215889	1.422847 4	0.083664	1	24
3	51.072314 50.979048 51.088116	0.625362 4 1.331826 4 2.030644 4	-0.064379 0.124186 0.19095	1	12 12 12
3	51.088116 52.500116 52.786292	2.030644 4 16.822433 3 24.226555 2	0.19095 0.63554 1.050171	1	12 9 18
6	52.786293 50.622105 51.605667	24.236555 3 5.441789 4 5.522002 4	1.050171 -0.141755 0.282206	1	18 24 24
6	51.605667 52.489924 51.102274	5.522003 4 10.868497 3 11 142275 2	0.382396 0.284688	1	24 18
3	51.102374	11.143375 3	1.327794	1	9
	52.500116	1.790862 4	0.145553	1	12
3	52.708355	2.445321 4	0.290744	1	12
	51.904292	3.581978 4	-0.151528	1	12
3	50.782483 50.644483	7.500199 4 9.642797 4 19.825042 2	1.191277 1.451057 2.111626	1	12 12 0
3	50.830483 52.549354	18.825943 3 11.68217 3	2.111626 0.847944 0.076011	1	9 9 12
3	52.096239	0.864937 4	0.076011	1	12
3	52.549354	24.847705 3	0.412849		9
3	52.708355 52.708355	16.959817 3 30.993143 3 24.002225 2	0.90814 -0.052555	1	9 9
3 3	52.708355 52.708355	24.993335 3 20.992289 3	0.463496 1.003177 1.270372	1	9 9
3	52.708355 52.500116 52 500116	11.721626 3 11.655273 3 21 595495 3	1.379373 1.404746 1.549841	1	9 9
3	52.500116 53.757637 59.296345	21.595495 3 22.086824 3 25 718292 3	1.549841 2.192501 -2 782495	1	9 9 9
3	59.296345	25.718292 <mark>3</mark>	-2.782495	1	9



	656 657 658 659 660 661 662 663 664 665 666	182953 182963 182973 182983 182983 182983 182973 182973 182964 182964 182964 182959	650632 650631 650632 650612 650612 650613 650622 650622 650612 650612	56.385326 56.416628 56.462201 56.232446 56.990775 57.274246 58.363628 57.806941 58.263142 59.010119 59.407081	12.306441 6 12.405277 6 7.153391 4 5.132115 4 5.282503 4 6.901939 4 6.381248 4 8.218749 6 7.95001 4 3.359831 2 3.096498 2	1 0.2 0.2 0.1 0.1 0.1 0.2 0.2 0.2 0.1 0.1 0.2	56.216628 1 56.262201 1 56.132446 1 56.890775 1 57.174246 1 58.163628 1 57.606941 1 58.163142 1 58.910119 1
	667 668 669 670 671 672 673 674 675 676 677 678 679	182954 182953 182944 182934 182933 182946 182953 182953 182953 182943 182943 182943 182943 182943	650621 650612 650621 650612 650612 650602 650592 650581 650581 650592 650602 650602	58.534863 59.244128 58.151586 57.399747 58.617097 59.203854 59.749996 60.197924 60.669125 60.352353 59.859584 59.431094 59.190907	7.943128 4 2.761841 2 8.935706 6 8.480763 6 5.68765 4 3.252534 2 2.706394 2 2.67494 2 2.751856 2 3.076597 2 3.16055 2 3.092933 2 3.153284 2	0.4 0.01 0.01 0.2 0.7 0.3 0.1 0.01 0.1 0.4 0.6 0.01	59.234128 1 58.141586 1 57.389747 1 58.417097 1 58.503854 2 59.449996 1 60.097924 1 60.659125 1 60.252353 1 59.459584 1 58.831094 2
	680 681 682 683 684 685 686 687 688 689 690 691	182934 182950 182960 182970 182981 182980 182980 182980 182980 182980 182970 182970	650591 650488 650489 650489 650489 650479 650470 650460 650449 650439 650439 650449	59.837678 64.240061 63.394013 62.947856 62.510804 63.617484 64.185297 64.749832 65.159406 65.481604 65.724786 65.247542	3.620551 2 4.51051 4 7.050921 4 8.91176 6 7.877866 4 6.650883 4 5.866902 4 4.843012 4 3.443922 2 2.79991 2 3.701533 2 2.78303 2	0.01 0.01 0.4 0.01 0.2 0.5 0.3 0.3 0.1 0.1 0.1 0.01 0.2	59.827678 1 64.230061 1 62.994013 1 62.937856 1 62.310804 1 63.117484 1 63.885297 1 64.449832 1 65.059406 1 65.381604 1 65.714786 1
	692 693 694 695 696 697 698 699 700 701 702 703	182970 182970 182970 182960 182961 182960 182960 182960 182949 182941 182931	650459 650469 650479 650469 650464 650460 650449 650439 650440 650440	64.922159 64.802754 64.488938 64.284761 64.690475 65.18942 65.199754 65.7187 66.215891 66.70623 67.134613 67.63655	1.921147 1 1.83187 1 5.463158 4 3.785216 2 2.97734 2 4.030413 4 3.931317 2 4.024986 4 4.024986 4 4.024986 4 4.024986 4 4.009829 4 3.80809 2	0.3 0.3 0.1 0.9 0.01 0.1 0.01 0.01 0.01 0.01 0.	64.502754 1 64.388938 1 63.384761 2 64.680475 1 65.08942 1 65.189754 1 65.7087 1 66.205891 1 66.69623 1 67.124613 1 66.63655 2
	704 705 706 707 708 709 710 711 712 713 714 715	182932 182930 182931 182931 182931 182941 182941 182951 182951 182951 182951 182951	650450 650470 650479 650489 650469 650459 650449 650449 650459 650469 650480	67.099902 66.666934 66.118592 65.648372 65.170016 65.665059 66.167571 66.671294 66.173988 65.681537 65.155452 64.646462	4.02498644.02498644.03649843.97570823.95875524.03865344.02498644.02499544.02499244.02500144.03782444.0464654	0.01 0.4 0.1 0.1 0.3 0.6 1 0.4 0.01 0.01 0.01 0.01	66.266934 1 66.018592 1 65.548372 1 64.870016 1 65.065059 2 65.167571 2 66.271294 1 66.163988 1 65.671537 1 65.145452 1
Slope Angles	0 2 4 8 15	<b>Co-eff.</b> 2.0 4.0 8.0 15.0 35.0	1.0 2.0 4.0 6.0 8.0				
Peat depths	0 0.51 1.01 3.01	<b>Co-eff.</b> 0.5 1.0 3.0 6.0	1.0 2.0 3.0 8.0				
<b>Substrate</b> G R C not proven slip material		Co-eff.	1.0 1.5 2.0 2.0 5.0				
Receptor Roads and Tracks Minor Water Feature Dwelling Major Water Feature Site Infrastructure Important Habitat		Co-eff	3.0 6.0 6.0 8.0 3.0 8.0				
Receptor Dist.	0 10 100 1000	<b>Co-eff.</b> 10.0 100.0 1000.0 2000.0	4.0 3.0 2.0 1.0				
Receptor Elev.	0 10 50 100	<b>Co-eff.</b> 10.0 50.0 100.0 200.0	1.0 2.0 3.0 4.0				
risk rating normalisation	0 5 15 31 50	5.0 15.0 31.0 50.0 100.0	1.0 2.0 3.0 4.0 5.0				
impact rating normalisa	tion 0 10 20 30 50	10.0 20.0 30.0 50.0 100.0	1.0 2.0 3.0 4.0 5.0				

.385326 2	G	1	12	2	Site Infrastructu
.216628 1		1	12 C	2	Site Infrastructu
.262201 1	G	1	8	2	Site Infrastructu
.132446 1	0	1	4	1	Site Infrastructu
	G		4	1	
.890775 1 .174246 1	G		4		Site Infrastructu Site Infrastructu
	R	1.5	6	2	
.163628 1	G		4		Site Infrastructu
.606941 1	G	1	6	2	Site Infrastructu
.163142 1	G	1	4		Site Infrastructu
.910119 1	G	1	2		Site Infrastructu
.207081 1	G	1	2		Site Infrastructu
.134863 1	G	1	4	1	Site Infrastructu
.234128 1	G	1	2		Site Infrastructu
.141586 1	G	1	6	2	Site Infrastructu
.389747 1	G	1	6	2	Site Infrastructu
.417097 1	G	1	4	1	Site Infrastructu
.503854 2	G	1	4	1	Site Infrastructu
.449996 1	G	1	2	1	Site Infrastructu
.097924 1	G	1	2	1	Site Infrastructu
.659125 1	G	1	2	1	Site Infrastructu
.252353 1	R	1.5	3	1	Site Infrastructu
.459584 1	G	1	2	1	Site Infrastructu
.831094 2	G	1	4	1	Site Infrastructu
.180907 1	G	1	2	1	Site Infrastructu
.827678 1	G	1	2	1	Site Infrastructu
.230061 1	G	1	4	1	Site Infrastructu
.994013 1	G	1	4	1	Site Infrastructu
.937856 1	G	1	6	2	Site Infrastructu
.310804 1	G	1	4	1	Site Infrastructu
.117484 1	G	1	4	1	Site Infrastructu
.885297 1	G	1	4	1	Site Infrastructu
.449832 1	G	1	4	1	Site Infrastructu
.059406 1	G	1	2	1	Site Infrastructu
.381604 1	G	1	2	1	Site Infrastructu
.714786 1	G	1	2	1	Site Infrastructu
.047542 1	G	1	2	1	Site Infrastructu
.622159 1	G	1	1	1	Site Infrastructu
.502754 1	G	1	1	1	Site Infrastructu
.388938 1	G	1	4	1	Site Infrastructu
.384761 2	G	1	4	1	Site Infrastructu
.680475 1	G	1	2	1	Site Infrastructu
5.08942 1	G	1	4	1	Site Infrastructu
.189754 1	G	1	2	1	Site Infrastructu
65.7087 1	G	1	4	1	Site Infrastructu
.205891 1	G	1	4	1	Site Infrastructu
6.69623 1	G	1	4	1	Site Infrastructu
.124613 1	G	1	4	1	Site Infrastructu
6.63655 2	G	1	4	1	Site Infrastructu
.089902 1	G	1	4	1	Site Infrastructu
266934 1	G	1	4	1	Site Infrastructu
.018592 1	G	1	4	1	Site Infrastructu
548372 1	G	1	2	1	Site Infrastructu
870016 1	G	1	2	1	Site Infrastructi
.065059 2	G	1	8	2	Site Infrastructu
.167571 2	R	1.5	12	2	Site Infrastructu
.271294 1	G	1	4	1	Site Infrastructu
.163988 1	G	1	4	1	Site Infrastructu
.671537 1	G	1	4	1	Site Infrastructu
.145452 1	G	1	4	1	Site Infrastructu
.636462 1	G	1	4	1	Site Infrastructu

3	59.296345	22.471134 3	-2.911019
3	59.158161	21.810418 3	-2.741533
3	59.158161	24.944131 3	-2.69596
3	59.158161	30.065969 3	-2.925715
3	59.158161	23.783009 3	-2.167386
3	59.158161	20.280245 3	-1.883915
3	59.158161	11.252384 <mark>3</mark>	-0.794533
3	59.158161	16.126681 <mark>3</mark>	-1.35122
3	59.158161	12.690023 <mark>3</mark>	-0.895019
3	59.158161	2.764139 4	-0.148042
3	59.446995	0.748544 4	-0.039914
3	59.296345	11.880523 <mark>3</mark>	-0.761482
3	59.296345	4.392523 4	-0.052217
6	59.296345	17.477821 3	-1.144759
3	59.440273	24.372949 3	-2.040526
	59.440273	21.539099 3	-0.823176
	59.440273	8.747812 4	-0.236419
	59.589793	3.751776 <mark>4</mark>	0.160203
	59.642346	11.085441 3	0.555578
	59.642346	21.430214 3	1.026779
	59.642346	25.206808 <mark>3</mark>	0.710007
	59.538669	17.654832 3	0.320915
	59.538669	12.16299 3	-0.107575
	59.538669	20.838103 3	-0.347762
	59.538669	25.526764 <mark>3</mark>	0.299009
	65.068296	21.508104 3	-0.828235
	64.874209	21.880059 3	-1.480196
	64.874209	24.780092 3	-1.926353
	64.874209	30.917025 3	-2.363405
	64.876686	24.694258 3	-1.259202
	64.876686	20.388798 3	-0.691389
	64.979092	19.725854 <mark>3</mark>	-0.22926
	65.276186	23.917605 3	-0.11678
	65.276186	29.752489 3	0.205418
	65.276186	23.710231 3	0.4486
	65.276186	15.552023 <mark>3</mark>	-0.028644
	64.979092	10.407739 <mark>3</mark>	-0.056933
	64.876686	10.309738 <mark>3</mark>	-0.073932
	64.874209	16.537597 <mark>3</mark>	-0.385271
	64.874209	11.304632 3	-0.589448
	64.874209	2.632823 4	-0.183734
	65.173811	0.842227 4	0.015609
	65.276186	1.373031 4	-0.076432
	65.276186	10.830744 3	0.442514
	65.276186	20.150882 3	0.939705
	65.474173	19.973103 3	1.232057
	65.474173	23.847294 3	1.66044
	65.474173	30.765302 3	2.162377
	65.474173	24.146124 3	1.625729
	65.474173	22.163352 3	1.192761
	65.268363	22.220068 3	0.850229
	65.268363	25.710363 3	0.380009
	65.268363	32.329312 3	-0.098347
	65.268363	12.577125 3	0.396696
	65.474173	12.157651 3	0.693398
	65.474173	17.073941 3	1.197121
	65.474173	10.804956 3	0.699815
	65.474173	3.071322 4	0.207364
3 3 3	65.068296 65.068296	4.286947 4 12.666104 3	0.087156 -0.421834





APPENDIX D – PEAT CORING RECORDS



# Background

Peat cores were obtained from two locations at the proposed Crossaig Substation and associated infrastructure in July 2022, one at the northern boundary of the proposed substation footprint and one in the proposed temporary works area. Cores were advanced in areas of the Site where peat probing had identified the presence of deep peat to characterise the properties of the peatland in accordance with the *Peatland Survey. Guidance on Developments on Peatland (2017).* The document, which was published jointly by the Scottish Government, Scottish Natural Heritage (NatureScot) and SEPA, defines a consistent sampling methodology to quantify and qualify the peat material on site. It also provides advice on how to publish peat surveys as part of wider site investigations for development management applications, with a particular focus on wind farm developments.

The parameters used to determine the characteristics of the peat materials are outlined below.

## i. Surface firmness estimation

An average man standing on one foot applies a pressure to the ground of between 5 and 6 lbs / p.s.i. and this fact is used to estimate the bearing capacity. The following symbols are used to denote the pressure the ground will stand.

Firmness of surface (P)

PO = Surface too soft to walk on

- P1 = Surface just passable
- P2 = Surface fairly firm
- P3 = Surface firm

### ii. Observations on the vegetation

The Site is largely surrounded by commercial forestry plantations at varying stages of development and will require felling prior to the beginning of construction. The Temporary Works Area and proposed access tracks are situated in a previously felled area adjacent to the existing Crossaig Substation.

#### iii. Observations on the peat

### a. Botanical observations

Botanical observations of peat samples identified that Carex species are likely to make up a significant proportion of the organic material in the lower horizons where catotelmic peat is typically found.

### b. Degree of humification - von POST SCALE

The degree of humification of peat samples is estimated in the field according to the method devised by the Swedish botanist L. von Post by squeezing a small amount of peat in the hand and the water and / or peat exuded indicates, by its colour and consistency, the degree to which the peat has undergone humification or, more correctly, a type of decomposition which includes breakdown under anaerobic conditions. The von Post scale ranges from 1 to 10, the higher the number the higher the degree of humification. The full scale is as follows:

Von Post Scale (H)					
H1	Completely undecomposed peat free of amorphous material. On squeezing, clear				
	colourless water is pressed out.				



H2	Nearly undecomposed peat, free of amorphous material, yielding only yellowish brown water on pressing.
H3	Very slightly decomposed peat, containing a little amorphous material. On squeezing, muddy brown water but no peat passes between the fingers. Residue is not pasty.
H4	Slightly decomposed peat containing some amorphous material. Strongly muddy brown water but no peat passes between the fingers. Residue is somewhat pasty.
H5	Moderately decomposed peat containing a fair amount of amorphous material. Plant structure recognisable though somewhat vague. On squeezing, some peat but mainly muddy water issues. Residue is strongly pasty.
H6	Moderately decomposed peat with a fair amount of amorphous material and indistinct plant structure. On pressing, about one third of the peat passes between the fingers. Residue is strongly pasty, but shows the plant structure more distinctly than in unsqueezed peat.
H7	Strongly decomposed peat with much amorphous material and faintly recognisable plant structure. On squeezing, about one half of the peat is extruded. The water is very dark in colour.
H8	Strongly decomposed peat with much amorphous material and very indistinct plant structure. On squeezing, two thirds of the peat and some water passes between the fingers. Residue consists of plant tissues capable of resisting decomposition (roots, fibres, wood, etc.).
H9	Practically fully decomposed peat with almost no recognisable plant structure. Nearly all the peat squeezed between the fingers as a uniform paste.
H10	Completely decomposed peat with no discernible plant structure. On squeezing, all the peat, without water, passes between the fingers.

#### iv. Fibre

The fibre content of each peat sample is estimated visually and the amounts of the two types (classified 'fine' or 'coarse') are noted on a scale ranging from 0 to 3 as shown below.

Fine fibres, mainly derived from *Eriophorum spp*. (F)

FO = NII

FI = Low content

- F2 = Moderate content
- F3 = High content

Coarse fibres, mainly rootlets (R)

R0 = NiI

RI = Low content

R2 = Moderate content

R3 = High content

## v. Wood

Wood remains, especially if they are large and resistant, may conceivably cause a certain amount of difficulty during the exploitation of a bog. An attempt is therefore made when sampling to assess the extent of wood. It is estimated on a scale ranging from 0 to 3 as detailed below.

Wood remains (W) W0= Nil



WI = Low content W2 = Moderate content W3 = High content

### vi. Other observations

When peat is freshly sampled and before it darkens by oxidation, note is taken of its colour, stratification, the presence of visible mineral matter and any other features of interest.

Photographs of the peat cores obtained from Crossaig along with information relating to the parameters outlined above are presented overleaf with a summary of the information gathered during the peat coring process presented in the main body of text of the Peat Slide Risk Assessment (PSRA).

It was noted during sampling that the water table at sample 1 was 0.3 m below the surface and that sample 2 had a high water content.



Core 1					
Core Samples	Detail	Surrounding Environment			

Location	Depth (m)	Firmness of Surface (P)	Von Post (H)	Fine Fibres (F)	Coarse Fibres (R)	Wood Remains (W)	Other Observations (Colour)
E 18255, N 650413	0.00 – 0.50	2	3	2	3	1	Dark Brown
	0.51 – 1.00		4	2	2	2	Dark Brown
	1.01 – 1.50		5	1	2	2	Dark Brown
	1.51 – 2.00		6	2	1	1	Dark Brown



Core 2					
Core Samples	Detail	Surrounding Environment			

Location	Depth (m)	Firmness of Surface (P)	Von Post (H)	Fine Fibres (F)	Coarse Fibres (R)	Wood Remains (W)	Other Observations (Colour)
E 182671, N 650128	0.00 – 0.50	3	4	2	3	1	Brown
	0.51 – 1.00		4	3	2	1	Brown
	1.01 – 1.50		6	3	1	1	Dark Brown
	1.51 – 2.00		7	3	1	1	Dark Brown