

Annex P - Peat Slide Risk Assessment (PSRA)

February 2023





**CROSSAIG SUBSTATION
ENVIRONMENTAL APPRAISAL**

PEAT LANDSLIDE HAZARD AND RISK ASSESSMENT

FEBRUARY 2023



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1 INTRODUCTION

1.1 Background

Arcus Consultancy Services Ltd (Arcus) was commissioned by SSEN Ltd (the Applicant) to carry out a Peat Landslide Hazard and Risk Assessment (PLHRA) for the proposed Crossaig Substation, Temporary Works Area (TWA), Sustainable Urban Drainage System (SUDS) attenuation pond and permanent access tracks (the Development) as part of the Argyll and Kintyre 275 kV Substations Upgrade located approximately 18 kilometres (km) south of Tarbert and 12 km north of Carradale on the eastern coast of the Kintyre peninsula (the Site).

The Development will be subject to Town and Country Planning, while the OHL Tie-In, temporary Diversion Towers and Temporary Works Area (hereby known as the Associated Development) will be submitted for Section 37 consent. The Site Layout Plan is shown on **Figure 1 in Appendix A**.

It should be noted that the Project's construction schedules will be aligned. Therefore, peat excavation and re-use will be considered within the wider scope of the Project.

This PLHRA has been prepared to inform Argyll & Bute Council (ABC) and statutory consultees of the prevalence of peat across the Proposed Development and Associated Development as well as highlighting any potential risk of peat slide.

This PLHRA has been undertaken to Scottish Government Guidance 'Proposed electricity generation developments: peat landslide hazard best practice guide'¹.

The PLHRA is accompanied by the following appendices:

- Appendix A: Figures;
- Appendix B: Site Photographs;
- Appendix C: Hazard Rank Calculations, and;
- Appendix D: Peat Coring Records.

1.2 The Development

The Development will consist of the following key infrastructure:

- Substation (approx. 184 m x 129 m) ;
- Two Pylon Towers at least 43 m in height to make the connection into and out of the proposed substation;
- Four temporary Diversion Towers to divert the electricity transmission from the existing substation during construction phase of the Development;
- Temporary Work Area (approx 300 m x 120 m);
- A Sustainable Urban Drainage System (SUDS) Attenuation Pond (approximately 80 m x 30 m);
- Permanent access track, approximately 660 m in length to the new access track between the existing Crossaig substation and the proposed Crossaig North substations and for access to the SuDS pond; and
- An extension to the south of the substation platform at the existing Crossaig substation of (approx 17.5m x 30m) to support electrical equipment and associated access.

The Site Layout is shown on **Figure 1 in Appendix A**.

¹ Scottish Government (2017) Proposed electricity generation developments: peat landslide hazard best practice guide [Proposed electricity generation developments: peat landslide hazard best practice guide - gov.scot \(www.gov.scot\)](https://www.gov.scot/publications/proposed-electricity-generation-developments-peat-landslide-hazard-best-practice-guide/pages/1-1-introduction.aspx) (Accessed 02/08/2022)

1.3 Scope and Purpose

The scope of this PLHRA is to:

- Review available desk-based information on the Site;
- Undertake a site walkover survey and peat probe surveys to characterise the prevailing ground conditions and identify existing or potential peat instability;
- Report on the findings of the survey and assess the potential instability risk and estimate the hazard from any potential peat slide; and
- Recommend mitigation measures and specific construction methodologies that should be considered during the construction period, if required.

This PLHRA provides factual information on the peat survey results relating to the proposed infrastructure locations. The desk-based information and site surveys have been utilised to assess the potential risk of any peat slide. The methodology adopted, and details on the assessment, are outlined in **Sections 3, 4 and 5** of this PLHRA. The assessment has been undertaken in accordance with Scottish Government Guidance in assessing the likelihood, and consequence, of peat slide².

1.4 Project Team

Team Member	Job Title	Qualifications	No. Years Experience
Gregor Hirst	Senior Engineer	BSc (Hons)	6 Years
David Ballentyne	Principal Engineer	BSc (Hons)	18 Years
Tomos Ap Tomos	Technical Director	BEng (Hons) MCIHT	25 Years

This assessment was undertaken by Gregor Hirst (BSc Hons), a Geo-Environmental Engineer of 6 years, and was supported by David Ballentyne a Geo-Environmental Civil Engineer with for over 18 years of experience in ground condition assessment. This Chapter has been technically reviewed by Tomos Ap Tomos, Technical Director of Engineering.

² Scottish Government (2017): Peat Landslide Hazard and Risk Assessments: Best Practice Guide for Proposed Electricity Generation Developments; Second Edition, April 2017 [Online]. Available at: <https://www.gov.scot/binaries/content/documents/govscot/publications/advice-and-guidance/2017/04/peat-landslide-hazard-risk-assessments-best-practice-guide-proposed-electricity/documents/00517176-pdf/00517176-pdf/govscot%3Adocument/00517176.pdf> (Accessed 02/08/2022)

2 SITE INFORMATION AND DESK STUDY

2.1 Site Description and Topography

The land within the site boundary (the Site) which contains the Development is located approximately 18 kilometres (km) south of Tarbert, covering an area of approximately 80 hectares (ha) centred on National Grid Reference (NGR) 182545, 650307. The Site is located within the administrative boundary of Argyll & Bute Council (the Council). The Site is adjacent to the existing Crossaig Substation which connects to the B842 from the east.

The topography of the Site and immediate vicinity is gently undulating throughout. The elevation of the Site ranges from around 80 metres (m) Above Ordnance Survey Datum (AOD) to around 96 m AOD in the area of the proposed substation.

There are a number of unnamed surface water features, mainly in the form of drainage channels associated with the forestry plantation, however no watercourses are recorded other than Allt na Buaille Salaich, which runs along the south western Project boundary and is the receptor for the proposed SUDS outfall.

The predominant land use within the Site consists of commercial forestry plantation.

2.2 Site Walkover

The purpose of the desk study and site visit was to gain a thorough understanding of site conditions including topography, geology, existing peat instability and hydrology. The outcome of this stage of the study was to determine which areas required detailed intrusive survey (by peat probing) and ultimately provide data for the assessment of PLHRA.

A site walkover was undertaken in November 2021 prior to the commencement of the peat probing exercise. The Site was examined for evidence of peatlands, presence of landslip and localised haggling. Geological mapping and areas of interest were pre-loaded to a handheld device for reference during the site walkover. Following a review of these in parallel with the initial site walkover, the desk study aimed to identify and or verify the following:

- The general condition of peat deposits;
- Evidence of any previous peat instability;
- The presence of low lying wet/peat lands; and
- Watercourses and potential other receptors.

2.2.1 Site Conditions

The entirety of the Site is utilised for forestry plantations, other than the area of the proposed temporary works area, adjacent to the south of the existing Crossaig substation. This area contains a mixture of upfilled land that has been engineered to act as a working platform with an access track running through it, while the remainder of the area has been subject to felling and currently comprises open hummocky ground. Within the plantation area there are a number of forestry rides and clearings which were noted to contain sphagnum and high groundwater levels, resulting in areas of soft ground.

Extensive felling has recently been undertaken in the area north and east of the proposed substation, associated with the ongoing infrastructure works in the area.

Neither mining or quarry activities are known to have taken place at the Site.

Site photographs taken during the site walkover are included in **Appendix B**.

2.3 Published Geology

2.3.1 Superficial Soils

Available British Geological Survey (BGS)³ indicates an absence of superficial deposits across the majority of the Site. The exception being the presence of glacial deposits in the form of Devensian Till which are recorded at the northern extent of the Site.

Figure 2 illustrates the 'Superficial Soils' map included in **Appendix A**.

2.3.2 Solid Geology

Published bedrock geology mapping information on solid geology indicates the entirety of the Site to be underlain by Gritty Psammite and Pelite of the Beinn Bheula Schist Formation.

No geological faults or linear features are present at the Site or in the surrounding area.

Figure 3 illustrates the 'Solid Geology' included in **Appendix A**.

2.4 Hydrology and Hydrogeology

The Site is characterised by its generally low-gradient topography, but the area surrounding the Site has a more variable landscape in terms of topography. The Site lies within the Kintyre Coastal catchment that is mainly drained by a river, the Crossaig Water.

Crossaig Water passes to the north of the Site and flows in an eastern direction. This watercourse has a Scottish Environment Protection Agency (SEPA) overall classification⁴ of 'Good'. There are several smaller watercourses located on the Site that drain either directly to the Firth of Clyde, or into Crossaig Water.

Initial desk-based review indicated the Site is likely to be partially underlain by peat with significant quantities of pockets of deep peat in isolated areas.

The SEPA Aquifer Classification Map of Scotland⁵ reveals that the Site is situated within an area underlain by a low productivity aquifer where flow is virtually all through fractures and other discontinuities.

The SEPA River Basin Management Plan Interactive Map reveals that the Site is underlain by the Oban and Kintyre groundwater body. This groundwater body is classified by SEPA under the Water Framework Directive⁶ as having a status of Good.

Figure 4 illustrates the Geomorphology of the Site and is included in **Appendix A**.

2.5 Historical Landslip and Geomorphology

No evidence of historic landslip or peat haggings was noted during the Site walkover and topsoil, where undisturbed, generally appeared to be in good condition. Due to the presence of extensive forestry plantations at the Site; it is considered that properties of the peat deposits may have been altered and may not pose the same risk of instability as undisturbed peat. Nonetheless, the possibility of instability within peat soils cannot be discounted, especially where there are significant topographic variances and the presence of watercourses.

³ British Geological Survey (2019) Geology of Britain [Online] Available at: <http://mapapps.bgs.ac.uk/geologyofbritain/home.html> (Accessed 03/08/2022)

⁴ SEPA Water Classification Hub (2020) [Online] Available at: [Water Classification Hub \(sepa.org.uk\)](http://www.sepa.org.uk/water-classification-hub) (Accessed 03/08/2022)

⁵ Scotland's Environment (2019) SEPA Aquifer Classification Map of Scotland [Online] Available at: <https://map.environment.gov.scot/sewebmap/> (Accessed 03/08/2022)

⁶ European Parliament (2000) Directive 2000/60/EC [Online] Available at: https://eur-lex.europa.eu/resource.html?uri=cellar:5c835afb-2ec6-4577-bdf8-756d3d694eeb.0004.02/DOC_1&format=PDF (Accessed 03/08/22)

3 SITE SURVEYS AND RESULTS

3.1 Investigations

The existing peat depths across the Site have been determined through a multi-phased peat probe survey undertaken as recommended in the NatureScot (formally Scottish Natural Heritage), Scottish Government and James Hutton Institute guidance for investigating peat⁷.

The probe positions for the survey were determined by the proposed layout of the Development and provided detailed information across the various proposed infrastructure at frequencies as follows:

- Substation – 10 m x 10 m grid to the extent of the proposed footprint;
- Pylon Locations – 10 m x 10 m grid to an area of 50 m²;
- Temporary Works Area – 25 m x 25 m grid; and
- Tracks – Every 50 m along the centreline with perpendicular offsets, 15-25 m either side.

It should be acknowledged that natural variations in peat depth/thickness could occur between probe positions, although areas of infrastructure had undergone intensely spaced probing and this would be less likely.

3.2 Summary of Peat Depths

Throughout the peat survey, a total of 714 probes were progressed. The average peat depth across the Site is 0.40 m with greater than 77% of probes recording peat depths of 0.5 m or less and 91% recording depths of 1.0 m or less. Thick peat (where the depth was greater than >1.0 m) was recorded at 9% of locations. The majority of thick peat was recorded at depths between 1.0 m – 2.0 m with only 1.3% of all probes recording depths in excess of 2.0 m.

The maximum peat depth recorded at the Site was 3.2 m within a clearing between trees not utilised within the commercial plantation. Topographically the area is relatively flat and surface vegetation in the form of sphagnum and high groundwater levels were recorded. The area is located between the proposed substation and the first proposed pylon location to the north of the proposed substation, therefore there is no proposed infrastructure in this area.

Table 1 summarises the recorded peat depths.

Table 1: Peat Depth Summary

Peat Depth Range (m)	Nº of Peat Probes	Percentage of Total
0.00 - 0.50	551	77.17
0.51 - 1.00	99	13.87
1.01 - 1.50	39	5.46
1.51 - 2.00	16	2.24
2.01 - 2.50	5	<1.0
2.51 - 3.00	3	<1.0
3.01 - 3.50	1	<1.0
Σ =	714	

⁷ Scottish Government, Scottish Natural Heritage, SEPA (2017) Peatland Survey. Guidance on Developments on Peatland, on-line version only. Available at: [Guidance+on+developments+on+peatland+--+peatland+survey+-+2017.pdf \(www.gov.scot\)](https://www.gov.scot/resources/consultation-papers/collections/documents/Guidance-on-developments-on-peatland-+-+peatland-survey-+-+2017.pdf) Accessed (03/08/2022)

The peat probe locations and depths are shown on **Figure 5** appended with this PLHRA, and details of probe records are included in **Appendix C**.

The Interpolated Peat Depths are illustrated on **Figure 6**.

4 GUIDANCE AND METHODOLOGY

4.1 Overview of Guidance and Peat Failure Mechanisms

4.1.1 Peat Depth and Slope

The Scottish Government guidance divides peat instability into two categories: 'peat slides' and 'bog bursts'. The guidance states that peat slides have a greater risk of occurrence in areas where:

- Peat is encountered at or near to ground surface level;
- The thicknesses are recorded in the region of 2.0 m (above which, in general terms, peat instability would increase with peat thickness); and
- The slope gradients are steep (between 5° and 15°).

Bog bursts are considered to have a greater risk of occurrence in areas where:

- Peat depth is greater than 1.5 m; and
- Slope gradients are shallow (between 2° and 10°).

It should be noted however that peat instability events, although uncommon, can occur out with these limits. Reports of bog bursts are generally restricted to the Republic and Northern Ireland.

Further to the general guidance above, in relation to peat depth, it is considered that the extent and depth of peat is controlled to a degree by rainfall and elevation, giving rise to three common types of peat (Boylan et al. 2008⁸):

- Upland Blanket Bog: Blanket bogs are typically about 3 m thick however, they can be up to 5 m thick. Generally thinning at greater elevations;
- Raised Bog: Raised bogs generally tend to be 3-12 m thick, averaging 7 m with their growth occurring above the water table; and
- Lowland Blanket Bog: Much the same as the upland version; however, they form around sea level in areas of very high rainfall.

Generally, the potential for peat instability increases with peat depth, however other instability indicators need to be considered, namely slope and substrate.

4.1.2 Substrate

Peat slide failures tend to occur at the interface of the peat and underlying substrate therefore, understanding the nature of the underlying substrate can provide a key factor when considering the risk stability.

Using the peat probe refusal, an estimation of the underlying materials can be determined based on:

- Gradual refusal – Clay;
- Crunching/Gritty – Weathered Rock/Sand and Gravel; or
- Abrupt Refusal/Hard – Rock.

Where sand and/or gravel is recorded, the interface is considered to be the best-case scenario with the highest friction value.

Where clay is recorded, the upper horizons of the clay are typically softened through poor drainage in this soil group with low shear strengths expected. While rock substrate provides a high strength, the surface being smooth can lead to a weak interface, with similar risk to that of a clay substrate.

⁸ Boylan et al (2008) Peat Slope Failure in Ireland

The presence of slip material, or evidence of peat instability would represent the worst-case scenario for the assessment of substrate.

The substrate parameters are included in the Hazard and Exposure Assessment in **Section 5** of this PLHRA.

4.1.3 Other Considerations

Preparatory factors which effect the stability of peat slopes in the short to medium-term include:

- Loss of surface vegetation (deforestation);
- Changes in sub-surface hydrology;
- Increase in the mass of peat through accumulation, increase in water content and growth of tree planting; or
- Reduction in shear strength of peat or substrate due to chemical or physical weathering, progressive creep and tension cracking.

Triggering factors which can have immediate effect on peat stability and act on susceptible slopes include:

- Intensive rainfall or snow melt causing pressures along existing or potential peat/substrate interfaces;
- Snow melt;
- Alterations to drainage patterns, both surface and sub-surface;
- Peat extraction at the toe of the slope reducing the support of the upslope material;
- Peat loading (commonly due to stockpiling) causing an increase in shear stress; and
- Earthquakes or rapid ground accelerations such as due to blasting or mechanical movement.

Consideration of peat stability should form an integral part of the design and construction of infrastructure in peatland areas. While peat does not wholly provide a development constraint, areas of deep peat or peat deposits on steep slopes should be either avoided through design and micro-siting; or mitigation measures should be designed to avoid instability and movement.

4.2 Methodology

Despite being an application under the Town and Country Planning (Scotland) Act 1997⁹, the PLHRA has been carried out in accordance with the Energy Consents Unit, Scottish Government guidance of 2017 titled Peat Landslide Hazard and Risk Assessments - Best Practice Guide for Proposed Electricity Generation Developments¹⁰.

In June 2014, Scottish Planning Policy¹¹ (SPP) and National Planning Framework (NPF3)¹² were published. In relation to peat and the assessment of effects on resource, NPF3 references SNH Scotland's National Peatland Plan¹³. These policy, framework and guidance documents are considered in this PLHRA. The PLHRA undertaken is based on:

- Desk based assessment;
- Site Walkover;

⁹ Scottish Government (1997) Town and Country Planning (Scotland) Act 1997 [Online] Available at: <http://www.legislation.gov.uk/ukpga/1997/8/contents> (Accessed 20/08/22)

¹⁰ Scottish Government (2017) Peat Landslide Hazard and Risk Assessment: Best Practice Guide for Proposed Electricity Generation Development [Online] Available at: <https://www.gov.scot/Publications/2017/04/8868> (Accessed 20/08/22)

¹¹ Scottish Government (2014) Scottish Planning Policy [Online] Available at: <http://www.scotland.gov.uk/Topics/Built-Environment/planning/Policy> (Accessed 20/08/22)

¹² Scottish Government (2014) National Planning Framework 3 [Online] Available at: <http://scotland.gov.uk/Resource/0045/00453683.pdf> (Accessed 20/08/22)

¹³ SNH (2015) Scotland's National Peatland Plan [Online] Available at: <https://www.nature.scot/climate-change/taking-action/carbon-management/restoring-scotlands-peatlands/scotlands-national-peatland-plan> (Accessed 20/08/22)

- Infrastructure specific probing; and
- A hazard and risk ranking assessment.

The area of the Site subject to assessment was determined by the proposed development layout which considered both anticipated peat deposits as well as other physical and environmental constraints.

4.2.1 Development of Hazard Rank

The early stages of the PLHRA including the desk study, site visit and peat probing were carried out in parallel with the assessment of wider constraints to inform the layout of the Development. Following identification of peat depths within the Site, the assessment has determined the potential effects on the peat resource from construction activities which would include:

- Construction of tracks;
- Foundation construction;
- Construction of hardstanding; and
- Temporary storage of peat and soils.

An assessment of the peat probing data and a review against desk study information was undertaken and a hazard rank was calculated for different zones across the site reflecting risk of peat instability/constraint to construction.

Where practical, the Development design would be progressed to avoid areas of a risk score above 'low'. Where this has would not be achievable, areas affected would be discussed in both the EIA as having significant effect, with relative mitigation measures proposed to reduce this, and recorded on a risk register which sets out specific mitigation measures which are considered necessary to reduce the risk of inducing instability.

Details of the hazard and risk ranking assessment is included in **Sections 5 and 6** of this PLHRA.

5 HAZARD AND EXPOSURE ASSESSMENT

5.1 Background

A 'Hazard Ranking' system has been applied across the Site based on the analysis of risk of peat slide as outlined in the Scottish Government guidance. This is applied on the principle:

$$\text{Hazard Ranking} = \text{Hazard} \times \text{Exposure}$$

Where 'Hazard' represents the likelihood of any peat slide event occurring and 'Exposure' being the impact or consequences that a peat slide may have on sensitive receptors that exist on and around the Site.

5.2 Methodology

The determination of Hazard and Exposure values is based on a number of variables which impact the likelihood of a peat slide (the Hazard), and the relative importance of these variables specific to the Site.

Similarly, the consequences or Exposure to receptors is dependent on variables including the particular scale of a peat slide, the distance it will travel and the sensitivity of the receptor.

In the absence of a predefined system, the approach to determining and categorising Hazard and Exposure is determined on a Site by Site basis. The particular system adopted for the Development PLHRA assessment is outlined in the following sub sections.

5.3 Hazard Assessment

The potential for a peat slide to occur during construction depends on several factors, the importance of which can vary from Site to Site. The factors requiring considerations would typically include:

- Peat depth;
- Slope gradient;
- Substrate material;
- Evidence of instability or potential instability;
- Vegetation cover; and
- Hydrology.

Of these, peat depth and slope gradient are considered to be principal factors. Without a sufficient peat depth and a prevailing slope, peat slide hazard would be negligible.

The Slope Gradient has been established using a Digital Terrain Model (DTM) to a resolution of 5 m, which is illustrated on **Figure 7**. For the Development and Associated Development, the substrate material is also considered a relevant factor in relation to slide.

Vegetation cover and evidence of instability or potential instability were assessed during site surveys and, alongside satellite photography, informed the Geomorphology Map presented in **Figure 4**. This information was also considered during the adoption of hazard zones across the Site, which are presented in **Figure 9: Hazard Rank Zonation Plan**.

Due to the nature of the assessment and number of data points used to establish hazard ranking, gathering hydrological data at each probe point through the use of groundwater boreholes and a subsequent monitoring period is considered impractical. Therefore, an assumption on groundwater levels has been adopted for the assessment that 90% of the

peat at each probe location is below the water table. As such, it is assumed that the water table across the Site is relatively high.

5.4 Hazard Rating

When several factors may impact on the Hazard potential, a relative ranking process is applied attributing different weighting to each factor as shown below.

Table 2: Coefficients for Slope Gradients

Slope Angle (degrees)	Slope Angle Coefficients
Slope < 2°	1
2° < Slope < 4°	2
4° < Slope < 8°	4
8° < Slope < 15°	6
Slope >15°	8

Table 3: Coefficients for Peat Thickness and ground conditions

Peat Thickness	Ground Conditions Coefficients
Peaty or organic soil (<0.5 m)	1
Thin Peat (0.5 – 1.0 m)	2
Deep Peat (>1.0 m)	3*
Deep Peat (>3.0 m)	8

* - Note that thicker peat generally occurs in areas of shallow gradient and records and research indicate that thick peat does not generally occur on the steeper gradients.

Table 4: Coefficients for Substrate

Substrate Material	Substrate Coefficients
Sand/gravel	1
Rock	1.5
Clay	2
Not proven	2
Slip material (Existing materials)	5

The Hazard Rating Coefficient for a particular location is calculated using the following equation:

$$\text{Hazard Rating Coefficient} = \text{Slope Gradient} \times \text{Peat Thickness} \times \text{Substrate}$$

From the Hazard Rating Coefficient, the risk to stability can be ranked as set out in **Table 5**.

Table 5: Hazard Rating

Hazard Rating Co-efficient	Potential Stability Risk (Pre-Mitigation)
<5	Negligible
5 to 15	Low
16 to 30	Medium
31 to 50	High

> 50	Very High
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5.5 Peat Stability Assessment

The likelihood of a particular slope or hillside failing can be expressed as a Factor of Safety. For any potential failure surface, there is a balance between the weight of the potential landslide (driving force or shear force) and the inherent strength of the soil or rock within the hillside (shear resistance).

The guidance states that the 'Infinite Slope' method of analysis, after Skempton and DeLory (1957), is the most well established and commonly applied method for the assessment of peat slope stability. The stability of a slope can be assessed by calculating the factor of safety F , which is the ratio of the sum of resisting forces (shear strength) and the sum of the destabilising forces (shear stress):

$$F = \frac{c' + (\gamma - m\gamma_w)z \cos^2 \beta \tan \phi'}{\gamma z \sin \beta \cos \beta}$$

Where c' is the effective cohesion, γ is the bulk unit weight of saturated peat, γ_w is the unit weight of water, m is the height of the water table as a fraction of the peat depth, z is the peat depth in the direction of normal stress, β is the angle of the slope to the horizontal and ϕ' is the effective angle of internal friction. Values of $F < 1$ indicate a slope would have undergone failure under the conditions modelled; values of $F > 1$ suggest conditions of stability.

Assumed geotechnical parameters have been utilised in the formula to inform the stability assessment, based on literature values to inform the stability analysis, as included in **Table 6**.

Table 6: Literature for Geotechnical Parameters of Peat

Reference	Effective Cohesion C' (kPa)	Effective Angle of Friction ϕ (°)	Unit Weight γ (kN/m ²)	Comments
Hanrahan et al (1967) ¹⁴	5.5 – 6.1	36.6 - 43.5	-	Remoulded H4 Sphagnum peat
Hollingshead and Raymond (1972) ¹⁵	4.0	34	-	-
Hollingshead and Raymond (1972)	2.4 – 4.7	27.1 – 35.4	-	Sphagnum peat (H3, mainly fibrous)
Carling (1986) ¹⁶	6.52	0	10	-
Kirk (2001) ¹⁷	2.7 – 8.2	26.1 – 30.4		Ombrotrophic blanket peat

¹⁴ Hanrahan et al (1967) - Hanrahan, E.T., Dunne, J.M., and Sodha, V.G. 1967. Shear strength of peat. Proceedings Geotechnical Conference, Oslo, Vol. 1, pp. 193–198.

¹⁵ Hollingshead and Raymond (1972) - Hollingshead, G.W., and Raymond, G.P. 1972. Field loading tests on Muskeg, Canadian Geotechnical Journal, 9(3): 278–289.

¹⁶ Carling (1986) - Peat slides in Teesdale and Weardale, northern pennines, July 1983: Description and failure mechanisms

¹⁷ Kirk (2001) - Initiation of a multiple peat slide on Cullcagh Mountain, Northern Ireland

Warburton et al (2003) ¹⁸	5.0	23	9.68	Basal Peat
Warburton et al (2003)	8.74	21.6	9.68	Fibrous Peat
Dykes and Kirk (2006)	3.2	30.4	9.61	Acrotelm
Dykes and Kirk (2006)	4.0	28.8	9.71	Catotelm

C' – effective cohesion (kPa), typically ranging from 2.5 to 8.5 therefore 5.0 has been adopted for the purposes of the assessment.

ϕ – effective angle of friction ($^{\circ}$), typically ranging from 21.6 to 43.5 therefore 29.6 has been adopted for the purposes of the assessment.

γ – unit weight (kN/m²), typically ranging from 9.61 to 10, therefore 10 has been adopted for the purposes of the assessment.

In accordance with the best practice method, F values of <1.0 indicate slopes that would experience failure under the modelled conditions and as such are considered areas of high risk. However, Boylan et al (2008) indicate that a relatively high value of F=1.4 should be used to identify slopes with the potential for instability. Adopting this approach, high risk areas are indicated where F is <1.0, medium risk areas are indicated as 1.01 to 1.50 and >1.5 are low risk.

Using digital terrain modelling and GPS co-ordinates of each peat probe, a factor of Safety, F has been calculated for each probe locations which has been interpolated through ArcGIS Spatial Analyst tools. The Factor of Safety Assessment provides a sense check of the ranking based system, providing an absolute approach to the 'Factor of Safety Plan' is shown on **Figure 8**.

The results of the Factor of Safety calculations indicated all points on the Site as low risk. This was primarily due to the light undulating topography and generally flat-lying conditions on the Site combined with generally shallow peat depths across the Site.

5.6 Exposure Assessment

The main exposure receptors identified at the Site and in the surrounding areas which could potentially be affected in the event of a peat slide are the existing Crossaig Substation, located adjacent to the Site to the east, the proposed development, private dwellings located approximately 200 m north east of the northernmost temporary tower and various unnamed watercourses that flow within the Site boundary before joining the Firth of Clyde to the east.

The impact of a peat slide on receptors can be assessed on a relative scale based on the potential for loss of habitat, a historical feature or disruption/danger to the public. To effectively assess the impact, the assessment of Exposure effect must also consider the distance between the hazard and the receptor, and the relative elevation between the two.

5.7 Exposure Rating

Similar to the Hazard Rating, the Exposure Ratings were determined using relative ranking process by attributing the different weighting systems to each factor as shown below:

¹⁸ Warburton et al (2003) - Anatomy of a Pennine peat slide, Northern England

Table 7: Coefficients for Receptor Type

Receptor	Receptor Coefficients
Road, path or track	3
Minor water feature	6
Site infrastructure	6
Dwelling	8
Major water feature	8
Blanket bog	8

Table 8: Coefficients for Distance from Receptor

Distance from Receptor	Distance Coefficients
> 1 km	1
100 m to 1 km	2
10 m to 100 m	3
<10 m	4

Table 9: Coefficients for Receptor Elevation

Receptor Elevation	Elevation Coefficients
< 10 m	1
10 m to 50 m	2
50 m to 100 m	3
> 100 m	4

The Exposure Rating Coefficient for a particular location is calculated using the following equation:

$$\text{Exposure Rating Coefficient} = \text{Receptor} \times \text{Distance} \times \text{Elevation}$$

From the Exposure Rating Coefficient, the risk to stability can be ranked as set out in **Table 10**.

Table 10: Exposure Rating

Exposure Rating Co-efficient	Potential Stability Risk (Pre-Mitigation)
<6	Very Low
6 to12	Low
13 to 24	High
24 to 30	Very High
>30	Extremely High

5.8 Rating Normalisation

In order to achieve an overall Hazard Ranking in accordance with the Scottish Government Guidance, the Hazard and Exposure Rating Coefficient derived from the coefficient tables are normalised as shown in **Table 11**.

Table 11: Rating Normalisation

Hazard Rating		Exposure Rating	
Current Scale	Normalised Scale	Current Scale	Normalised Scale
< 5 Negligible	1	<6 Very Low	1
5 to 15 Low	2	6 to 12 Low	2
15 to 30 Medium	3	13 to 24 High	3
30 to 50 High	4	25 to 30 Very High	4
>50 Very high	5	>30 Extremely High	5

The record of the Hazard Rank Assessment is included in **Appendix C** of this PLHRA.

6 HAZARD RANKING

Having identified the rating coefficients in **Section 5** of this PLHRA, it is possible to categorise areas of the Site with a Hazard Ranking by multiplying the Hazard and Exposure Rating. Hazard Ranking and associated suggested actions matrix are shown in **Tables 12 and 13** below:

Table 12: Hazard Ranking and Suggested Actions

Hazard Ranking		Action Suggested in the Scottish Executive Guidance
17-25	High	Avoid project development at these locations.
11-16	Medium	Project should not proceed unless hazard can be avoided or mitigated at these locations, without significant environmental impact, in order to reduce hazard ranking to low or less
5-10	Low	Project may proceed pending further investigation to refine assessment. Mitigation of hazards maybe required through micro-siting or re-design at these locations.
1-4	Negligible	Project should proceed with monitoring and mitigation of peat landslide hazards at these locations as appropriate.

Table 13: Hazard Ranking Matrix

Hazard Rating	5	Low	Low	Medium	High	High
	4	Negligible	Low	Medium	Medium	High
	3	Negligible	Low	Low	Medium	Medium
	2	Negligible	Negligible	Low	Low	Low
	1	Negligible	Negligible	Negligible	Negligible	Low
		1	2	3	4	5
		Exposure Rating				

Receptor exposure was assessed for each of the seven hazard zones using the approach in **Section 5**. A summary of the Hazard Ranking result for each identified area is summarised in **Table 14** and is presented in **Figure.9** - Hazard Ranking Zonation Plan. The zonation is based on a combination of considerations including calculated hazard result, peat depth, topography and receptors and land uses.

7 SLIDE RISK AND MITIGATION

7.1 General

The PLHRA has shown the Site to be generally of ‘negligible’ hazard ranking, with isolated areas of ‘low’ hazard ranking. No Medium or High risk areas have been identified within the Proposed Development or Associated Development and therefore a significant risk of peat slide is not considered to be present based on the Hazard Ranking assessment. Nonetheless, a risk from peat slide may still exist and mitigation measures as outlined in **Section 7.3** of this PLHRA should be applied to minimise any risk.

Where the hazard ranking has been lowered through mitigation measures, the original ranking will remain in the overall hazard zoning plan. It should be acknowledged that the hazard zonation plan is based on the pre-mitigation status.

While specific recommended mitigation in ‘low’ ranked areas are proposed, other mitigation is embedded in the design. It is also necessary for detailed design and construction of the Proposed Development and Associated Development to be undertaken in a competent and controlled manner and in line with best practice measures, specifically relating to the management and reuse of excavated peat.

The embedded mitigation and good practice measures are set out in **Section 7.2** and **Section 7.3** of this PLHRA. It should be noted that the mitigation measures defined are not exclusive and other forms of mitigation may well be required and should be implemented during construction of the Proposed Development and Associated Development.

Table 14: Hazard Ranking

Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
Hazard Area	Infrastructure Affected	Ranking	Key Aspects	Specific Actions	Ranking
H1	Proposed temporary works area, SUDS attenuation pond and proposed permanent access track	Negligible	Location and topography: Southern and eastern sectors of the Proposed Development. Indicated by the Indicative Town & Country Planning Boundary in Figure 9 within Appendix A . Hydrology: None Peat Depth: 0.0 m – 3.0 m. Generally, <1.0 m Slope Gradient: 0° to >10° Exposure: Proposed infrastructure	Micro-siting in to areas of thinner peat where required. Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Annex N: Water Construction Environmental Management Plan (WCEMP) and management of peat and peaty soils as outlined in Annex O: Peat Management Plan (PMP) .	Negligible
H2	Proposed Substation	Negligible	Location and topography: Western and north western	Micro-siting in to areas of thinner	Negligible

Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
			<p>sectors of the Proposed Development comprising the southern two thirds of the proposed substation.</p> <p>Hydrology: None</p> <p>Peat Depth: 0.0 m – 2.1 m. Generally, <0.5 m</p> <p>Slope Gradient: 0° to <5°</p> <p>Exposure: Proposed Infrastructure</p>	<p>peat where required.</p> <p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Annex N: WCEMP and management of peat and peaty soils as outlined in Annex O: PMP.</p>	
H3	Proposed Substation	Low	<p>Location and topography: Small zone to the north of the Proposed Development containing the northern third of the proposed substation.</p> <p>Hydrology: None</p> <p>Peat Depth: 0.0 m – 3.0 m. Generally, <1.0 m</p> <p>Slope Gradient: 0° to <10°</p> <p>Exposure: Proposed Infrastructure</p>	<p>Micro-siting in to areas of thinner peat where required.</p> <p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Annex N: WCEMP and management of peat and peaty soils as outlined in Annex O: PMP.</p> <p>During construction visual inspections and monitoring in areas with the potential for peat slide risk should take place.</p>	Negligible
H4	Proposed indicative tower location, proposed OHL alignment and proposed permanent access track	Negligible	<p>Location and topography: Southern sector of the Associated Development, adjacent to the north of the Proposed Development.</p> <p>Hydrology: None</p>	<p>Micro-siting in to areas of thinner peat where required.</p> <p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Annex N: WCEMP and management of</p>	Negligible

Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
			<p>Peat Depth: 0.1 m – 3.2 m. Generally, <1.0 m</p> <p>Slope Gradient: 0° to <15°</p> <p>Exposure: Proposed infrastructure</p>	<p>peat and peaty soils as outlined in Annex O: PMP.</p>	
H5	Proposed OHL alignment	Low	<p>Location and topography: Central western sector of the Associated Development</p> <p>Hydrology: An unnamed watercourse runs from west to east through the zone</p> <p>Peat Depth: 0.1 m – 1.7 m. Generally, <1.0 m</p> <p>Slope Gradient: 0° to <10°</p> <p>Exposure: Proposed infrastructure</p>	<p>Micro-siting in to areas of thinner peat where required.</p> <p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Annex N: WCEMP and management of peat and peaty soils as outlined in Annex O: PMP.</p> <p>During construction visual inspections and monitoring in areas with the potential for peat slide risk should take place.</p>	Negligible
H6	Proposed indicative tower location, proposed OHL alignment and proposed permanent access track	Negligible	<p>Location and topography: Central eastern sector of the Associated Development</p> <p>Hydrology: An unnamed watercourse runs from west to east through the zone</p> <p>Peat Depth: 0.0 m - 0.3 m. Generally, <0.2 m</p> <p>Slope Gradient: 0° to <10°</p> <p>Exposure: Proposed infrastructure</p>	<p>Micro-siting in to areas of thinner peat where required.</p> <p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Annex N: WCEMP and management of peat and peaty soils as outlined in Annex O: PMP.</p>	Negligible

Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
H7	Proposed temporary towers	Negligible	<p>Location and topography: Eastern sector of the Associated Development</p> <p>Hydrology: An unnamed watercourse runs from south west to north east through the zone</p> <p>Peat Depth: 0.0 m - 1.5 m. Generally, <0.5 m</p> <p>Slope Gradient: 0° to <10°</p> <p>Exposure: Proposed infrastructure</p>	<p>Micro-siting in to areas of thinner peat where required.</p> <p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Annex N: WCEMP and management of peat and peaty soils as outlined in Annex O: PMP.</p>	Negligible

7.2 Embedded Mitigation

Embedded mitigation includes measures taken during design of the Development to reduce the potential for peat slide risk. In summary the principal measures that have been taken are:

- Locating infrastructure on shallower slopes, where possible; and
- Locating infrastructure on areas of shallow peat (or no peat) where possible.

7.3 Peat Slide Mitigation Recommendations

The following mitigation measures should be adopted post consent stage to validate the PLHRA and influence the detailed design of the Development, including:

- Ground investigations prior to detailed design;
- Identification of areas sensitive to changes in drainage regime prior to detailed design;
- Update the PLHRA as necessary following detailed ground investigations;
- Development of a drainage strategy that will not create areas of concentrated flow and will not affect the current peatland hydrology;
- Design of a Development drainage system for tracks and hardstanding that will require minimal ongoing maintenance during the operation of the windfarm;
- Inspection and maintenance of the drainage systems during construction and operation;
- Identification of suitable areas for stockpiling material during construction prior to commencement of works; and
- Consideration of specific construction methods appropriate for infrastructure in peat land (i.e. geogrids) as part of design Development.

8 CONCLUSIONS

This PLHRA has been undertaken for the Development in accordance with best practice, as detailed in **Section 4.2** of the PLHRA. The assessment included a desk study followed by completion of an intensive probing exercise across the proposed infrastructure and surrounding areas at the Proposed Development and Associated Development. The information gathered during this investigation was used to develop a Hazard Ranking across the Site.

The findings of the probing indicate that deep peat is present at the Site, however a vast majority of the Development is underlain by peat less than 1.0 m in thickness. Pockets of deep peat were recorded at up to 3.0 m in the southern area of the Proposed Development and up to 3.2 m in the southern area of the Associated Development.

Based on the scope of the study, the PLHRA has indicated that the majority of the Site is generally of 'negligible hazard ranking with two areas highlighted as 'low' hazard ranking.

Notwithstanding the findings of the PLHRA, the final design of infrastructure should be carefully sited and micro-siting adopted if required in order to maintain the design objective of avoiding any potential peat slide risk.

9 SOURCES OF INFORMATION

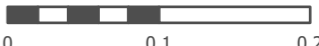

The following sources of information were used as part of the desk study investigations:

- British Geological Survey - Online GeoIndex;
- Ordnance Survey (OS) topographical information;
- Aerial and Satellite photography.
- Soil Survey of Scotland - MacAulay Institute for Soil Research (1984);
- Soil Survey of Scotland - Scottish Peat Surveys (1964);
- Scottish Government - Peat Landslide Hazard and Risk Assessments (2017);
- Scottish Government, Scottish Natural Heritage, SEPA (2017) Peatland Survey, Guidance on Developments on Peatland;
- The Scottish Government - Scotland's Third National Planning Framework (2014);
- The Scottish Government - Scottish Planning Policy (2014);
- Assessments by other EIA specialists (specifically hydrology and ecology for data on sensitive receptors); and
- Scotland's Environment Interactive Map.

APPENDIX A - FIGURES



- Existing Substation Platform
- Existing Inveraray to Crossaig Overhead Line
- Existing Access Track
- Proposed Development:**
- Indicative Town & Country Planning Boundary
- Proposed Permanent Access Track
- SUDs Inlet Pipeline
- SUDs Outfall Pipeline
- SUDs Pond
- Proposed Platform Extension
- Proposed Substation Temporary Works Area
- Proposed Substation Layout
- Crossaig Temporary Peat Storage Areas
- Permitted Development:**
- 132 kV Interconnector Cable Route
- Associated Development:**
- Existing Tower - Proposed to be Removed
- Proposed Temporary Tower Location
- Proposed Indicative Tower Location
- Proposed OHL Alignment
- Proposed Temporary OHL Bypass
- Proposed Permanent Access Track
- Temporary Access Track

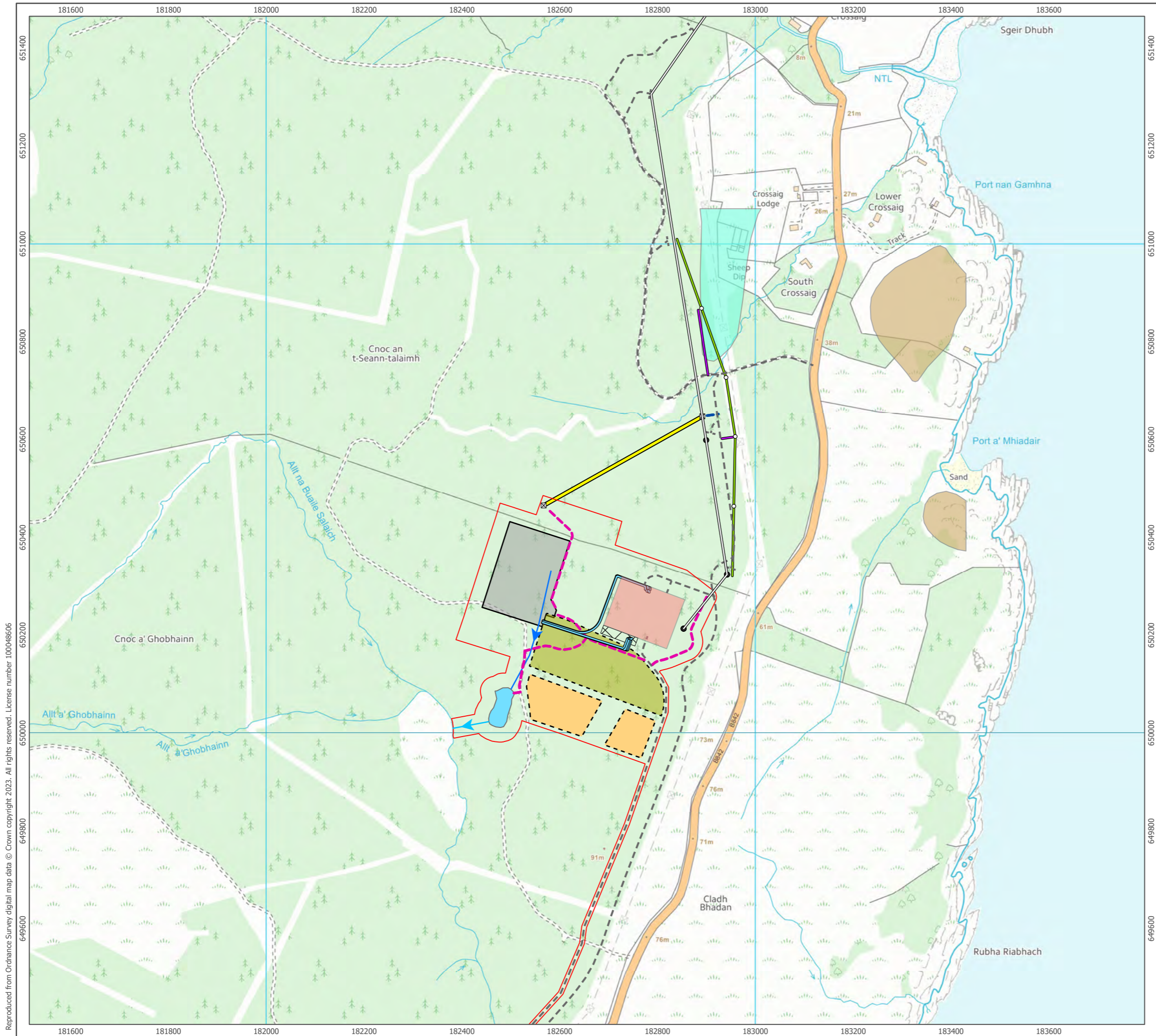
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Site Layout Plan
 Figure 1

Crossaig
Annex P: Peat Landslide
Hazard and Risk Assessment

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- Proposed Indicative Tower Location
- Proposed OHL Alignment
- Proposed Temporary OHL Bypass
- Proposed Permanent Access Track
- Temporary Access Track
- Superficial Soils**
- Till, Devensian - Diamicton
- Raised Marine Deposits - Sand and gravel

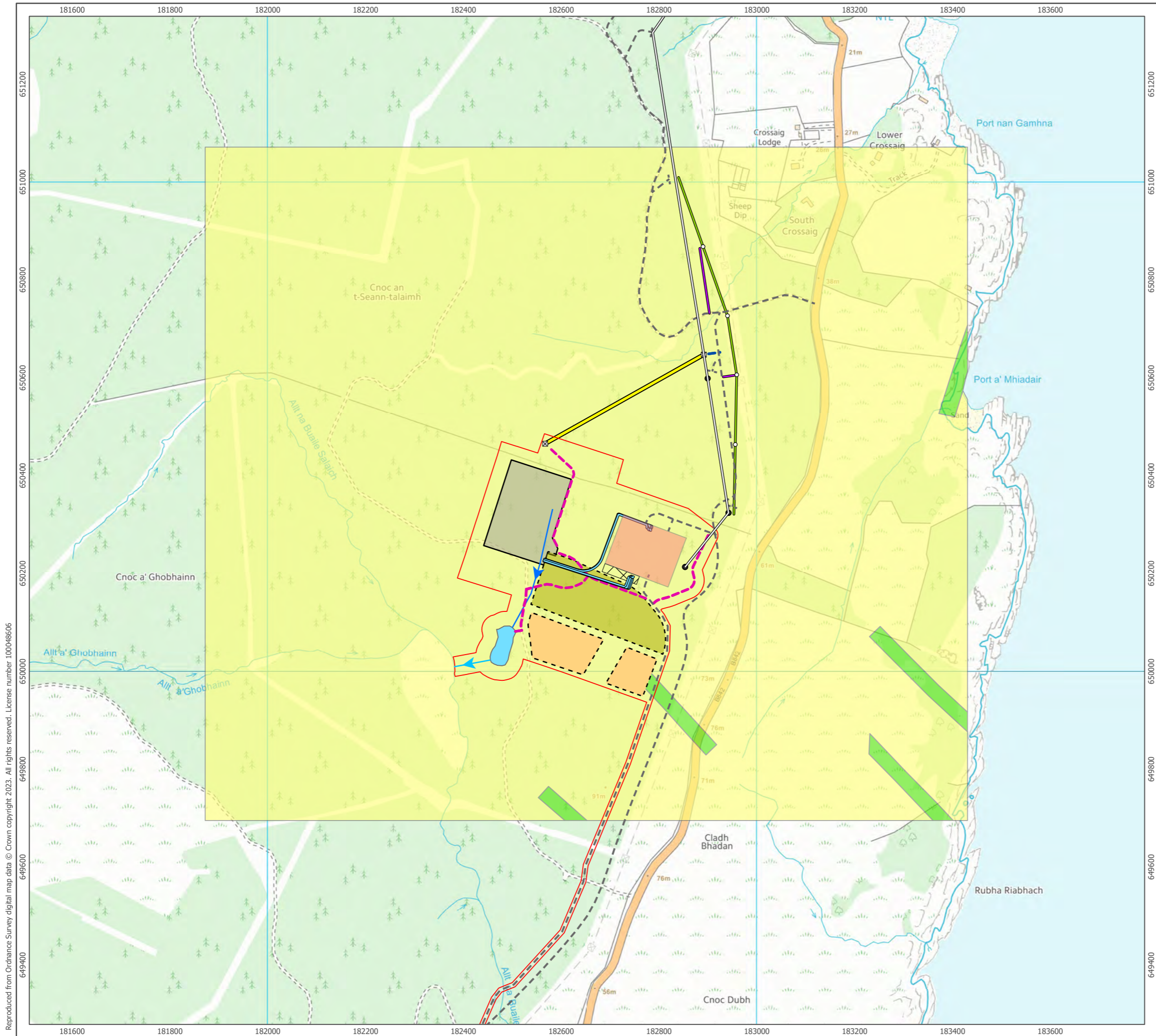
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NORTH

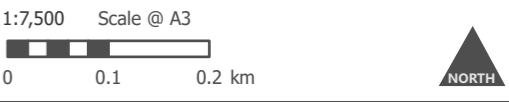
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Superficial Soils
Figure 2

Crossaig
Annex P: Peat Landslide
Hazard and Risk Assessment



- Existing Substation Platform
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- Proposed Temporary Tower Location
- Proposed Indicative Tower Location
- Proposed OHL Alignment
- Proposed Temporary OHL Bypass
- Proposed Permanent Access Track
- Temporary Access Track
- Solid Geology**
- Beinn Bheula Schist Formation
- North Britain Palaeogene Dyke Suite





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Solid Geology
Figure 3

Crossaig
Annex P: Peat Landslide
Hazard and Risk Assessment

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Existing Substation Platform
 Existing Inverarray to Crossaig Overhead Line
 Existing Access Track
Proposed Development:
 Indicative Town & Country Planning Boundary
 Proposed Permanent Access Track
 SUDs Inlet Pipeline
 SUDs Outfall Pipeline
 SUDs Pond
 Proposed Platform Extension
 Proposed Substation Temporary Works Area
 Proposed Substation Layout
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 132 kV Interconnector Cable Route
Associated Development:
 Existing Tower - Proposed to be Removed
 Proposed Temporary Tower Location
 Proposed Indicative Tower Location
 Proposed OHL Alignment
 Proposed Temporary OHL Bypass
 Proposed Permanent Access Track
 Temporary Access Track
Geomorphology
 Deforested Area
 Mature Forestry
 Bottom of Slope
 Artificial Drainage
 Top of Slope
 Minor Watercourse
 1:5,000 Scale @ A3



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Geomorphology Map
 Figure 4

Crossaig
Annex P: Peat Landslide
Hazard and Risk Assessment

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Existing Substation Platform

Existing Inveraray to Crossaig Overhead Line

Existing Access Track

Proposed Development:

- Indicative Town & Country Planning Boundary
- Proposed Permanent Access Track
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- SUDs Outfall Pipeline
- SUDs Pond
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- Proposed Substation Layout
- Crossaig Temporary Peat Storage Areas

Permitted Development:

- 132 kV Interconnector Cable Route

Associated Development:

- Existing Tower - Proposed to be Removed
- Proposed Temporary Tower Location
- Proposed Indicative Tower Location
- Proposed OHL Alignment
- Proposed Temporary OHL Bypass
- Proposed Permanent Access Track
- Temporary Access Track

Peat Depth (m)

- 0.00 - 0.50
- 0.51 - 1.00
- 1.01 - 1.50
- 1.51 - 2.00
- 2.01 - 2.50
- 2.51 - 3.00
- 3.01 - 3.50
- 3.51 - 4.00

1:5,000 Scale @ A3

0 0.1 0.2 km

NORTH

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Recorded Peat Depths
Figure 5

Crossaig
Annex P: Peat Landslide
Hazard and Risk Assessment

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Existing Substation Platform

Existing Inveraray to Crossaig Overhead Line

Existing Access Track

Proposed Development:

- Indicative Town & Country Planning Boundary
- Proposed Permanent Access Track
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- SUDs Outfall Pipeline
- SUDs Pond
- Proposed Platform Extention
- Proposed Substation Temporary Works Area
- Proposed Substation Layout
- Crossaig Temporary Peat Storage Areas

Permitted Development:

- 132 kV Interconnector Cable Route

Associated Development:

- Existing Tower - Proposed to be Removed
- Proposed Temporary Tower Location
- Proposed Indicative Tower Location
- Proposed OHL Alignment
- Proposed Temporary OHL Bypass
- Proposed Permanent Access Track
- Temporary Access Track
- Peat Probe Locations

Peat Depth (m)

- 0.00 - 0.50
- 0.51 - 1.00
- 1.01 - 1.50
- 1.51 - 2.00
- 2.01 - 2.50
- 2.51 - 3.00
- 3.01 - 3.50
- 3.51 - 4.00
- 4.01 - 4.50

1:5,000 Scale @ A3

0 0.1 0.2 km

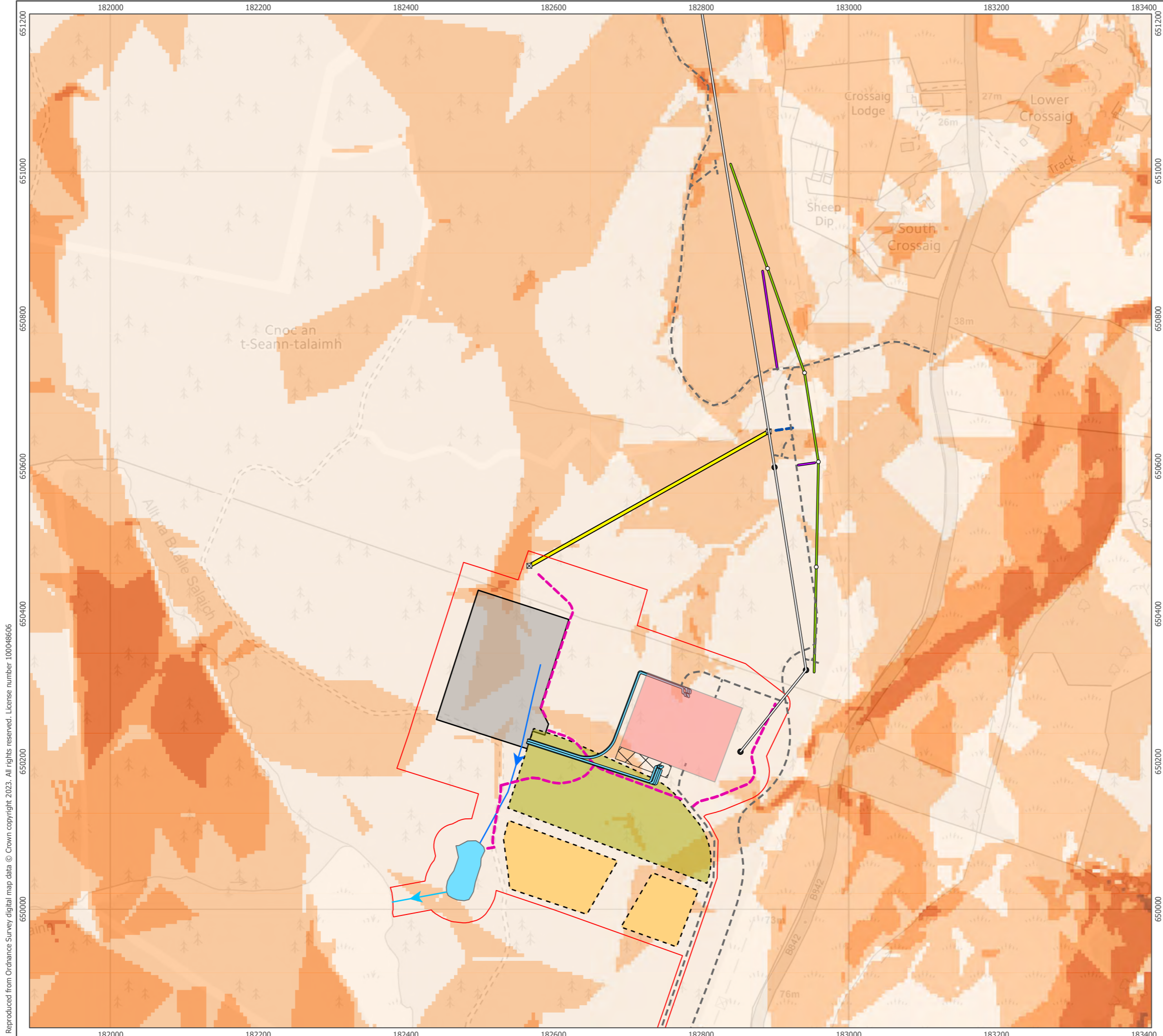
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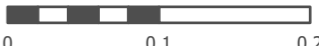

Interpolated Peat Depths
Figure 6

Crossaig
Annex P: Peat Landslide
Hazard and Risk Assessment

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Existing Substation Platform
 Existing Inveraray to Crossaig Overhead Line
 Existing Access Track
Proposed Development:
 Indicative Town & Country Planning Boundary
 Proposed Permanent Access Track
 SUDs Inlet Pipeline
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Associated Development:
 Existing Tower - Proposed to be Removed
 Proposed Temporary Tower Location
X Proposed Indicative Tower Location
 Proposed OHL Alignment
 Proposed Temporary OHL Bypass
 Proposed Permanent Access Track
 Temporary Access Track
Slope Gradient (deg)
 0.00 - 5.00
 5.01 - 10.00
 10.01 - 15.00
 15.01 - 30.00
 30.00 +

1:5,000 Scale @ A3



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Slope Map
 Figure 7

Crossaig
Annex P: Peat Landslide
Hazard and Risk Assessment

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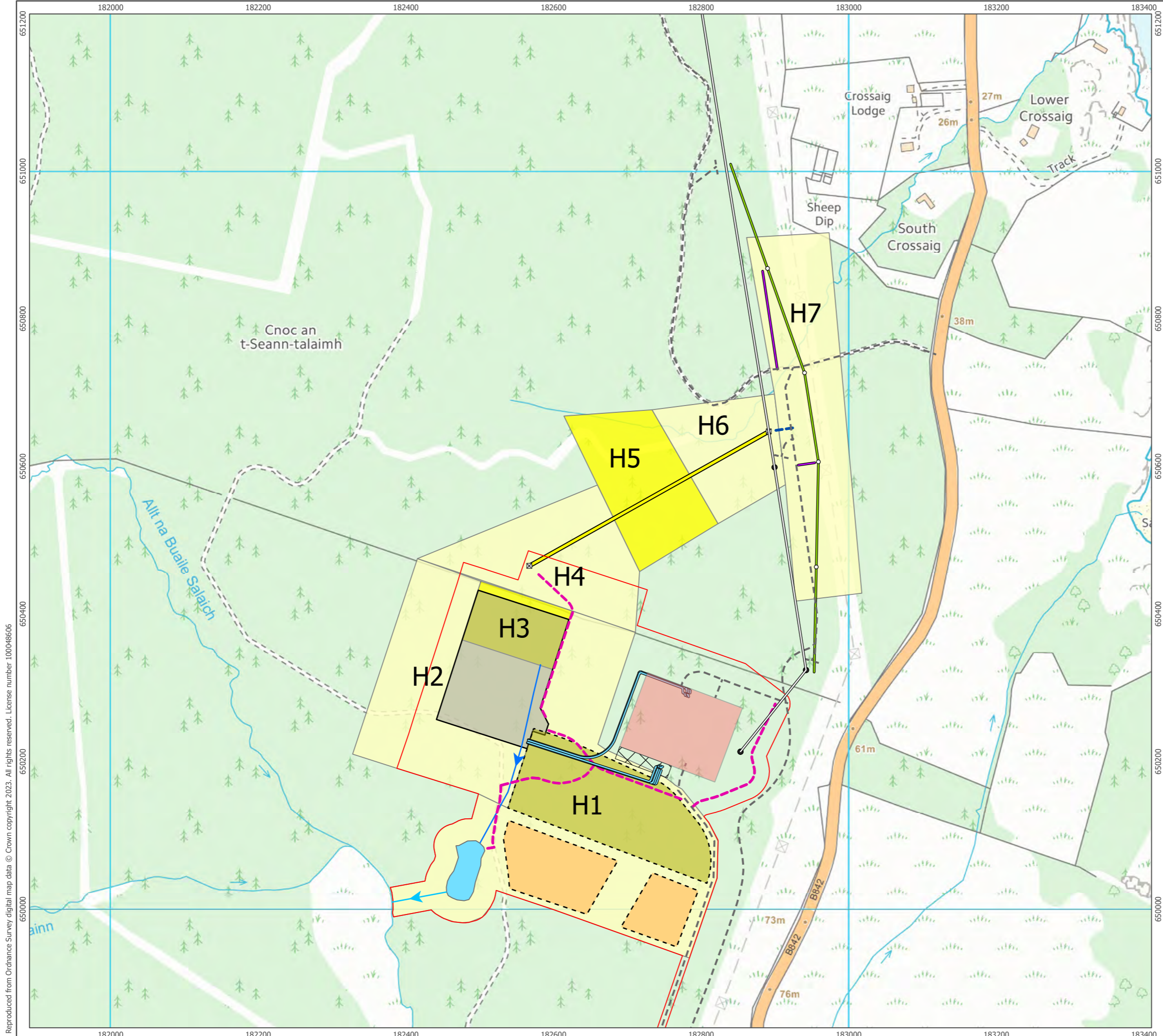
- Existing Substation Platform
- Existing Inveraray to Crossaig Overhead Line
- Existing Access Track
- Proposed Development:**
- Indicative Town & Country Planning Boundary
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- SUDs Pond
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- Proposed Substation Layout
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- Permitted Development:**
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- Associated Development:**
- Existing Tower - Proposed to be Removed
- Proposed Temporary Tower Location
- Proposed Indicative Tower Location
- Proposed OHL Alignment
- Proposed Temporary OHL Bypass
- Proposed Permanent Access Track
- Temporary Access Track
- Factor of Safety**
- Low Risk

1:5,000 Scale @ A3
 0 0.1 0.2 km 
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Factor of Safety Plan
 Figure 8

Crossaig
Annex P: Peat Landslide
Hazard and Risk Assessment

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Existing Substation Platform
 Existing Inveraray to Crossaig Overhead Line
 Existing Access Track

Proposed Development:
 Indicative Town & Country Planning Boundary
 Proposed Permanent Access Track

SUDs Outfall Pipeline
 SUDs Inlet Pipeline
 SUDs Outfall Pipeline
 SUDs Pond

Proposed Platform Extention
 Proposed Substation Temporary Works Area
 Proposed Substation Layout
 Crossaig Temporary Peat Storage Areas

Permitted Development:
 132 kV Interconnector Cable Route

Associated Development:
 Existing Tower - Proposed to be Removed
 Proposed Temporary Tower Location
 Proposed Indicative Tower Location
 Proposed OHL Alignment
 Proposed Temporary OHL Bypass
 Proposed Permanent Access Track
 Temporary Access Track

Hazard Rank
 Low
 Negligible

1:5,000 Scale @ A3
 0 0.1 0.2 km

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Hazard Rank Zonation Plan
Figure 9

Crossaig
Annex P: Peat Landslide
Hazard and Risk Assessment

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APPENDIX B - SITE PHOTOGRAPHS

Photograph 1: View north west from existing access track showing existing Crossaig Substation.



Photograph 2: Cutting for installation of drainage ditch showing ground conditions at existing access track.



Photograph 3: View east showing current conditions of proposed Temporary Works Area



Photograph 4: Windblown tree at eastern edge of proposed substation area



Photograph 5: Current conditions at proposed substation in area of forestry plantation



Photograph 6: Windblown trees in at proposed substation location



Photograph 7: View north west of recently felled area north of the proposed substation



Photograph 8: View south east from northernmost temporary tower across felled area



Photograph 9: View north from northernmost permanent tower across felled area



Photograph 10: View west from southernmost temporary tower of log piles and recently constructed track



APPENDIX C – HAZARD RANK ASSESSMENT RECORDS

4534 - Argyll Substations - PLHRA - Tabulated Peat Probe Data - Crossfall



ID	X	Y	Z	SLDPS	Slope Co-efficient	PEAT DEPTH	Peat Level	Peat Co-efficient	Gen Substrate	Substrate Co-eff.	Risk Rating Coefficient	Risk Rating Normalisation	Receptor	Receptor Co-eff.	Z Receptor	Distance	Receptor Dist Co-eff.	Z Difference (remove +/-)	Receptor elevation Co-eff	Impact Rating	Impact Rating Normalisation	Hazard Ranking
1	182808	60035	80.27459	3.442082	2	0.01	80.264499	1	G	1	2	1	80.161298	3	0	80.161298	0	0	0.113201	1	12	2
2	182797	60038	79.594204	3.463088	2	0.01	79.584204	1	G	1	2	1	79.547444	3	0	79.547444	1.495225	4	0.046764	1	12	2
3	182825	60038	81.133384	2.847420	2	0.2	81.133384	1	G	1	2	1	80.933342	3	0	80.933342	6.388124	4	0.059464	1	12	2
4	182837	60092	78.208765	5.752233	4	0.2	78.008765	1	G	1	4	1	78.313435	3	0	78.313435	15.976199	3	0.10467	1	9	1
5	182802	60087	76.493803	7.346636	4	0.3	76.193803	1	G	1	4	1	76.529624	3	0	76.529624	0	0	-0.038821	1	12	2
6	182814	60088	77.336711	6.426611	4	0.01	77.345711	1	G	1	4	1	77.345711	3	0	77.345711	2.875974	4	-0.059592	1	12	2
7	182810	60017	74.621644	2.473116	2	0.5	74.121644	1	G	1	2	1	74.066825	3	0	74.066825	10.477288	3	0.554819	1	9	1
8	182790	60022	74.544615	1.448391	1	2.7	71.844615	3	G	1	2	1	74.552259	3	0	74.552259	0	0	0.027644	1	12	2
9	182771	60100	74.468991	1.42064	1	1.2	73.268991	3	G	1	2	1	74.493381	3	0	74.493381	0	0	-0.043388	1	12	2
10	182757	60085	74.386609	1.431718	1	0.7	73.486609	2	G	1	2	1	74.36622	3	0	74.36622	0	0	0.028349	1	12	2
11	182745	60069	74.371794	2.528519	2	0.4	73.871794	1	G	1	2	1	74.347391	3	0	74.347391	0	0	0.024403	1	12	2
12	182734	60085	72.051018	4.20014	1	0.4	71.651018	1	G	1	4	1	72.101408	3	0	72.101408	0	0	0.05005	1	12	2
13	182734	60082	73.336617	2.901791	2	0.6	72.836617	1	G	1	4	1	73.337111	3	0	73.337111	0	0	0.019584	1	12	2
14	182750	60021	73.690883	2.248737	2	0.6	73.090883	2	G	1	4	1	73.887237	3	0	73.887237	0	0	0.008646	1	12	2
15	182771	60043	73.632729	1.43006	1	0.3	73.532729	1	G	1	2	1	73.462089	3	0	73.462089	0	0	0.010631	1	12	2
16	182765	60037	73.490993	2.029292	2	0.1	73.460993	1	G	1	2	1	73.460993	3	1.002574	73.460993	0	0	-0.024226	1	12	2
17	182755	60010	73.17532	2.292666	2	0.1	73.16532	1	G	1	2	1	73.170372	3	0	73.170372	0	0	0.004948	1	12	2
18	182733	60044	72.483726	2.134081	2	0.01	72.473726	1	G	1	2	1	72.452089	3	0	72.452089	0	0	0.031637	1	12	2
19	182715	60028	71.846648	2.570742	2	1.2	70.746648	3	G	1	2	1	71.925248	3	0	71.925248	0	0	0.02599	1	12	2
20	182698	60013	70.543411	5.28134	1	0.9	69.643411	2	G	1	2	1	70.488735	3	0	70.488735	0	0	0.054676	1	12	2
21	182680	60093	70.827582	1.366475	1	1.7	69.127582	3	G	1	2	1	70.828779	3	0	70.828779	0	0	0.003703	1	12	2
22	182651	600107	70.17883	1.579186	1	1	69.17883	2	G	1	2	1	70.200695	3	0	70.200695	0	0	-0.022365	1	12	2
23	182672	60039	71.474988	2.338694	2	3	68.147498	3	G	1	2	1	71.170234	3	0	71.170234	0	0	0.027275	1	12	2
24	182693	60045	71.698514	2.063882	2	1.6	70.098514	3	G	1	6	1	71.718003	3	0	71.718003	0	0	-0.019489	1	12	2
25	182707	600163	71.637456	0.825421	1	0.1	71.537456	1	G	1	2	1	71.647876	3	0	71.647876	0	0	-0.01042	1	12	2
26	182724	600178	72.846013	3.917571	1	0.1	72.836013	1	G	1	2	1	72.825509	3	0	72.825509	0	0	0.020604	1	12	2
27	182734	600194	73.604595	2.226678	2	0.1	73.594595	1	G	1	2	1	73.917052	3	8.211862	73.917052	0	0	-0.312457	1	12	2
28	182692	600192	72.610634	2.251287	2	0.1	72.510634	1	G	1	2	1	72.629001	3	0	72.629001	0	0	-0.009267	1	12	2
29	182681	600174	72.682121	2.256821	2	0.1	72.582121	1	G	1	2	1	72.548212	3	0	72.548212	0	0	-0.027002	1	12	2
30	182666	60014	72.199108	2.327157	2	1.9	70.299108	3	G	1	6	1	72.158405	3	0	72.158405	0	0	0.047003	1	12	2
31	182648	600137	71.513887	2.334999	2	1	70.513887	2	G	1	4	1	71.534261	3	0	71.534261	0	0	-0.020374	1	12	2
32	182629	60017	70.60622	2.82721	2	0.8	69.80622	2	G	1	4	1	70.720441	3	0	70.720441	0	0	-0.025839	1	12	2
33	182600	60010	71.605551	2.063378	2	0.3	70.705551	1	G	1	2	1	71.046918	3	0	71.046918	0	0	0.003631	1	12	2
34	182568	60043	71.166678	2.083035	2	0.3	70.866678	1	G	1	2	1	71.193028	3	0	71.193028	0	0	-0.02635	1	12	2
35	182541	60049	71.20789	1.46991	1	0.1	71.19789	1	G	1	2	1	71.30944	3	0	71.30944	0	0	-0.01155	1	12	2
36	182552	600173	71.90421	2.060121	2	0.5	71.40421	1	G	1	2	1	71.910108	3	0	71.910108	0	0	-0.002609	1	12	2
37	182579	600162	71.939319	2.084684	2	0.01	71.929319	1	G	1	2	1	71.927036	3	0	71.927036	0	0	0.012283	1	12	2
38	182615	60048	71.805748	2.24741	2	0.01	71.845748	1	G	1	2	1	71.828559	3	0	71.828559	0	0	0.027189	1	12	2
39	182634	60048	72.90275	2.286486	2	0.1	72.750275	1	G	1	2	1	72.750275	3	0	72.750275	0	0	0.023825	1	12	2
40	182602	600182	72.917495	2.065268	2	0.1	72.907495	1	G	1	2	1	72.913024	3	0	72.913024	0	0	0.004471	1	12	2
41	182646	600192	73.70049	2.300121	2	0.01	73.73049	1	G	1	2	1	73.730094	3	0	73.730094	0	0	0.009355	1	12	2
42	182659	60036	74.115989	3.338062	2	0.01	74.105989	1	G	1	2	1	74.09852	3	0	74.09852	0	0	0.017407	1	12	2
43	182625	60020	74.39138	1.16564	1	0.1	74.329138	1	G	1	2	1	74.324518	3	0	74.324518	0	0	0.034462	1	12	2
44	182612	6002	73.747567	2.084688	2	0.01	73.737567	1	G	1	2	1	73.732028	3	0	73.732028	0	0	0.024539	1	12	2
45	182588	600213	73.757209	1.79811	1	0.01	73.777209	1	G	1	2	1	73.715568	3	0	73.715568	0	0	-0.028599	1	12	2
46	182593	60023	74.157376	0.934011	1	0.1	74.147376	1	G	1	2	1	74.150979	3	0	74.150979	0	0	0.009739	1	12	2
47	182563	60010	73.387478	2.505024	2	0.1	73.287478	1	G	1	2	1	73.365029	3	0	73.365029	0	0	0.022449	1	12	2
48	182566	60044	73.939929	0.952031	1	0.2	73.739929	1	G	1	2	1	73.99244	3	0	73.99244	0	0	0.001486	1	12	2
49	182572	60011	73.85016	2.08292	2	0.1	73.75016	1	G	1	2	1	73.873041	3	0	73.873041	0	0	-0.017025	1	12	2
50	182548	60012	73.280416	2.068705	2	0.3	73.280416	1	G	1	2	1	73.255025	3	0	73.255025	0	0	0.025391	1	12	2
51	182539	60016	73.287557	1.817235	1	0.2	73.087557	1	G	1	2	1	73.26039	3	0	73.26039	0	0	0.024518	1	12	2
52	182528	60019	73.09811	6.999912	4	0.1	73.02811	3	G	1	4	1	73.033108	3	0	73.033108	0	0	-0.003468	1	12	2
53	182520	60026	74.89112	6.007652	4	0.2	74.619112	1	G	1	4	1	74.70563	3	0	74.70563	0	0	0.113482	1	12	2
54	182529	60035	74.17988	6.26231	4	0.3	74.07988	1	G	1	4	1	74.441469	3	0	74.441469	0	0	0.04181	1	12	2
55	182519	60036	75.38097	5.28004	4	0.3	75.00097	1	G	1	4	1	75.371991	3	0	75.371991	0	0	-0.047044	1	12	2
56	182509	60036	75.86192	2.345202	2	0.1	75.56192	1	G	1	2	1	75.893257	3	0	75.893257	0	0	-0.031337	1	12	2
57	182499	60036	76.012999	3.44562	2	0.1	75.912999	1	R	1.5	3	1	75.971051	3	0	75.971051	0	0	0.041948	1	12	2
58	182499	60045	76.29168	1.893191	1	0.1	76.19168	1	R	1.5	3	1	76.293252	3	0	76.293252	0	0	-0.043084	1	12	2
59	182481	60027	75.90213	4.91138	4	0.1	75.80213	1	G	1	4	1	75.960701	3	0	75.960701	0	0	0.004488	1	12	2
60	182480	60036	75.543803	5.03844	4	0.6	74.943803	2	G	1	4	1	75.546619	3	0	75.546619	0					

161	182510	600426	87.875248	11.1294	0.3	87.5752481	G	1	A	6	2	Site Infrastructure	3	87.17846	0.4	0.156788	1	12	2	4
162	182510	600416	86.595551	6.626411	0.4	86.1955511	G	1	A	6	2	Site Infrastructure	3	86.521057	0.4	0.074494	1	12	2	4
163	182510	600406	85.707592	5.631876	0.2	85.3075921	G	1	A	6	2	Site Infrastructure	3	85.657889	0.4	0.072903	1	12	2	4
164	182510	600396	85.026265	4.648306	0.2	84.6262651	G	1	A	6	2	Site Infrastructure	3	84.954304	0.4	0.071993	1	12	2	4
165	182500	600396	85.296584	4.607984	0.2	85.0965841	G	1	A	6	2	Site Infrastructure	3	85.249149	0.4	0.047445	1	12	2	4
166	182510	600386	84.204796	3.643132	0.1	84.0047961	G	1	A	6	2	Site Infrastructure	3	84.186776	0.4	0.061002	1	12	2	4
167	182500	600386	84.294984	3.602812	0.2	84.0949841	G	1	A	6	2	Site Infrastructure	3	84.290319	0.4	0.049881	1	12	2	4
168	182490	600376	84.032913	4.546326	0.1	83.8329131	G	1	A	6	2	Site Infrastructure	3	83.986825	0.4	0.046088	1	12	2	4
169	182490	600366	83.727249	4.076775	0.1	83.5272491	G	1	A	6	2	Site Infrastructure	3	83.239492	0.4	0.033457	1	12	2	4
170	182480	600356	82.713736	4.720066	0.1	82.5137361	G	1	A	6	2	Site Infrastructure	3	82.724106	0.4	0.047406	1	12	2	4
171	182490	600347	82.45559	3.420723	0.2	82.255591	G	1	A	6	2	Site Infrastructure	3	82.285851	0.4	0.040051	1	12	2	4
172	182480	600346	81.982918	4.369433	0.1	81.7829181	G	1	A	6	2	Site Infrastructure	3	81.93683	0.4	0.046088	1	12	2	4
173	182480	600336	81.24694	3.840622	0.2	81.046941	G	1	A	6	2	Site Infrastructure	3	81.280214	0.4	0.040438	1	12	2	4
174	182490	600336	81.406313	3.181812	0.01	81.2063131	G	1	A	6	2	Site Infrastructure	3	81.500313	0.4	0.041460	1	12	2	4
175	182490	600336	82.632752	3.657714	0.2	82.4327521	G	1	A	6	2	Site Infrastructure	3	82.666265	0.4	0.027513	1	12	2	4
176	182500	600326	80.326256	5.875595	0.4	79.9262561	G	1	A	6	2	Site Infrastructure	3	80.274465	0.4	0.061991	1	12	2	4
177	182500	600316	81.121473	5.879681	0.2	80.7214731	G	1	A	6	2	Site Infrastructure	3	80.521473	0.4	0.039292	1	12	2	4
178	182500	600346	81.887795	5.545061	0.6	81.2877952	G	1	B	2	2	Site Infrastructure	3	81.806775	0.4	0.08102	1	12	2	4
179	182500	600356	82.66254	4.99972	0.4	82.262541	G	1	A	6	2	Site Infrastructure	3	82.574262	0.4	0.081992	1	12	2	4
180	182500	600366	82.362636	4.192961	0.1	82.1626361	G	1	A	6	2	Site Infrastructure	3	82.304279	0.4	0.062527	1	12	2	4
181	182499	600376	83.970949	3.890802	0.1	83.7709491	G	1	A	6	2	Site Infrastructure	3	83.908124	0.4	0.062825	1	12	2	4
182	182510	600376	83.501474	5.865155	0.2	83.3014741	G	1	A	6	2	Site Infrastructure	3	83.419098	0.4	0.062376	1	12	2	4
183	182510	600386	82.756253	5.875595	0.5	82.3562531	G	1	A	6	2	Site Infrastructure	3	82.854262	0.4	0.081991	1	12	2	4
184	182520	600386	81.251473	5.879681	0.9	80.8514731	G	1	A	6	2	Site Infrastructure	3	81.189096	0.4	0.061991	1	12	2	4
185	182510	600356	81.967797	5.873394	0.6	81.3677972	G	1	B	2	2	Site Infrastructure	3	81.886777	0.4	0.08102	1	12	2	4
186	182510	600346	81.204792	5.878974	0.6	80.6047922	G	1	B	2	2	Site Infrastructure	3	81.119096	0.4	0.062376	1	12	2	4
187	182510	600356	80.426253	5.875595	0.9	79.8262532	G	1	B	2	2	Site Infrastructure	3	80.350261	0.4	0.081992	1	12	2	4
188	182510	600226	79.607795	5.873389	0.6	79.0077952	G	1	B	2	2	Site Infrastructure	3	79.586776	0.4	0.081019	1	12	2	4
189	182510	600316	78.901473	5.878988	0.3	78.3014731	G	1	A	6	2	Site Infrastructure	3	78.819096	0.4	0.062377	1	12	2	4
190	182510	600315	78.211861	5.874171	0.1	77.6118611	G	1	A	6	2	Site Infrastructure	3	78.221861	0.4	0.060095	1	12	2	4
191	182520	600226	78.981471	5.879876	0.4	78.3814711	G	1	A	6	2	Site Infrastructure	3	78.899096	0.4	0.062376	1	12	2	4
192	182520	600336	79.747795	5.873394	1.3	78.4477953	G	1	A	6	2	Site Infrastructure	3	79.666776	0.4	0.081019	1	12	2	4
193	182521	600345	80.401488	5.872027	1.1	79.2014883	G	1	A	6	2	Site Infrastructure	3	80.434383	0.4	0.030115	1	12	2	4
194	182520	600346	82.47795	5.873394	0.4	81.677951	G	1	A	6	2	Site Infrastructure	3	81.966776	0.4	0.08102	1	12	2	4
195	182520	600376	82.816255	5.873312	0.7	82.1162552	G	1	A	6	2	Site Infrastructure	3	82.734264	0.4	0.081991	1	12	2	4
196	182520	600386	83.201474	6.12082	0.4	83.1814741	R	1	B	2	2	Site Infrastructure	3	83.499997	0.4	0.082377	1	12	2	4
197	182520	600386	84.101178	7.274451	0.3	83.9011781	G	1	B	2	2	Site Infrastructure	3	84.181178	0.4	0.131433	1	12	2	4
198	182520	60046	84.652217	8.352251	0.1	84.5522171	G	1	B	2	2	Site Infrastructure	3	84.555001	0.4	0.117166	1	12	2	4
199	182520	600416	85.08635	7.521274	0.3	85.386351	G	1	B	2	2	Site Infrastructure	3	85.588021	0.4	0.118320	1	12	2	4
200	182520	600416	85.04728	11.019228	0.2	85.9047281	G	1	B	2	2	Site Infrastructure	3	85.278991	1.09324	0.174283	1	12	2	4
201	182530	600426	84.402065	10.650164	0.2	84.2020651	G	1	B	2	2	Site Infrastructure	3	84.229902	4.338894	0.172163	1	12	2	4
202	182530	600416	84.36989	9.273737	0.2	84.169891	G	1	B	2	2	Site Infrastructure	3	84.210004	0.4	0.159286	1	12	2	4
203	182530	600346	83.68384	9.482519	0.2	83.383841	G	1	B	2	2	Site Infrastructure	3	83.368404	0.4	0.142519	1	12	2	4
204	182530	600396	82.788121	8.355026	0.6	81.6881213	R	1	B	2	2	Site Infrastructure	3	82.646077	0.4	0.142044	1	12	2	4
205	182530	600386	82.438121	8.15127	0.8	81.6381212	R	1	B	2	2	Site Infrastructure	3	82.296077	0.4	0.142044	1	12	2	4
206	182530	600376	82.03985	7.042124	1.3	80.739853	R	1	B	2	2	Site Infrastructure	3	81.895127	0.4	0.123958	1	12	2	4
207	182530	600366	81.451475	6.08092	1	80.3514751	G	1	B	2	2	Site Infrastructure	3	81.279098	0.4	0.082377	1	12	2	4
208	182530	600356	80.596254	5.873743	1.3	79.2962543	G	1	B	2	2	Site Infrastructure	3	80.514263	0.4	0.081991	1	12	2	4
209	182530	600346	79.827795	5.873394	0.3	79.2277951	G	1	A	6	2	Site Infrastructure	3	79.746775	0.4	0.08102	1	12	2	4
210	182530	600336	79.051473	5.878974	0.4	78.6514731	G	1	A	6	2	Site Infrastructure	3	78.979097	0.4	0.082376	1	12	2	4
211	182530	600326	78.296253	5.875606	0.1	78.1962531	G	1	A	6	2	Site Infrastructure	3	78.214262	0.4	0.081991	1	12	2	4
212	182530	600316	77.527794	5.873394	0.3	77.2277941	G	1	A	6	2	Site Infrastructure	3	77.446775	0.4	0.081019	1	12	2	4
213	182540	600316	76.757797	3.102624	0.5	76.5577971	G	1	A	6	2	Site Infrastructure	3	76.711019	0.4	0.066266	1	12	2	4
214	182540	600306	76.144335	4.318731	0.5	75.6443351	G	1	A	6	2	Site Infrastructure	3	76.084244	0.4	0.060091	1	12	2	4
215	182540	600316	76.841471	5.801514	0.5	76.3414711	G	1	A	6	2	Site Infrastructure	3	76.759096	0.4	0.082375	1	12	2	4
216	182540	600326	77.607796	5.873394	0.7	77.2077961	G	1	A	6	2	Site Infrastructure	3	77.526776	0.4	0.08102	1	12	2	4
217	182540	600336	78.376255	5.875606	0.4	77.9762551	G	1	A	6	2	Site Infrastructure	3	78.294504	0.4	0.081991	1	12	2	4
218	182540	600346	79.141473	5.981071	1	78.3414732	R	1	B	2	2	Site Infrastructure	3	79.059097	0.4	0.082376	1	12	2	4
219	182540	600356	79.834885	6.703997	0.9	78.9348852	R	1	B	2	2	Site Infrastructure	3	79.726722	0.4	0.081013	1	12	2	4
220	182540	600366	80.304013	7.93862	1.2	79.1040131	R	1	B	2	2	Site Infrastructure	3	80.161019	0.4	0.08102	1	12	2	4
221	182540	600376	80.4812	8.170424	1.5	79.48123	R	1	B	2	2	Site Infrastructure	3	80.506076	0.4	0.142044	1	12	2	4
222	182540	600386	81.391233	7.878988	0.2	81.0912331	G	1	B	2	2	Site Infrastructure	3	81.266562	0.4	0.124281	1	12	2	4
223	182540	600386	80.99812	7.700012	0.6	80.398121	G	1	B	2	2	Site Infrastructure	3	80.856076	0.4	0.120044	1	12	2	4
224	182540	60046	82.008779	11.041999	0.4	81.6087791	G	1	B	2	2	Site Infrastructure	3	81.795023	0.4	0.213756	1	12	2	4
225	182540	600416	82.30846	11.681549	0.3	82.098461	G	1	B	2	2	Site Infrastructure	3	82.202872	0.4	0.195574	1	12	2	4
226	182550	600416	80.51691	7.79964	1	79.716911	G	1	B	2	2	Site Infrastructure	3	79.716911	1.09324	0.134211	1	12	2	4
227	182550	60046	80.285193	7.004344	1	79.2851932	G	1	B	2										

656	182953	650632	56.385326	12.306441	6	1	55.385326	G	1	1	Site Infrastructure	3	59.296345	22.471134	3	-2.911039	1	1	9	1	1
657	182963	650631	56.416628	12.405277	6	1	56.216628	G	1	6	Site Infrastructure	3	59.158161	21.810418	3	-2.741533	1	1	9	1	2
658	182973	650632	56.462201	7.151391	4	1	56.262201	G	1	4	Site Infrastructure	3	59.158161	24.944131	3	-2.69596	1	1	9	1	1
659	182983	650621	56.232446	5.132114	4	1	56.132446	G	1	4	Site Infrastructure	3	59.158161	30.065969	3	-2.925215	1	1	9	1	1
660	182983	650622	56.990775	5.282503	1	1	56.890775	G	1	1	Site Infrastructure	3	59.158161	23.783009	3	-2.167386	1	1	9	1	1
661	182983	650612	57.274246	6.901939	4	1	57.174246	R	1	4	Site Infrastructure	3	59.158161	20.280245	3	-1.883915	1	1	9	1	2
662	182973	650613	58.362628	6.321216	4	1	58.162628	G	1	4	Site Infrastructure	3	59.158161	11.252394	3	-0.794633	1	1	9	1	1
663	182973	650622	57.806941	8.218749	6	1	57.606941	G	1	6	Site Infrastructure	3	59.158161	16.126681	3	-1.35122	1	1	9	1	2
664	182964	650622	58.263142	7.95001	4	1	58.163142	G	1	4	Site Infrastructure	3	59.158161	12.690023	3	-0.895019	1	1	9	1	1
665	182964	650612	59.001119	3.339831	2	1	58.901119	G	1	2	Site Infrastructure	3	59.158161	2.794139	4	-0.148042	1	1	9	1	2
666	182959	650606	59.407081	3.096494	2	1	59.207081	G	1	2	Site Infrastructure	3	59.446995	0.748544	4	-0.039914	1	1	12	2	2
667	182954	650621	58.534863	7.943128	4	1	58.134863	G	1	4	Site Infrastructure	3	59.296345	11.880523	3	-0.761482	1	1	9	1	1
668	182953	650612	59.244128	2.761841	1	1	59.244128	G	1	2	Site Infrastructure	3	59.296345	4.392323	4	-0.023217	1	1	12	2	2
669	182944	650621	58.151386	8.917056	4	1	58.141386	G	1	4	Site Infrastructure	3	59.296345	17.477821	3	-1.144729	1	1	9	1	1
670	182934	650621	57.399747	8.480761	6	1	57.399747	G	1	6	Site Infrastructure	3	59.440273	24.372949	3	-2.040526	1	1	9	1	1
671	182933	650612	58.617097	5.68765	4	1	58.417097	G	1	4	Site Infrastructure	3	59.440273	21.539099	3	-0.823176	1	1	9	1	1
672	182946	650610	59.320854	2.223234	2	1	59.320854	G	1	2	Site Infrastructure	3	59.440273	8.749212	4	-0.236419	1	1	12	2	2
673	182953	650602	59.749996	2.706394	2	1	59.449996	G	1	2	Site Infrastructure	3	59.589793	3.751776	4	0.160203	1	1	12	2	2
674	182953	650592	60.197924	2.67494	1	1	60.097924	G	1	2	Site Infrastructure	3	59.642346	11.085441	3	0.555578	1	1	9	1	1
675	182953	650581	60.609125	2.731854	2	1	60.659125	G	1	2	Site Infrastructure	3	59.642346	21.430214	3	1.020779	1	1	9	1	1
676	182943	650581	60.352353	3.076597	2	1	60.252353	R	1	3	Site Infrastructure	3	59.642346	25.206808	3	0.710007	1	1	1	1	1
677	182943	650592	59.895984	3.16055	2	1	59.495984	G	1	2	Site Infrastructure	3	59.586669	17.654832	3	0.320915	1	1	9	1	1
678	182943	650602	59.451094	3.091951	2	1	58.851094	G	1	2	Site Infrastructure	3	59.586669	12.162999	3	-0.107575	1	1	9	1	1
679	182934	650602	59.190907	3.153194	2	1	59.190907	G	1	2	Site Infrastructure	3	59.586669	20.838103	3	-0.347762	1	1	9	1	1
680	182934	650591	59.837678	3.620551	2	1	59.837678	G	1	2	Site Infrastructure	3	59.586669	25.526764	3	0.290009	1	1	9	1	1
681	182950	650488	64.240061	4.51051	4	1	64.230061	G	1	4	Site Infrastructure	3	65.086296	21.508104	3	-0.828235	1	1	9	1	1
682	182960	650489	63.394013	7.050921	4	1	62.994013	G	1	4	Site Infrastructure	3	64.874209	21.880509	3	-1.480196	1	1	9	1	1
683	182970	650489	62.947856	8.91174	6	1	62.937856	G	1	6	Site Infrastructure	3	64.874209	24.780092	3	-1.926353	1	1	9	1	2
684	182981	650489	62.510804	7.877864	4	1	62.310804	G	1	4	Site Infrastructure	3	64.874209	30.917025	3	-2.364405	1	1	9	1	1
685	182981	650479	63.617484	6.650884	4	1	63.117484	G	1	4	Site Infrastructure	3	64.874209	24.684258	3	-1.259202	1	1	9	1	1
686	182980	650470	64.185297	5.866902	4	1	63.885297	G	1	4	Site Infrastructure	3	64.874209	20.388798	3	0.691389	1	1	9	1	1
687	182980	650460	64.749832	4.843012	4	1	64.449832	G	1	4	Site Infrastructure	3	64.979092	19.725854	3	0.22926	1	1	9	1	1
688	182980	650449	65.150406	3.443992	2	1	65.050406	G	1	2	Site Infrastructure	3	65.276186	23.917065	3	-0.11678	1	1	9	1	1
689	182980	650459	65.481604	2.799912	1	1	65.381604	G	1	1	Site Infrastructure	3	65.276186	29.752489	3	0.295418	1	1	9	1	1
690	182970	650439	65.724786	3.701533	2	1	65.714786	G	1	2	Site Infrastructure	3	65.276186	23.710231	3	0.4486	1	1	9	1	1
691	182970	650489	65.247542	2.78203	2	1	65.047542	G	1	2	Site Infrastructure	3	65.276186	15.552023	3	-0.028644	1	1	9	1	1
692	182970	650459	64.922159	1.921141	1	1	64.622159	G	1	1	Site Infrastructure	3	64.979092	10.402739	3	-0.056933	1	1	9	1	1
693	182970	650469	64.802754	1.83187	1	1	64.502754	G	1	1	Site Infrastructure	3	64.874209	10.309738	3	-0.073932	1	1	9	1	1
694	182970	650479	64.488938	5.463158	4	1	64.388938	G	1	4	Site Infrastructure	3	64.874209	16.537597	3	-0.385271	1	1	9	1	1
695	182960	650479	64.284761	3.782124	2	1	63.384761	G	1	2	Site Infrastructure	3	64.874209	11.309622	3	-0.589448	1	1	9	1	1
696	182961	650469	64.60475	2.97734	2	1	64.60475	G	1	2	Site Infrastructure	3	64.874209	10.830744	3	0.442514	1	1	12	2	2
697	182956	650464	65.18942	4.030413	4	1	65.08942	G	1	4	Site Infrastructure	3	65.173811	0.842227	4	0.035609	1	1	12	2	2
698	182960	650460	65.199754	3.931312	2	1	65.189754	G	1	2	Site Infrastructure	3	65.276186	13.73021	4	-0.076432	1	1	12	2	2
699	182960	650449	65.7187	4.024986	4	1	65.7087	G	1	4	Site Infrastructure	3	65.276186	10.830744	3	0.442514	1	1	9	1	1
700	182960	650439	66.215891	4.024986	4	1	66.205891	G	1	4	Site Infrastructure	3	65.276186	20.150882	3	0.939705	1	1	9	1	1
701	182949	650440	66.70823	4.024986	4	1	66.60823	G	1	4	Site Infrastructure	3	65.474173	19.973103	3	1.230207	1	1	9	1	1
702	182941	650440	67.134613	4.009829	4	1	67.124613	G	1	4	Site Infrastructure	3	65.474173	23.840794	3	1.60044	1	1	9	1	1
703	182931	650439	67.63655	3.80809	2	1	66.63655	G	1	2	Site Infrastructure	3	65.474173	30.765302	3	2.162377	1	1	9	1	1
704	182932	650450	67.099902	4.024986	4	1	67.089902	G	1	4	Site Infrastructure	3	65.474173	24.146124	3	1.625729	1	1	9	1	1
705	182930	650459	66.666934	4.024986	4	1	66.266934	G	1	4	Site Infrastructure	3	65.474173	22.165352	3	1.152761	1	1	9	1	1
706	182931	650470	66.118592	4.036498	4	1	66.018592	G	1	4	Site Infrastructure	3	65.268363	22.220668	3	0.850229	1	1	9	1	1
707	182931	650479	65.648372	3.975708	2	1	65.548372	G	1	2	Site Infrastructure	3	65.268363	25.710363	3	0.380009	1	1	9	1	1
708	182931	650489	65.170216	3.95875	2	1	64.870216	G	1	2	Site Infrastructure	3	65.268363	32.329322	3	-0.098347	1	1	9	1	1
709	182941	650469	65.665059	4.038613	4	1	65.065059	G	1	4	Site Infrastructure	3	65.268363	12.571225	3	0.396696	1	1	9	1	2
710	182941	650459	66.167571	4.024986	4	1	65.167571	R	1	5	Site Infrastructure	3	65.474173	12.157651	3	0.693398	1	1	9	1	2
711	182941	650489	66.271294	4.024986	4	1	66.271294	G	1	4	Site Infrastructure	3	65.474173	17.070491	3	1.197121	1	1	9	1	1
712	182951	650449	66.173988	4.024986	4	1	65.163988	G	1	4	Site Infrastructure	3	65.474173	10.804956	3	0.699815	1	1	9	1	1
713	182951	650459	65.681537	4.025001	4	1	65.671537	G	1	4	Site Infrastructure	3	65.474173	3.071322	4	0.207364	1	1	12	2	2
714	182951	650469	65.155452	4.07824	4	1	65.145452	G	1	4	Site Infrastructure	3	65.086296	4.286947	4	0.087156	1	1	12	2	2
715	182951	650480	64.654662	4.06446	4	1	64.634662	G	1	4	Site Infrastructure	3	65.086296	12.666104	3	-0.421834	1	1	9	1	1

Slope Angles

	Co-eff.	
0	2.0	1.0
2	4.0	2.0
4	8.0	4.0
8	15.0	6.0
15	35.0	8.0

Peat depths

	Co-eff.	
0	0.5	1.0
0.51	1.0	2.0
1.01	3.0	3.0
3.01	6.0	8.0

Substrate

	Co-eff.	
G	1.0	
R	1.5	
C	2.0	
net grown		

APPENDIX D – PEAT CORING RECORDS



Background

Peat cores were obtained from two locations at the proposed Crossaig Substation and associated infrastructure in July 2022, one at the northern boundary of the proposed substation footprint and one in the proposed temporary works area. Cores were advanced in areas of the Site where peat probing had identified the presence of deep peat to characterise the properties of the peatland in accordance with the *Peatland Survey. Guidance on Developments on Peatland (2017)*. The document, which was published jointly by the Scottish Government, Scottish Natural Heritage (NatureScot) and SEPA, defines a consistent sampling methodology to quantify and qualify the peat material on site. It also provides advice on how to publish peat surveys as part of wider site investigations for development management applications, with a particular focus on wind farm developments.

The parameters used to determine the characteristics of the peat materials are outlined below.

i. Surface firmness estimation

An average man standing on one foot applies a pressure to the ground of between 5 and 6 lbs / p.s.i. and this fact is used to estimate the bearing capacity. The following symbols are used to denote the pressure the ground will stand.

Firmness of surface (P)

PO = Surface too soft to walk on

P1 = Surface just passable

P2 = Surface fairly firm

P3 = Surface firm

ii. Observations on the vegetation

The Site is largely surrounded by commercial forestry plantations at varying stages of development and will require felling prior to the beginning of construction. The Temporary Works Area and proposed access tracks are situated in a previously felled area adjacent to the existing Crossaig Substation.

iii. Observations on the peat

a. Botanical observations

Botanical observations of peat samples identified that *Carex* species are likely to make up a significant proportion of the organic material in the lower horizons where catotelmic peat is typically found.

b. Degree of humification - von POST SCALE

The degree of humification of peat samples is estimated in the field according to the method devised by the Swedish botanist L. von Post by squeezing a small amount of peat in the hand and the water and / or peat exuded indicates, by its colour and consistency, the degree to which the peat has undergone humification or, more correctly, a type of decomposition which includes breakdown under anaerobic conditions. The von Post scale ranges from 1 to 10, the higher the number the higher the degree of humification. The full scale is as follows:

Von Post Scale (H)	
H1	Completely undecomposed peat free of amorphous material. On squeezing, clear colourless water is pressed out.



H2	Nearly undecomposed peat, free of amorphous material, yielding only yellowish brown water on pressing.
H3	Very slightly decomposed peat, containing a little amorphous material. On squeezing, muddy brown water but no peat passes between the fingers. Residue is not pasty.
H4	Slightly decomposed peat containing some amorphous material. Strongly muddy brown water but no peat passes between the fingers. Residue is somewhat pasty.
H5	Moderately decomposed peat containing a fair amount of amorphous material. Plant structure recognisable though somewhat vague. On squeezing, some peat but mainly muddy water issues. Residue is strongly pasty.
H6	Moderately decomposed peat with a fair amount of amorphous material and indistinct plant structure. On pressing, about one third of the peat passes between the fingers. Residue is strongly pasty, but shows the plant structure more distinctly than in unsqueezed peat.
H7	Strongly decomposed peat with much amorphous material and faintly recognisable plant structure. On squeezing, about one half of the peat is extruded. The water is very dark in colour.
H8	Strongly decomposed peat with much amorphous material and very indistinct plant structure. On squeezing, two thirds of the peat and some water passes between the fingers. Residue consists of plant tissues capable of resisting decomposition (roots, fibres, wood, etc.).
H9	Practically fully decomposed peat with almost no recognisable plant structure. Nearly all the peat squeezed between the fingers as a uniform paste.
H10	Completely decomposed peat with no discernible plant structure. On squeezing, all the peat, without water, passes between the fingers.

iv. Fibre

The fibre content of each peat sample is estimated visually and the amounts of the two types (classified 'fine' or 'coarse') are noted on a scale ranging from 0 to 3 as shown below.

Fine fibres, mainly derived from *Eriophorum spp.* (F)

F0 = Nil

F1 = Low content

F2 = Moderate content

F3 = High content

Coarse fibres, mainly rootlets (R)

R0 = Nil

R1 = Low content

R2 = Moderate content

R3 = High content

v. Wood

Wood remains, especially if they are large and resistant, may conceivably cause a certain amount of difficulty during the exploitation of a bog. An attempt is therefore made when sampling to assess the extent of wood. It is estimated on a scale ranging from 0 to 3 as detailed below.

Wood remains (W)

W0= Nil

Peat Coring Record



W1 = Low content
W2 = Moderate content
W3 = High content

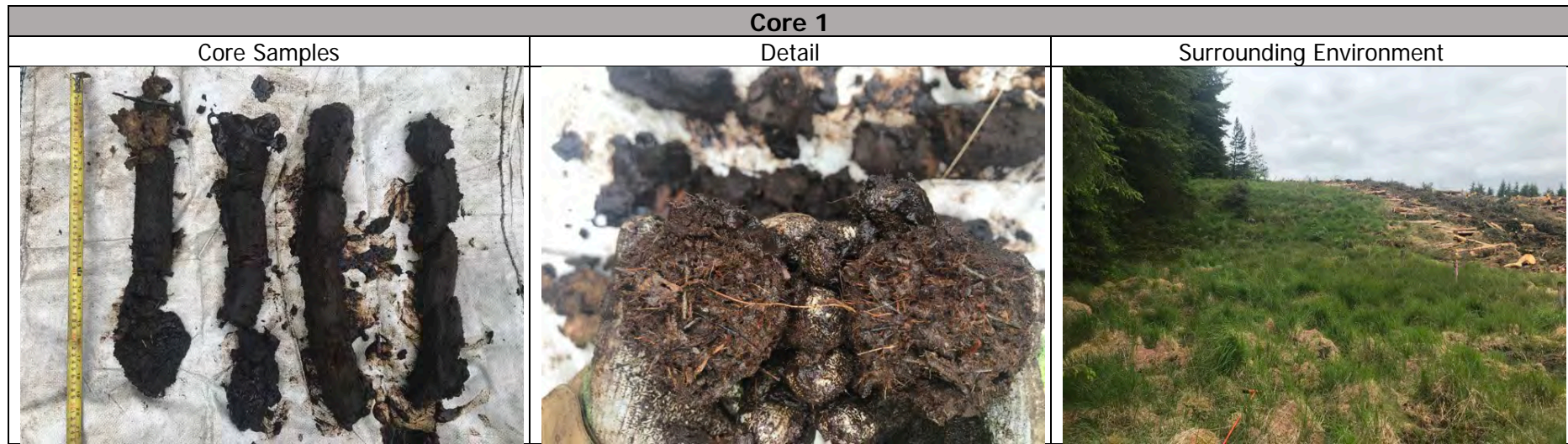
vi. Other observations

When peat is freshly sampled and before it darkens by oxidation, note is taken of its colour, stratification, the presence of visible mineral matter and any other features of interest.

Photographs of the peat cores obtained from Crossaig along with information relating to the parameters outlined above are presented overleaf with a summary of the information gathered during the peat coring process presented in the main body of text of the Peat Slide Risk Assessment (PSRA).

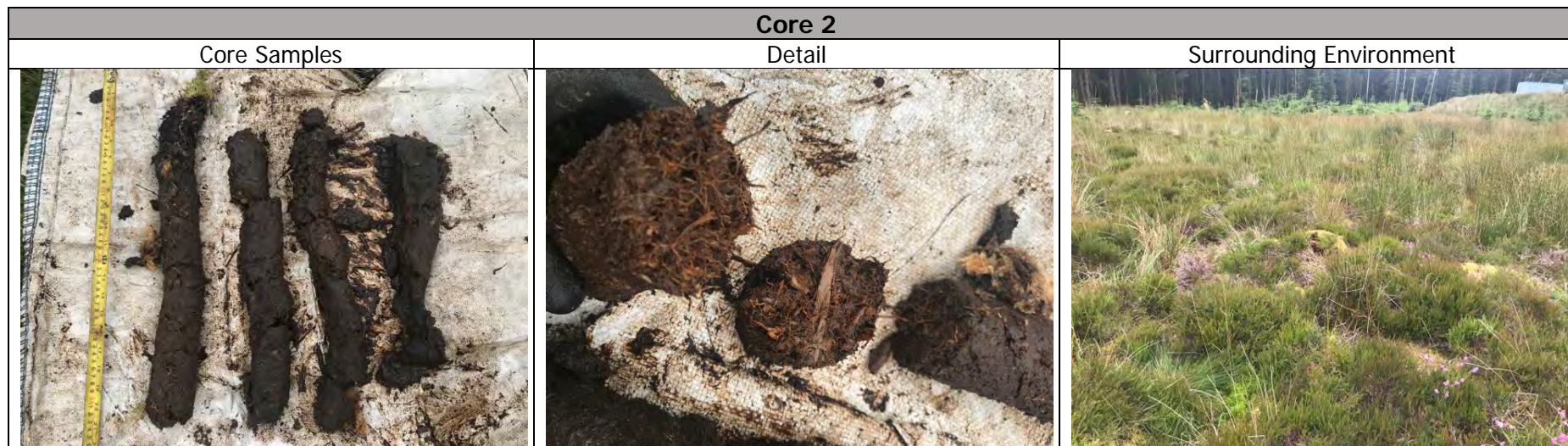
It was noted during sampling that the water table at sample 1 was 0.3 m below the surface and that sample 2 had a high water content.

Peat Coring Record



Location	Depth (m)	Firmness of Surface (P)	Von Post (H)	Fine Fibres (F)	Coarse Fibres (R)	Wood Remains (W)	Other Observations (Colour)
E 18255, N 650413	0.00 – 0.50	2	3	2	3	1	Dark Brown
	0.51 – 1.00		4	2	2	2	Dark Brown
	1.01 – 1.50		5	1	2	2	Dark Brown
	1.51 – 2.00		6	2	1	1	Dark Brown

Peat Coring Record



Location	Depth (m)	Firmness of Surface (P)	Von Post (H)	Fine Fibres (F)	Coarse Fibres (R)	Wood Remains (W)	Other Observations (Colour)
E 182671, N 650128	0.00 – 0.50	3	4	2	3	1	Brown
	0.51 – 1.00		4	3	2	1	Brown
	1.01 – 1.50		6	3	1	1	Dark Brown
	1.51 – 2.00		7	3	1	1	Dark Brown